

Indoor Air Quality Impacts
of Residential HVAC Systems
Phase II.A Report: Baseline
and Preliminary Simulations

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Abstract

NIST has completed Phase II.A of a project to study the impact of HVAC systems on residential indoor air quality and to assess the potential for using residential forced-air systems to control indoor pollutant levels. In this effort, NIST is performing whole building airflow and contaminant dispersal computer simulations with the program CONTAM93 to assess the ability of modifications of central forced-air heating and cooling systems to control pollutant sources relevant to the residential environment. This report summarizes the results of Phase II.A of this project, which consisted of three major efforts: baseline simulations of contaminant levels without indoor air quality (IAQ) controls, design of the IAQ control retrofits, and preliminary simulations of contaminant levels with the IAQ control retrofits. In Phase II.B of the study, all of the baseline cases will be modified to incorporate the IAQ control retrofits. The retrofit results will then be compared to the baseline results to evaluate the effectiveness of the retrofits.

The pollutant concentrations in a building depend on many factors including the configuration of the building zones, the air leakage of the building envelope and of interior partitions, wind pressure profile on the building envelope, pollutant source strengths and temporal profiles, heating and cooling system airflow rates, furnace filter efficiency, characteristics of reversible pollutant sinks in the building, individual pollutant decay or deposition rates, and ambient weather and pollutant concentrations. This report describes the input data used to model the baseline houses with CONTAM93 and presents the results of the baseline simulations in the form of the transient pollutant concentrations for selected simulations and a summary of peak and average concentrations for all baseline simulations. Three indoor air quality control technologies were then selected for incorporation into the baseline house models to determine their effectiveness in controlling the modeled pollutant sources. The technologies include the following: electrostatic particulate filtration, heat recovery ventilation, and an outdoor air intake damper on the forced-air system return. Selected baseline cases were then modified to implement these indoor air quality control retrofits, and preliminary simulations were performed to demonstrate the ability of the program to model the control technologies.

Key Words: airflow modeling, building technology, computer simulation, filtration, heat recovery ventilator, HVAC system, indoor air quality, infiltration, residential buildings, ventilation



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Introduction

Despite the increasing interest in residential indoor air quality (IAQ) problems, only limited research has been conducted which integrates the analysis of pollutant sources, residential heating and cooling system operation, and building characteristics. While central forced-air heating and cooling systems may provide solutions to some IAQ problems, such an integrated approach is required to analyze these options. Because large quantities of indoor air circulate through these systems, they offer the potential for treating the indoor air and then distributing this treated air through the system ductwork to the building. Also, outdoor air brought into the building by the forced-air system can be distributed throughout the building by this ductwork. Most modeling studies of IAQ in residential buildings have employed very simple models of the building and its systems, ignoring the multizone nature of the airflows involved. The use of such simple analytical procedures has limited our understanding of the impact of central forced-air heating and cooling systems on residential IAQ and the possibility of using these and other systems to mitigate IAQ problems.

The National Institute of Standards and Technology (NIST) is conducting a study for the U.S. Consumer Product Safety Commission (CPSC) to assess the potential effectiveness of existing heating, ventilating, and air conditioning (HVAC) technology to reduce the levels of selected pollutants in single-family residential buildings. This effort is employing a new multizone airflow and contaminant dispersal modeling program, CONTAM93 (1). In this effort, NIST is performing whole building airflow and contaminant dispersal computer simulations to assess the ability of modifications of central forced-air heating and cooling systems to control pollutant sources relevant to the residential environment. Phase I of the project included conducting a literature review, developing a detailed simulation plan, and hosting a workshop to discuss the project, and was described in a previous report (2). This report summarizes the results of Phase II.A which consisted of three major tasks: baseline simulations of contaminant levels without IAQ controls, design of the IAQ control retrofits, and preliminary simulations of contaminant levels with the IAQ control retrofits in place.

In Phase II.B of the study, the baseline HVAC systems will be modified to incorporate the IAQ control technologies described in this report and simulations will be performed for all conditions under which baseline simulations were performed. The Phase II.B simulation results will be compared with the results presented here to determine the effectiveness of the IAQ modifications at controlling the selected pollutant sources.

Contents of Report

The first section of the report describes the baseline simulations performed. The program CONTAM93 (1) was used to calculate airflows and pollutant distributions for the houses and pollutant sources described in the report on Phase I of the project (2). The houses modeled are not based on real buildings but are intended to be representative of typical buildings. This first section presents the input data used to describe the houses, HVAC systems, pollutants, sources, and boundary conditions in the baseline simulations. In addition, this section summarizes the

results of the baseline simulations including transient pollutant concentrations for selected simulations and a summary of peak and average concentrations for all baseline simulations.

The second section describes the indoor air quality control technologies that will be evaluated in the computer simulations during Phase II.B. These technologies will be incorporated into the baseline house models to determine their effectiveness in controlling the selected pollutant sources. The three technologies described in this section include electrostatic particulate filtration, heat recovery ventilation, and an outdoor air intake damper on the forced-air system return. This section describes each of these technologies and includes revisions of the baseline house duct drawings. In addition, this section contains an estimate of the equipment and installation costs and a revision of the thermal load calculations based on the modifications. Finally, the impacts of each of these technologies on "other contaminants" are discussed qualitatively. These other contaminants, as described in the original project work statement, include contaminants that have typically been of concern to designers of residential ventilation systems including cooking odors, tobacco smoke, moisture, outdoor pollen, outdoor odors and ozone.

The third section presents the results of preliminary simulations of the IAQ control retrofits. These simulations involved modifying selected baseline simulation cases with the three IAQ control retrofits. The preliminary simulations were performed to demonstrate the ability of the program to model the IAQ control technologies.

The report includes two appendices. The first appendix describes modeling performed to characterize the airflow in the houses including the results of fan pressurization simulations and whole house infiltration simulations. The second appendix includes summary tables of the baseline and preliminary simulation results.

Baseline Simulations

This section of the report describes the baseline simulations performed in Phase II.A. This section presents the input data describing the houses, HVAC systems, pollutants, sources, and boundary conditions modeled in the baseline simulations. In addition, this section summarizes the results of the baseline simulations including transient pollutant concentrations for selected simulations and a summary of peak and average concentrations for all baseline simulations.

Baseline Simulation Input Data

Calculating airflow rates and contaminant concentrations with CONTAM93 or any other multizone model requires the following input: the configuration and volume of the building zones, the air leakage paths through the building envelope and interior walls, wind pressure profile on the building envelope, pollutant source strengths and temporal profiles, HVAC system flows, furnace filter efficiency, characteristics of reversible pollutant sinks, individual pollutant decay or deposition rates, and ambient weather and pollutant concentrations. This section describes the input data used in the baseline simulations.

The study included eight building models - a ranch and a two-story house, located in two sites (Miami and Minneapolis), with typical and low values of airtightness. The Phase I NISTIR (2) described the layout and dimensions of each house and contained floorplan drawings. Simulations were performed under three sets of weather conditions (cold, mild, and hot) for each building. Each simulation was performed for a one-day cycle repeated until peak concentrations converged to a specified tolerance. Referring to all pollutant sources modeled for a single building as one simulation, there were a total of 24 baseline simulation cases. Table 1 lists the baseline simulations by house type, location, airtightness and weather condition.

Table 1 - Baseline simulations

| Simulation | House type | Location Location | Airtightness | Weather |
|------------|------------|-------------------|--------------|---------|
| SIM1FLC | ranch | Miami | typical | cold |
| SIM1FLM | ranch | Miami | typical | mild |
| SIM1FLH | ranch | Miami | typical | hot |
| SIM1FTC | ranch | Miami | tight | cold |
| SIM1FTM | ranch | Miami | tight | mild |
| SIM1FTH | ranch | Miami | tight | hot |
| SIM1MLC | ranch | Minneapolis | typical | cold |
| SIM1MLM | ranch | Minneapolis | typical | mild |
| SIM1MLH | ranch | Minneapolis | typical | hot |
| SIM1MTC | ranch | Minneapolis | tight | cold |
| SIM1MTM | ranch | Minneapolis | tight | mild |
| SIM1MTH | ranch | Minneapolis | tight | hot |
| SIM2FLC | two-story | Miami | typical | cold |
| SIM2FLM | two-story | Miami | typical | mild |
| SIM2FLH | two-story | Miami | typical | hot |
| SIM2FTC | two-story | Miami | tight | cold |
| SIM2FTM | two-story | Miami | tight | mild |
| SIM2FTH | two-story | Miami | tight | hot |
| SIM2MLC | two-story | Minneapolis | typical | cold |
| SIM2MLM | two-story | Minneapolis | typical | mild |
| SIM2MLH | two-story | Minneapolis | typical | hot |
| SIM2MTC | two-story | Minneapolis | tight | cold |
| SIM2MTM | two-story | Minneapolis | tight | mild |
| SIM2MTH | two-story | Minneapolis | tight | hot |

Detailed information on building component leakage of the houses is not available as the houses modeled were not based on real buildings. However, since there is no attempt to compare predictions with experimental data, the building leakage modeled needs only to be reasonable in magnitude and distribution. Table 2 shows all of the leakage paths between the zones of the Miami ranch house (see Figure 1 for the ranch house floorplan and zone labeling and Figure 2 for the two-story house floorplan and zone labeling). The Minneapolis houses have basements (zone label BMT) that are not shown in the figures. Table 3 lists the values for those leakage paths for both the typical and tight cases. The Table 3 leakage areas are for a reference pressure difference of 4 Pa and a discharge coefficient of 1.0 and are based on values listed in Table 23-3 of ASHRAE (3) unless otherwise noted. The typical values were generally based on "best estimate" and/or uncaulked entries in the ASHRAE table, while the tight values were based on minimum and/or caulked entries. All doors connecting zones other than closets were modeled as open. The same leakage values were used for the other houses, although the paths connecting the zones differed depending on the house configurations.

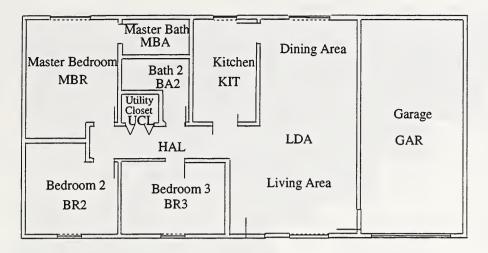


Figure 1 - Ranch house floorplan and zones

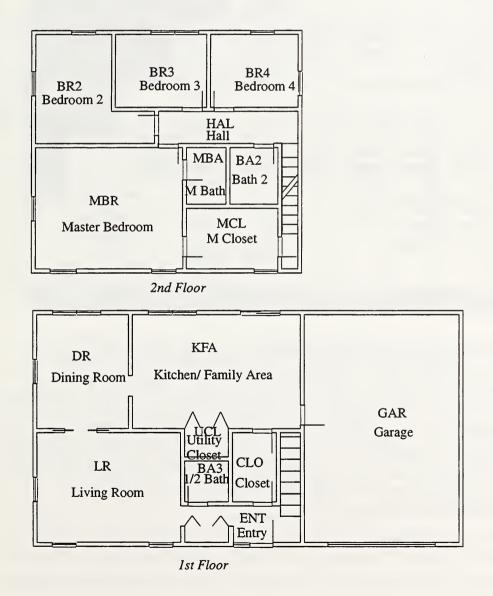


Figure 2 - Two-story house floorplan and zones

Table 2 - Air leakage paths for Miami ranch house

| | MBR | BR2 | BR3 | MBA | BA2 | UCL | KIT | LDA | HAL | GAR | ATC |
|-----|--------------------|--|----------------------|---------------------|---------------------|----------------------------------|---------------------------|-----------------------------------|-------------|--|-----|
| BR2 | INTW OUTL | 11 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 | . a.e.s | | in the second | | | | | | |
| BR3 | | INTW OUTL | | | | | | 3.40 | | | |
| MBA | INTD INTW | | | | latin. | e services States Services | | | | | |
| BA2 | INTW OUTL | | | INTW OUTL | | - | 7.26 | | | | |
| UCL | INTW | | | | INTW | | | | | | |
| KIT | | | | INTW OUTL | INTW OUTL | | | | | | |
| LDA | | | INTW OUTL | | | | INTW INTD OUTL | | | 1885 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - | |
| HAL | INTD INTW | INTD INTW | INTD INTW OUTL | | INTD INTW | CLD INTW | INTD INTW OUTL | HAD | | | |
| GAR | | | | | | | | EXTD EXW OUTL | | | |
| ATC | CEIL CPEN | CEIL CPEN | CEIL CPEN | CEIL CPEN PIP | CEIL CPEN PIP | CEIL | CEIL CPEN | CEIL CPEN CPEN | CEIL ATD | | |
| AMB | WIN EXW OUTL | WIN EXW OUTL | WIN EXW OUTL | EXV EXW OUTL | EXV | | WIN EXV EXW OUTL | SGD EXTD WIN EXW OUTL | | GAD GARF EXW | VNT |
| | MBR | BR2 | BR3 | MBA | BA2 | UCL | KIT | LDA | HAL | GAR | ATC |

The infiltration through a building's envelope also depends on the static pressure distribution created by the wind on the building's exterior surfaces. The relationship between wind and surface pressures are characterized by wind pressure coefficients which depend on the wind direction, the building shape, the position on the building surface, and the presence of shielding near the building. The surface pressure coefficients for the building walls were based on Equation 23-8 of ASHRAE (3). The coefficient for the flat garage roof was based on Figure 14-6 of ASHRAE (3). The ASHRAE wind pressure coefficients do not include shielding effects and no modifier for shielding effects was used, however, recent studies have reported on the shielding effects of trees (4) and rows of houses (5).

Table 3 - Air leakage values

| Name | Description | Typical | Tight |
|------|---|-------------------------------------|-------------------------------------|
| ATD | Attic door | 30 cm ² /ea | 18 cm ² /ea |
| CEIL | Ceiling [Based on general ceiling] | 1.8 cm ² /m ² | $0.79 \text{ cm}^2/\text{m}^2$ |
| CLD | Closet door (closed) [Based on interior door] | 0.9 cm ² /m | 0.25 cm ² /m |
| | Closet door frame [Based on general door frame] | 25 cm²/ea | 12 cm²/ea |
| CPEN | HVAC ceiling penetration [Based on kitchen vent with damper closed] | 5 cm ² /ea | 1 cm ² /ea |
| EXTD | Exterior door [Single] | 21 cm²/ea | 12 cm²/ea |
| | Door frame [Wood] | $1.7 \text{ cm}^2/\text{m}^2$ | $0.3 \text{ cm}^2/\text{m}^2$ |
| EXV | Bathroom exhaust vent | 20 cm²/ea | 10 cm²/ea |
| | Kitchen exhaust vent | 40 cm ² /ea | 5 cm ² /ea |
| EXW | Ceiling-wall joint | 1.5 m ² /m | 0.5 m ² /m |
| | Floor-wall joint | 4 cm ² /m | 0.8 cm ² /m |
| | Wall-wall joint [Based on ceiling-wall joint] | 1.5 m ² /m | 0.5 m ² /m |
| GAD | Garage door [Based on general door (2 m x 4 m)] | 0.45 cm ² /m | $0.31 \text{ cm}^2/\text{m}$ |
| | Garage door frame [Wood] | $1.7 \text{ cm}^2/\text{m}^2$ | $0.3 \text{ cm}^2/\text{m}^2$ |
| GARF | Garage roof [Based on general ceiling] | $1.8 \text{ cm}^2/\text{m}^2$ | $0.79 \text{ cm}^2/\text{m}^2$ |
| HAD | Hall doorway | 2.4 m²/ea | 2.4 m²/ea |
| INTD | Interior door (closed) [Based on Table 4.2 of Klote and Milke (6)] | 140 cm ² /ea | 75 cm²/ea |
| | Interior door (open) | 2.1 m²/ea | 2.1 m²/ea |
| INTW | Interior wall [Based on gypsum board on stud wall (Shaw et al. 7)] | 2.0 cm ² /m ² | 2.0 cm ² /m ² |
| OUTL | Electric outlet | 2.5 cm ² /ea | 0.5 cm ² /ea |
| PIP | Piping penetrations | 6 cm ² /ea | 2 cm²/ea |
| SGD | Sliding glass door | 22 cm²/ea | 3 cm ² /ea |
| VNT | Attic vent [Based on Table 21-1 of 3] | $1 \text{ cm}^2 / 300 \text{ cm}^2$ | $1 \text{ cm}^2 / 300 \text{ cm}^2$ |
| WIN | Double hung window | 2.5 cm ² /m | 0.65 cm ² /m |
| | Window framing [Wood] | 1.7 cm ² /m ² | $0.3 \text{ cm}^2/\text{m}^2$ |

The building HVAC systems were designed in Phase I of the study and are described in the Phase I report (2). This earlier report contains the heating and cooling equipment types and descriptions, overall and individual supply and return airflow rate design values for both heating and cooling, and drawings showing the system equipment and duct locations and duct sizes. In addition to this information, CONTAM93 requires information on the system operation, specifically, an on-off schedule. The schedule was determined by calculating the fractional on-time required to meet the cooling or heating load for each 3-hour period of the day. A control profile incorporating this schedule was then input for each simulation. For the baseline simulations, the HVAC systems included standard furnace filters with constant efficiencies of 5% for fine particles and 90% for coarse particles. Fine particles are defined as having a diameter less than 2.5 μ m (the efficiency is based on a diameter of 0.6 μ m); coarse particles are defined as having a diameter greater than 2.5 μ m (the efficiency is based on a diameter of 6 μ m). These

efficiency values are based on assumed arrestance for these filters of about 90% and a review of manufacturers' test data. No outdoor air intake is included for the baseline HVAC systems.

Another important consideration for the HVAC systems is duct leakage. Since the duct system itself is not modeled in these simulations, duct leakage is modeled by including an additional system supply or return point and reducing the other supply and return flows by the corresponding amount rather than by an effective leakage area. Cummings et al. 1991 (8) tested duct leakage in 160 houses in Florida and found that return leaks were dominant in the majority of homes. They reported an average return leak fraction of 10.7% (based on ratio of leakage flow to total system flow). For the Minneapolis houses, a return leak of 10% was included in the basement. For the Miami ranch house, a supply leak of 10% was included in the attic because the system has a central return. For the Miami two-story house, no leaks were included because all ducts and equipment are internal. The air distribution system layouts were designed based on guidelines published by the National Association of Home Builders (9) and drawings are included in the Phase I report (2).

The ambient boundary conditions required by CONTAM93 include weather and outdoor pollutant concentrations. The weather conditions were chosen by selecting a hot, mild, and cold day for each location from Weather Year for Energy Calculation (WYEC) data (10). The WYEC data is presented in Tables 5 and 6 for Miami and Minneapolis, respectively, and includes temperature, wind speed, and wind direction from north.

Table 5 - Miami weather data

| | | Cold | uoio s | | Mild | | Hot | | |
|------|-----------|-------------------------|------------|-----------|-------------------------|------------|-----------|-------------------------|------------|
| Hour | T (°C) | V _{wind} (m/s) | Dir (°) | T (°C) | V _{wind} (m/s) | Dir (°) | T (°C) | V _{wind} (m/s) | Dir (°) |
| 0 | 2.8 | 2.3 | 320 | 13.3 | 3.9 | 360 | 26.7 | 0 | 0 |
| 1 | 2.8 | 2.3 | 300 | 13.3 | 2.7 | 360 | 26.1 | 1.2 | 200 |
| 2 | 2.8 | 3.5 | 310 | 13.3 | 3.5 | 360 | 26.1 | 1.2 | 200 |
| 3 | 2.8 | 2.7 | 320 | 13.9 | 1.9 | 20 | 25.6 | 1.6 | 200 |
| 4 | 2.2 | 2.3 | 310 | 13.3 | 2.7 | 20 | 25.6 | 1.9 | 200 |
| 5 | 2.2 | 3.5 | 310 | 13.9 | 1.6 | 360 | 26.1 | 1.9 | 230 |
| 6 | 2.8 | 2.7 | 320 | 13.3 | 2.3 | 340 | 25.6 | 1.9 | 200 |
| 7 | 3.3 | 3.5 | 300 | 14.4 | 2.3 | 340 | 26.7 | 1.6 | 230 |
| 8 | 4.4 | 2.3 | 290 | 16.1 | 2.7 | 340 | 27.2 | 1.9 | 200 |
| 9 | 6.1 | 2.7 | 330 | 21.1 | 4.7 | 70 | 30.6 | 2.3 | 200 |
| 10 | 8.9 | 3.1 | 320 | 23.3 | 4.7 | 70 | 31.7 | 2.3 | 230 |
| 11 | 11.7 | 2.3 | 320 | 23.3 | 5.1 | 70 | 32.8 | 0 | 0 |
| 12 | 13.9 | 2.7 | 330 | 23.3 | 5.4 | 70 | 33.3 | 2.3 | 200 |
| 13 | 14.4 | 2.7 | 350 | 22.8 | 5.1 | 70 | 33.3 | 3.9 | 140 |
| 14 | 16.1 | 2.3 | 360 | 22.8 | 5.4 | 70 | 32.8 | 4.3 | 180 |
| 15 | 17.2 | 0.8 | 40 | 22.2 | 4.7 | 70 | 31.7 | 4.7 | 160 |
| 16 | 17.8 | 2.7 | 40 | 21.7 | 3.9 | 90 | 30.6 | 1.9 | 290 |
| 17 | 17.2 | 3.5 | 20 | 21.7 | 3.1 | 90 | 31.7 | 3.1 | 140 |
| 18 | 16.7 | 1.9 | 340 | 21.7 | 4.3 | 70 | 30.6 | 2.3 | 160 |
| 19 | 16.1 | 2.3 | 340 | 21.1 | 4.3 | 90 | 27.8 | 1.6 | 50 |
| 20 | 15 | 1.6 | 350 | 21.1 | 2.7 | 90 | 27.8 | 1.2 | 50 |
| 21 | 14.4 | 1.9 | 350 | 21.1 | 3.1 | 90 | 27.2 | 1.6 | 200 |
| 22 | 16.1 | 2.3 | 30 | 21.7 | 1.2 | 90 | 26.1 | 2.3 | 230 |
| 23 | 16.1 | 2.3 | 60 | 21.7 | 2.3 | 90 | 26.1 | 1.2 | 250 |
| 24 | 17.2 | 3.5 | 60 | 20.6 | 3.1 | 50 | 26.1 | 0 | 0 |

Table 6 - Minneapolis weather data

| | Cold | | | Mild | | | Hot | | |
|------|-----------|-------------------------|------------|-----------|-------------------------|------------|-----------|-------------------------|------------|
| Hour | T (°C) | V _{wind} (m/s) | Dir (°) | T (°C) | V _{wind} (m/s) | Dir (°) | T (°C) | V _{wind} (m/s) | Dir (°) |
| 0 | -21.1 | 1.6 | 330 | 7.8 | 1.9 | 60 | 21.1 | 3.1 | 180 |
| 1 | -21.1 | 1.6 | 330 | 7.8 | 1.9 | 40 | 20 | 2.7 | 180 |
| 2 | -21.1 | 3.1 | 350 | 7.8 | 3.1 | 90 | 18.9 | 2.7 | 180 |
| 3 | -21.1 | 3.1 | 350 | 7.2 | 1.9 | 100 | 17.8 | 1.9 | 180 |
| 4 | -21.1 | 3.1 | 350 | 7.2 | 4.7 | 130 | 18.3 | 1.6 | 158 |
| 5 | -21.1 | 3.1 | 350 | 7.2 | 3.9 | 130 | 17.2 | 2.7 | 135 |
| 6 | -21.7 | 3.5 | 350 | 7.2 | 3.1 | 120 | 17.8 | 3.5 | 158 |
| 7 | -21.7 | 2.7 | 340 | 7.2 | 3.9 | 140 | 20 | 1.9 | 158 |
| 8 | -21.7 | 2.7 | 350 | 7.8 | 2.7 | 120 | 24.4 | 4.7 | 180 |
| 9 | -21.1 | 3.9 | 340 | 8.9 | 3.1 | 130 | 26.1 | 5.8 | 180 |
| 10 | -20.6 | 3.9 | 310 | 7.8 | 4.3 | 130 | 28.3 | 6.6 | 203 |
| 11 | -20.6 | 4.7 | 310 | 8.3 | 4.7 | 130 | 30 | 6.2 | 203 |
| 12 | -20.6 | 3.9 | 320 | 8.9 | 4.3 | 140 | 30.6 | 6.2 | 203 |
| 13 | -20.6 | 4.3 | 320 | 8.9 | 4.7 | 140 | 31.1 | 7 | 203 |
| 14 | -20 | 5.1 | 300 | 8.3 | 6.2 | 120 | 31.1 | 7.4 | 203 |
| 15 | -20 | 4.7 | 290 | 8.9 | 6.2 | 110 | 31.1 | 6.6 | 203 |
| 16 | -20.6 | 4.3 | 310 | 8.9 | 5.8 | 130 | 31.1 | 6.6 | 203 |
| 17 | -21.1 | 3.5 | 290 | 9.4 | 5.1 | 130 | 28.9 | 4.7 | 203 |
| 18 | -22.8 | 3.1 | 280 | 9.4 | 5.4 | 130 | 29.4 | 4.7 | 180 |
| 19 | -23.3 | 2.7 | 280 | 11.1 | 5.4 | 160 | 27.8 | 4.7 | 180 |
| 20 | -24.4 | 3.1 | 300 | 11.7 | 5.8 | 170 | 26.1 | 4.3 | 180 |
| 21 | -25 | 3.1 | 280 | 11.1 | 6.2 | 180 | 24.4 | 3.9 | 180 |
| 22 | -25.6 | 2.7 | 280 | 11.1 | 5.8 | 200 | 23.9 | 3.9 | 180 |
| 23 | -27.2 | 2.3 | 240 | 10.6 | 6.2 | 220 | 23.3 | 4.7 | 158 |
| 24 | -28.9 | 2.3 | 240 | 7.8 | 2.7 | 240 | 22.8 | 4.3 | 180 |

Outdoor pollutant concentrations vary by location and over time at any one location. The concentrations used as boundary conditions for the indoor sources in the simulations were selected as typical outdoor conditions and are not meant to represent the actual conditions at any specific location. The values used were specified per the schedules in Table 7. The CO and NO₂ concentrations were chosen based on review of US EPA air quality documents (11, 12, 13). They were chosen to have a diurnal pattern with morning and afternoon peaks. The selected CO and NO₂ concentration schedules are very similar to values measured outside a research house in Chicago (Figure 3.2 of 14). Fine particles and TVOCs are not discussed in the EPA documents. The ambient fine particle concentration was chosen based on the average of reported average measurements for four US cities (Table 4 of 15). The TVOC concentration chosen is in the

middle of the reported range of 10 to 211 μ g/m³ measured at 68 sites in the US (16). The fine particle and TVOC concentrations were assumed to be constant throughout the day.

In addition to the ambient concentrations in Table 7 that served as the boundary conditions for the indoor sources, elevated levels of CO, coarse particles, and NO₂ were simulated in order to evaluate the effect of the IAQ control technologies on pollutants brought into residences from the outdoors. These elevated pollutant concentrations were selected based on review of US EPA air quality documents (11, 12, 13) and were specified per the schedules in Table 8.

Table 7 - Outdoor pollutant concentration schedules

| | A | | | | |
|------------------------|-------|------|-------|---------|---------|
| Hour of day | 0 - 7 | 7-9 | 9 -17 | 17 - 19 | 19 - 24 |
| CO (ppm) | 1 | 2 | 1.5 | 3 | 1.5 |
| NO ₂ (ppm) | 0.02 | 0.04 | 0.02 | 0.04 | 0.02 |
| Fine particles (µg/m³) | 13 | 13 | 13 | 13 | 13 |
| TVOCs (μg/m³) | 100 | 100 | 100 | 100 | 100 |

Table 8 - Elevated outdoor pollutant concentrations schedule

| Hour of day | 0 - 7 | 7-9 | 9 -17 | 17 - 19 | 19 - 24 |
|--------------------------|-------|-----|-------|---------|---------|
| CO (ppm) | 4 | 8 | 7 | 12 | 6 |
| NO ₂ (ppm) | 0.2 | 0.4 | 0.2 | 0.4 | 0.2 |
| Coarse particles (µg/m³) | 75 | 75 | 75 | 75 | 75 |

The Phase I report (2) described the pollutant sources considered for inclusion in the study. The pollutant sources used in the baseline simulations included several VOC burst sources (medium strength source based on a polish and high strength source based on a spray carpet cleanser (17)), a constant VOC area source (based on a PVC flooring material with high emissions (18)), and combustion sources (based on medium source strengths for ovens and space heaters (19)) of CO, NO₂, and fine particles. While the source strength used for the flooring material isbased on a material with high emissions, it is only moderately higher than the range of 0.17 to 2.11 mg/m²h recently reported in 5 day emission tests of finished particleboard (20). Table 9 lists detailed information on these sources including the zones (see Figures 1 and 2 for zone labels, also BMT is the basement zone) in which they are located, source strengths, and schedules.

Table 9 - Pollutant sources

| Source name | Pollutant | Zone(s) | Source strength | Schedule |
|-------------------|-----------------|---|-------------------------|-------------------------------------|
| Burst (medium) | TVOCs | Several | 300 mg/h | 9 - 9:30 am 7 - 7:30 p.m. |
| Burst (high) | TVOCs | GAR and BMT | 1100 mg/h | 9 - 10 am 7 - 8 p.m. |
| Flooring material | TVOCs | All but GAR, ATC | 7.0 mg/h m ² | constant |
| Oven | СО | KIT (ranch house), KFA (two-story house) | 1900 mg/h | 7 - 7:30 am 6 - 7 p.m. |
| Oven | NO ₂ | KIT (ranch house), KFA (two-story house) | 160 mg/h | 7 - 7:30 am 6 - 7 p.m. |
| Oven | Fine particles | KIT (ranch house), KFA (two-story house) | 0.2 mg/h | 7 - 7:30 am 6 - 7 p.m. |
| Heater | СО | GAR and BMT | 1000 mg/h | 7 - 10 am (GAR) 7 - 9 p.m. (BMT) |
| Heater | NO ₂ | GAR and BMT | 250 mg/h | 7 - 10 am (GAR) 7 - 9 p.m. (BMT) |
| Heater | Fine particles | GAR and BMT | 2 mg/h | 7 - 10 am (GAR) 7 - 9 p.m. (BMT) |

In addition to the sources listed in Table 9, the simulation plan in the Phase I report (2) included a newly-finished floor as a floor-area based decaying source of VOCs. A test simulation with a medium strength source, modeled as a first order exponential decay source with initial emission rate of 17400 mg/m²h and decay constant of 1.24 h⁻¹ (based on a stain product (21)) was performed for the Miami ranch house. This source resulted in extremely high concentrations of TVOCs with a peak concentration of over 2 g/m³ and a concentration of 37 mg/m³ at the end of the day. None of the IAQ control retrofits being evaluated can be expected to have a significant impact on the extremely high concentrations from this source during the one-day simulation period. Therefore, this source was not included in the remaining baseline simulations. Decaying high-strength sources such as this one are of interest and may be studied in the future with simulations of longer duration.

Reversible sink effects for the VOCs were modeled with sink elements based on a boundary layer diffusion controlled (BLDC) model with a linear adsorption isotherm. The BLDC adsorption model is described by Axley (22). The parameters required for this sink model are the film mass transfer coefficient, the adsorbent mass, and the isotherm partition coefficient, and these parameters would vary over time and by location within a house. However, since little real data is available for these parameters (which depend on factors such as gas diffusion properties, airflow rates, and adsorbent material) and because the goal was to obtain a reasonable estimate of the reversible sink effects, constant values were used for all of the parameters and only the adsorbent mass was varied by zone. The film mass transfer coefficient used was 35 μ m/s and was calculated from equation 3.17a of Axley (22) with an assumed air velocity of 0.001 m/s, effective length of 4 m, Schmidt number of 1.0, and binary diffusion coefficient of 1.0 x 10⁻⁵ m²/s. The partition coefficient used was 0.5 g-air/g-sorbent and was estimated from parameters reported for

an empirical sink model for an experimental case of alkanes emitted by a wood stain in a test house (23). The adsorbent mass used was based on a mass of 6 kg per m² of adsorbent surface area which was assumed to be equal to half of the zone interior surface area.

Nitrogen dioxide decay and particle deposition were modeled as single-reactant first order reactions with a single, constant value in all rooms of the houses. Nitrogen dioxide decay depends strongly on the materials present in a house (e.g., floor and wall coverings, furnishings, etc.) and a wide range of measured values have been reported including a range of 0.09 - 13.74 h⁻¹ by Lee et al. (24). Other studies have reported average NO₂ decay rates of 0.17, 0.29, 0.65, 0.8, 0.82, and 2.07 h⁻¹ (25, 26, 27, 28, 29, 24). The kinetic rate coefficient used for NO₂ decay was 0.87 h⁻¹ and is based on the average of measurements in a contemporary research house reported by Leslie et al. (14).

Particle deposition depends on the size and type of particles, particle concentration, airflow conditions, and surfaces available for deposition. The particle decay rate used for fine particles was 0.08 h⁻¹ and was reported by Traynor et al. (30) for combustion products from a wood-burning stove in a test house. Offerman et al. (31) reported a similar mass-averaged value of 0.1 h⁻¹ for tobacco smoke particles in a research house. The decay rate can be calculated as the product of an average deposition velocity and a room surface-to-volume ratio. Assuming a room surface-to-volume ratio of 2 m⁻¹ (the actual value will depend on room geometry, furnishings, and surface finishes), a decay rate of 0.08 h⁻¹ corresponds to a deposition velocity of approximately 0.001 cm/s. Sinclair et al. (32, 33) reported higher average deposition velocities of 0.005 cm/s for fine-mode sulfate in telephone equipment buildings. However, the nature of the indoor environment, and especially the airflow conditions, in a detached single-family home and a commercial building are very different. Nazaroff et al. (34) discusses the use of deposition velocity and warns that "Deposition velocities determined for one indoor environment can only be applied to another to the extent that the air flow conditions are similar."

In the only report of coarse particle deposition rates in a test house found in the literature, Byrne et al. (35) reported values of 1.51 and $2.10~h^{-1}$ for 4 μm particles in an unfurnished and furnished room, respectively. The reported mean deposition velocities of 0.027 to 0.038 cm/s fall within the range of approximately .01 to 0.1 cm/s calculated from a natural convection deposition model by Nazaroff and Cass (36). The actual decay rate for the coarse outdoor air particles modeled in the simulations would depend on the size distribution of the particles. Since no specific distribution has been assumed , a decay rate of 1.5 h^{-1} was chosen based on the lower value reported by Byrne.

Baseline Simulation Results

The results of each of the 24 simulations listed in Table 1 include pollutant concentrations for up to 18 pollutants in each of the building zones for each 15-minute time step of the 24-hour simulation period. The complete transient simulation results are not presented here but are available in spreadsheet files. Instead, this section presents examples of the transient pollutant concentrations for selected simulations. Figures 3 through 6 show the pollutant concentrations in Zone LDA resulting from selected pollutant sources for simulation SIM1FLC (the typical Miami

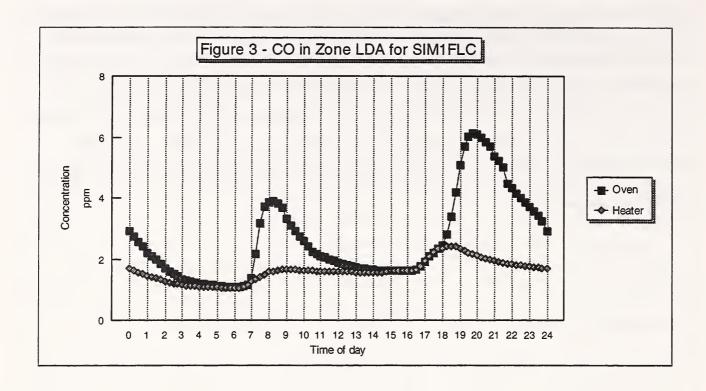
ranch house in cold weather). Figures 7 through 10 show the corresponding results for SIM1FTC (the tight Miami ranch house in cold weather). Although these figures are only examples of transient results, some observations can be made into trends and factors affecting the predicted contaminant concentrations. A complete summary of peak and 24-hour, 4-hour, and 1-hour average concentrations for all baseline simulations are included in Tables 1a through 24e of Appendix B.

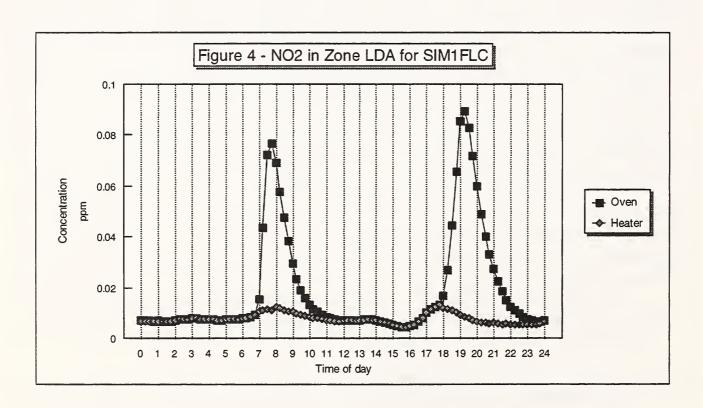
Figures 3 and 7 show the CO concentrations in Zone LDA resulting from the oven and heater sources (CO.1 and CO.2 in Tables 1 and 4 of Appendix B) for SIM1FLC and SIM1FTC, respectively. Both graphs show two daily peaks due to the operation of the oven. For the tight house, the peaks are shifted to a slightly later time due to reduced outdoor airflow into the house which resulted in less mixing of CO from the kitchen into the rest of the house. The heater source causes much lower concentrations than the oven source due to the low airflow rate from the garage into the house and the lower source emission rate. The resulting CO concentrations for the heater source are influenced primarily by the outdoor level. There is more damping of the outdoor variations in the tight house than the typical house due to the reduced air infiltration rate.

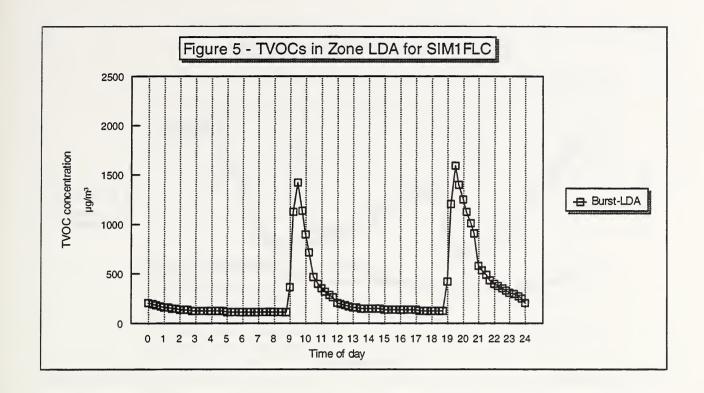
Figures 4 and 8 show the NO, concentrations (NO2.1 and NO2.2 in Tables 1 and 4 of Appendix B) in Zone LDA resulting from the oven and heater sources for SIM1FLC and SIM1FTC. The NO, concentrations show some of the same characteristics as the CO concentrations, with two peaks from the oven and a damped dependence on the outdoor concentration for the heater. However, the NO₂ peaks in the tight house are significantly less than in the typical house despite the reduced outdoor airflow into the house. In fact, the whole-house average NO₂ concentrations are lower in the tight house than in the typical house (0.025 ppm vs. 0.026 ppm for the oven source, and 0.003 ppm vs. 0.008 ppm for the heater source). These results may seem surprising as one might expect the reduced infiltration to result in higher NO₂ concentrations in the tight house. However, these results may be explained by the impact of NO, decay. The NO, in the house is either generated by the indoor sources or brought in from outside. During much of the day, when the combustion appliances are not operated, the outdoor air is the source of indoor NO, and, due to NO, decay, the indoor concentrations are lower than the outdoor concentration. Therefore, reducing the infiltration actually results in lower indoor NO, concentrations. When there is an indoor source of NO₂, a lower infiltration rate may still result in lower NO₂ concentrations in the zones without the source. However, the source-zone will have higher NO, concentrations when the infiltration rate is lower (the peak kitchen concentration from the oven is 1.686 ppm for the tight house and 1.434 ppm for the typical house). It is important to note that this result of lower NO₂ concentrations in tighter houses cannot be generalized to all cases. If the NO, decay rate was lower, the indoor NO, generation rate was higher, or the outdoor NO, concentration was lower, the tighter house could have higher concentrations. See Tables 1b and 4b of Appendix B for the peak and average NO₂ concentrations results for these simulations.

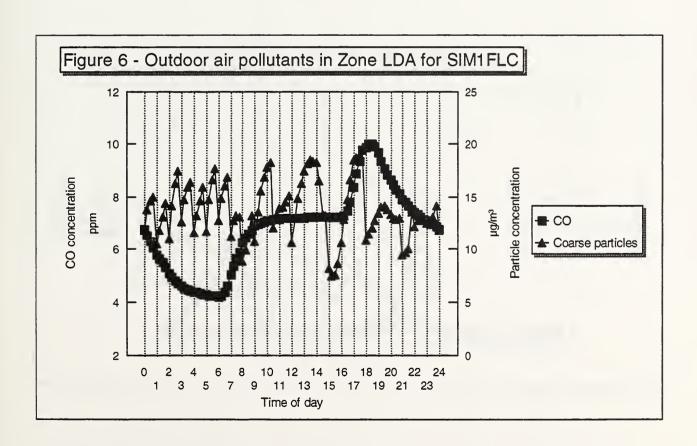
The TVOC concentrations in Zone LDA resulting from the burst source located in the LDA Zone (VOC4 in Tables 1 and 4 of Appendix B) are shown in Figures 5 and 9 for SIM1FLC and SIM1FTC. As expected, this source results in two daily peaks due to the source schedule and higher concentrations in the tight house due to the reduced airflow into the house.

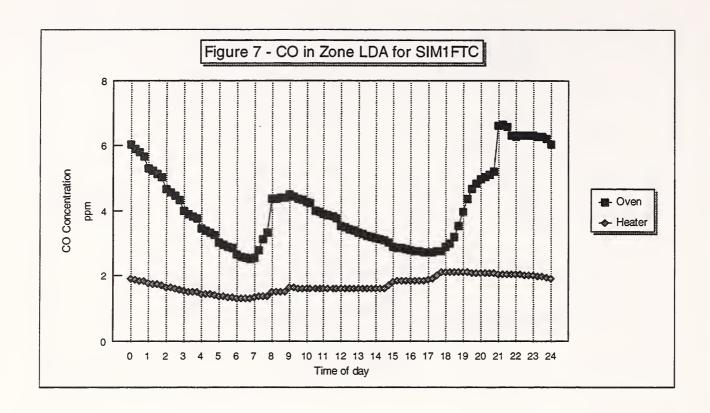
Figures 6 and 10 show the CO and coarse particle concentrations (CO.3 and PART.3 of Tables 1 and 4 in Appendix B) for SIM1FLC and SIM1FTC, respectively, due to the elevated outdoor pollutant concentrations of Table 8. The CO concentration in the typical house tracks the outdoor concentration with a time lag based on the building time constant (related to the inverse of the building air change rate). The particle concentration shows the effect of the HVAC system cycling which changes the air change rate of the house and filters particles from the air. When the furnace is on, the concentration of coarse particles decreases due to the impact of the furnace filter. The tight house results exhibit damped CO peaks and valleys due to the longer time constants. Because the particles come from outdoors, the lower air change rates result in lower particle concentrations.

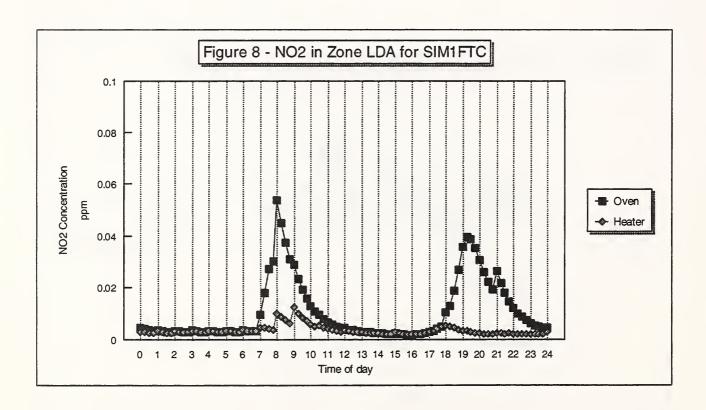


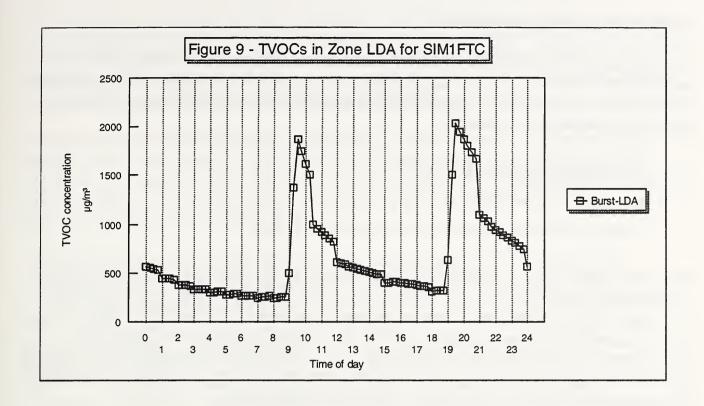


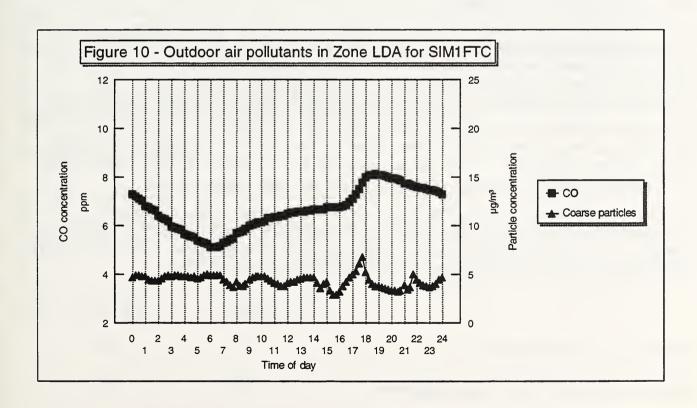












Indoor Air Quality Controls

This section describes the indoor air quality control technologies that will be evaluated in the study. These technologies will be incorporated into the baseline house models to determine their effectiveness in controlling the selected pollutant sources. The three technologies described in this section include the following:

Electrostatic particulate filtration

Heat recovery ventilation

Outdoor air intake damper on the forced-air system return

This section describes each of these technologies and includes revisions of the baseline house duct drawings. In addition, this section contains an estimate of the equipment and installation costs and a revision of the thermal load calculations based on the modifications. Finally, the impacts of each of these technologies on "other contaminants" are discussed. These other contaminants, as described in the original project work statement, include contaminants that have typically been of concern to designers of residential ventilation systems including cooking odors, tobacco smoke, moisture, outdoor pollen, outdoor odors, and ozone.

Electrostatic Particulate Filtration

The first IAQ control technology is increased particulate filtration through the installation of passive, electrostatic particulate filters. These filters were chosen based on the availability of performance data. In addition, the low pressure drop through these filters enables their installation without modification of the existing forced-air distribution system. The baseline houses are assumed to have standard furnace filters with an ASHRAE dust spot efficiency of less than 20% and an arrestance of 90%. These values are based on tests conducted in accordance with ASHRAE Standard 52.1 (37). The increased filtration is based on the use of electrostatic filters with an ASHRAE dust spot efficiency of 30% and an arrestance of 95%.

Although the efficiencies of particulate filters change over time as they become loaded, the computer simulations in this project will employ a constant filter efficiency. The efficiencies of the baseline and improved filters used in the simulations will be as follows:

| | Baseline | Control #1 |
|---|----------|------------|
| Particles <2.5 μm in diameter | 5% | 30% |
| Particles between 2.5 and 10 µm in diameter | 90% | 95% |

The improved filters are installed in place of the regular furnace filters. Their location is indicated in the revised duct drawings showing all of the IAQ control technologies, Figures 13 through 16.

The installation of the improved filters are assumed not to affect the thermal loads of the houses. Due to a higher pressure drop through the filters, they may cause a slight reduction in the airflow rate through the system, which could affect the pressures across the building envelope and the resultant building infiltration rates. However, this effect is expected to be small, and the thermal load calculations were not modified for this control technology.

The cost of this first control technology includes the cost of the filters themselves and their installation. For comparison, the furnace filters in the baseline houses are assumed to cost \$2 each and to be changed every month. Therefore, the annual cost of the baseline filters is \$24. The improved filters are assumed to cost \$15 each and to be changed every 2 months. Therefore, the annual cost of the improved filters is \$90.

The installation of improved filters will reduce the concentrations of the so-called "other contaminants" in the houses to the degree that the filtration of each contaminant is increased. The concentrations of particulate contaminants with outdoor sources (pollen) will be reduced due to the increased particulate filtration. The concentrations of VOCs associated with outdoor odors will not be decreased. The increased filtration will not affect indoor ozone levels due to outdoor sources, since ozone removal rates will be unaffected by the new filters. In addition, these electrostatic filters are not sources of ozone themselves. The concentrations of other contaminants with indoor sources will also be affected to the degree that the filtration of each contaminant is increased. The levels of cooking odors and tobacco smoke will be decreased based on the increased filter efficiency for both fine and coarse particulates. Indoor moisture levels will be unaffected by the new filters because the outdoor air change rates will not be affected and because the improved filters have no humidification or dehumidification impacts.

Electronic air cleaners are also of interest and may be investigated in follow-up work. The existence of reliable performance data is being investigated.

Heat Recovery Ventilator

The second IAQ control technology is the installation of a heat recovery ventilator (HRV) in conjunction with the forced-air distribution system. As seen in Figure 11, the device brings outdoor air into the building where it exchanges heat with an airstream leaving the return side of the forced air system. Under heating conditions, the outdoor air is warmed by the outgoing airstream, and under cooling the outdoor air is cooled. The outgoing airstream is exhausted to the outdoors after leaving the heat recovery ventilator. The airstream from outdoors flows into the return side of the forced-air system after leaving the HRV.

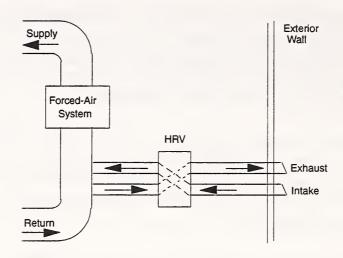


Figure 11 - Schematic of Heat Recovery Ventilator

The HRV specifications are based on a commercially-available model designed for residential use and installation in conjunction with forced-air systems. The airflow rate capacity of the device was selected to obtain an air change rate of at least 0.5 air changes per hour (ach) at full flow. The actual outdoor airflow rate during operation was selected to provide 0.35 ach through the HRV. The actual whole building air change rate will also include envelope infiltration, which in turn depends on the airtightness of the house, weather conditions and ventilation equipment operation. The HRV specifications for the four houses are as follows:

Miami, 2-story

Airflow capacity: 30 to 60 L/s (65 to 127 cfm), roughly 0.25 to 0.5 ach

Airflow rate during operation: 44 L/s (93 cfm)

Efficiency: 69% at 0 °C (32 °F), 60% at -25 °C (-13 °F)

Maximum power consumption: 115 W

No defrost

Miami, Ranch

Airflow capacity: 30 to 60 L/s (65 to 127 cfm), roughly 0.4 to 0.8 ach

Airflow rate during operation: 26 L/s (55 cfm)

Efficiency: 69% at 0 °C (32 °F), 60% at -25 °C (-13 °F)

Maximum power consumption: 115 W

No defrost

Minneapolis, 2-story

Airflow capacity: 55 to 95 L/s (115 to 200 cfm), roughly 0.3 to 0.5 ach

Airflow rate during operation: 66 L/s (140 cfm)

Efficiency: 68% at 0 °C (32 °F), 61% at -25 °C (-13 °F)

Maximum power consumption: 216 W

Defrost cycle

Minneapolis, Ranch

Airflow capacity: 30 to 70 L/s (65 to 150 cfm), roughly 0.2 to 0.5 ach

Airflow rate during operation: 52 L/s (110 cfm)

Efficiency: 76% at 0 °C (32 °F), 56% at -25 °C (-13 °F)

Maximum power consumption: 105 W

Defrost cycle

The defrost cycle involves closing the outdoor air dampers for 5 minutes when the outdoor temperature is below -5 °C (23 °F). For outdoor temperatures between -5 and -30 °C (23 and -22 °F), each 5-minute defrost cycle is followed by a 35 minute period of air exchange before the next defrost cycle. For outdoor temperatures below -30 °C (-22 °F), each 5-minute defrost cycle is followed by 20 minutes of air exchange.

The HRV can be operated in several different control modes. The operation of the device and the fan speed (high or low) can be controlled by a timer, manually by the occupant or by a dehumidistat.

The installation of the HRV in each of the four houses is indicated in the revised duct drawings in Figures 13 through 16.

The thermal loads of the houses are affected by the installation and operation of the HRV due to the increased outdoor air change rate of the house when the devices are in operation. The air change rate due to the HRV operation is assumed to be additive to the baseline infiltration rate of 0.75 ach assumed for the design thermal load calculations. The thermal loads are increased by only a fraction of the increased outdoor air change rate based on the heat exchange efficiencies of the devices. For an additional air change rate of 0.35 ach and the rated heat exchange efficiencies of the HRVs, the revised design thermal loads for the four houses are given below. The baseline design thermal loads are described in detail in the Phase I report (2).

| Baseline | With HRV |
|----------|--|
| 2.87 kW | $3.14 \mathrm{kW}$ |
| 6.43 kW | 6.60 kW |
| Baseline | With HRV |
| 1.83 kW | 1.99 kW |
| 5.76 kW | $5.88 \mathrm{kW}$ |
| יו די | 337°41 TID37 |
| | With HRV |
| 12.64 kW | 13.59 kW |
| 6.21 kW | 6.36 kW |
| Baseline | With HRV |
| | 9.86 kW |
| 4.89 kW | 4.97 kW |
| | 2.87 kW 6.43 kW Baseline 1.83 kW 5.76 kW Baseline 12.64 kW 6.21 kW Baseline 9.25 kW |

The cost of the HRVs includes the cost of the equipment and installation, the operating costs for the fans in the devices and the increased energy consumption due to the additional outdoor air change of the building. The cost of the equipment is \$500 for both of the Miami houses, \$600 for the Minneapolis ranch house and \$700 for the Minneapolis two-story house. These are list prices from the manufacturer of the HRV on which the specifications are based. The installation costs are more variable, based on the layout of the house and local labor rates, and they can range from \$200 to \$500. The cost of the energy consumed by the device and by the additional outdoor air change rate requires detailed thermal modeling of the building and system. As discussed in the Phase I report of the project, such modeling is beyond the scope of this project.

The installation of the HRV will impact the so-called "other contaminants" in the houses due to the increased outdoor air change rate. Due to the additional outdoor airflow into the houses, the concentrations of contaminants with outdoor sources (pollen, outdoor odors and ozone) will increase. For a simple, nonreactive and unfiltered contaminant, there will be an increased contaminant load equal to the outdoor concentration multiplied by the outdoor airflow rate. The impact of particulates will be reduced based on the efficiency of the filters in the HRV and of the furnace filter. The impact of outdoor ozone will be reduced somewhat by losses on the interior surfaces of the HRV ductwork. The concentrations of other contaminants with indoor sources (cooking odors and tobacco smoke) will be reduced based on the increased air change rate of the building. The impact of the additional ventilation on moisture will depend on the building location, indoor moisture sources, and season. Indoor humidity levels will be reduced when there are large indoor sources and low relative humidity outdoors, but will be increased when the outdoor humidity is higher than the indoor level. Detailed modeling of moisture transport is required to assess these impacts and is beyond the scope of the current project.

Outdoor Intake Duct

The third IAQ control technology is the installation of an outdoor air intake duct on the return side of the forced air distribution system. As seen in Figure 12, the system consists of an intake, a duct, a motorized damper, and a volume damper for adjusting the airflow rate, and is connected to the return side of the return duct. The maximum airflow rate capacity of the intake is 78 L/s (165 cfm), which corresponds to the following air change rates for the four houses:

Miami, 2-story: 0.62 ach Miami, Ranch: 1.05 ach

Minneapolis, 2-story: 0.41 ach Minneapolis, Ranch: 0.53 ach

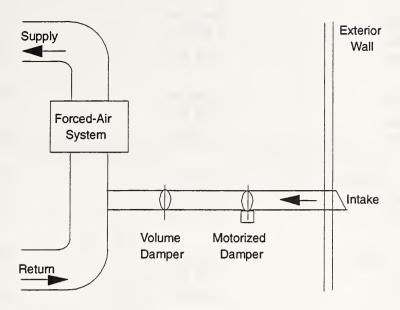


Figure 12 - Schematic of Outdoor Air Intake Duct

The actual airflow rate through the intake depends on the position of the volume damper, the overall airflow resistance of the intake system, and the pressure developed by the forced-air fan. In the computer simulations, it is assumed that the volume damper is adjusted such that the intake system provides 0.35 ach to the building when the furnace fan is in operation. This air change rate corresponds to the following outdoor air intake rates for the four buildings:

Miami, 2-story: 44 L/s (93 cfm) Miami, Ranch: 26 L/s (55 cfm)

Minneapolis, 2-story: 66 L/s (140 cfm) Minneapolis, Ranch: 52 L/s (110 cfm)

The motorized damper can be controlled in several different ways. It is generally interlocked with the forced-air system fan so that it opens only when the forced-air fan is operating. The motorized damper can also be controlled to open based on a timer, dehumidistat or pollutant (e.g. carbon monoxide or carbon dioxide) sensor.

The installation of the outdoor air intake duct in each of the four houses is indicated in the revised duct drawings in Figures 13 through 16.

The thermal loads of the houses are affected by the installation and operation of the outdoor air intake duct due to the increased outdoor air change rate of the house when the devices are in operation. The air change rate due to the HRV operation is assumed to be additive to the baseline infiltration rate of 0.75 ach assumed for the design thermal load calculations. Based on an additional air change rate of 0.35 ach and no heat exchange, the design thermal loads for the four houses are given below. The baseline thermal loads were described in detail in the Phase I report (2).

| Miami, 2-story | Baseline | With OAID |
|----------------------|----------|-----------|
| Heating | 2.87 kW | 3.54 kW |
| Cooling | 6.43 kW | 6.96 kW |
| Miami, Ranch | Baseline | With OAID |
| Heating | 1.83 kW | 2.23 kW |
| Cooling | 5.76 kW | 6.09 kW |
| Minneapolis, 2-story | Baseline | With OAID |
| Heating | 12.64 kW | 15.00 kW |
| Cooling | 6.21 kW | 6.71 kW |
| Minneapolis, Ranch | Baseline | With OAID |
| Heating | 9.25 kW | 10.73 kW |
| Cooling | 4.89 kW | 5.18 kW |

The cost of the outdoor air intake duct includes the cost of the equipment and installation and the increased energy consumption due to the additional outdoor air change of the building. The cost of the equipment, including the controls and the motorized dampers, is \$750 based on list prices from the manufacturer of the outdoor air intake duct on which the specifications are based. The installation costs are more variable, based on the layout of the house and local labor rates, and they can range from \$100 to \$300. The cost of the energy consumed by the device and by the additional outdoor air change rate requires detailed thermal modeling of the building and system. As discussed in the Phase I report of the project (2), such modeling is beyond the scope of this project.

The installation of the outdoor air intake duct will impact the so-called "other contaminants" in the houses. Due to the additional outdoor airflow into the houses, the concentrations of contaminants with outdoor sources (pollen, outdoor odors and ozone) will increase. For a simple, nonreactive and unfiltered contaminant, the impact will be an increased contaminant load equal to the outdoor concentration multiplied by the outdoor airflow rate. The impact of particulates will be lessened based on the removal efficiency of the furnace filter. The impact of ozone will be lessened by losses on the interior surfaces of the ductwork. The concentrations of other contaminants with indoor sources (cooking odors and tobacco smoke) will be reduced based on the increased air change rate of the building. As in the case of the HRV, the impact of the additional ventilation on moisture will depend on the building location, indoor moisture sources, and season.

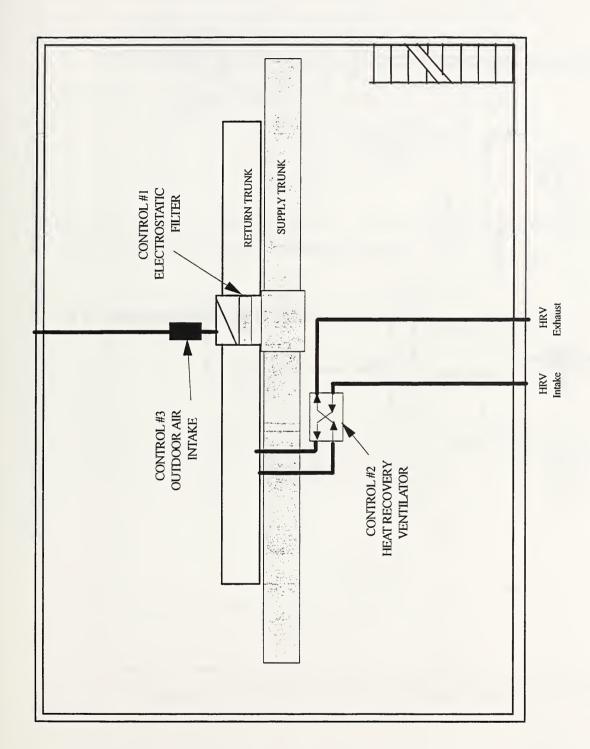


Figure 13 - IAQ Controls for Minneapolis Ranch House

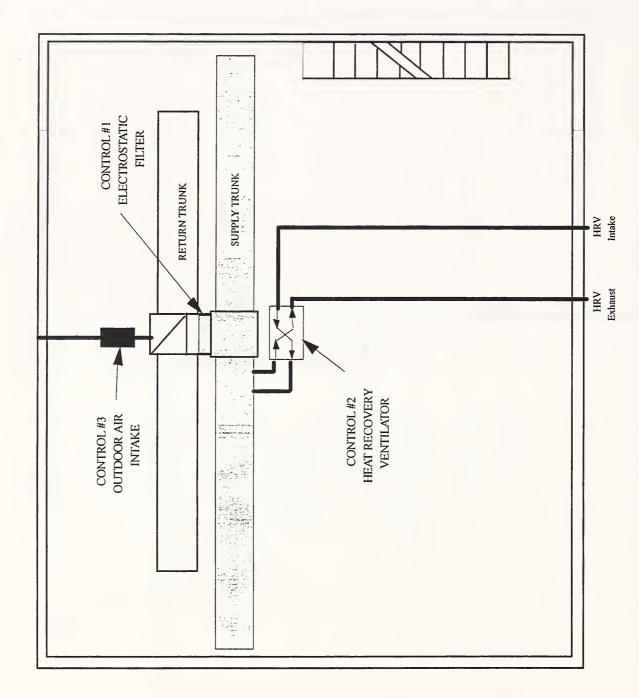
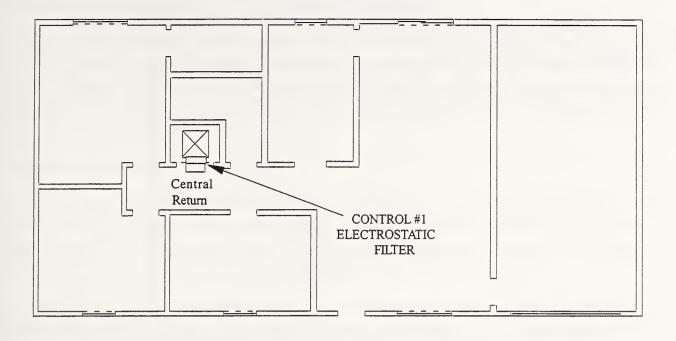


Figure 14 - IAQ Controls for Minneapolis 2-Story House



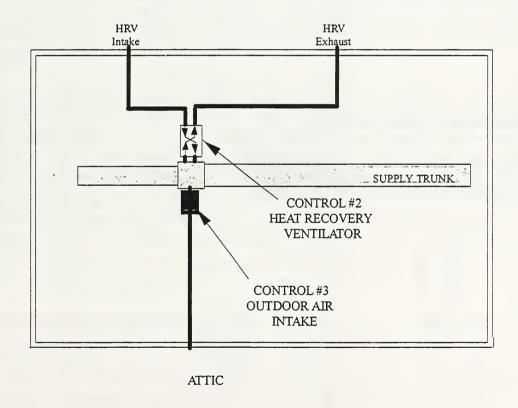


Figure 15 - IAQ Controls for Miami Ranch House

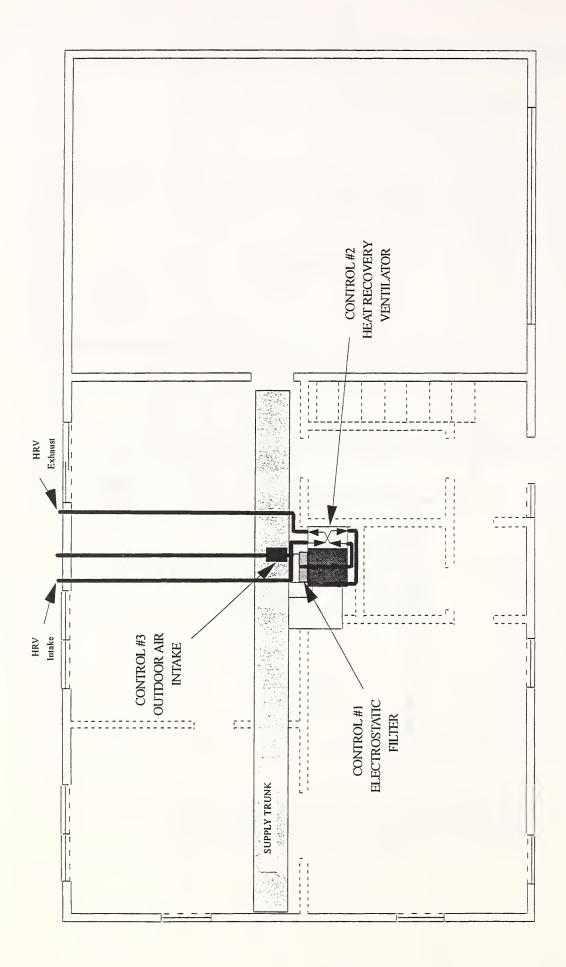


Figure 16 - IAQ controls for Miami 2-Story House

Preliminary Simulation of IAQ Control Retrofits

This section describes the preliminary simulations of the IAQ control retrofits. These simulations involved modifying selected baseline simulation cases with the IAQ control retrofits described above. The preliminary simulations were performed to verify the ability of the program to model the control technologies. In Phase II.B of the study, all of the baseline cases will be modified to incorporate each of the IAQ control retrofits.

IAQ Control Retrofits

The IAQ control retrofits selected for modeling in this study are an electrostatic particulate filter, a heat recovery ventilator, and an outdoor air intake damper installed on the forced-air system return. These three technologies were described in detail in the previous section. This section discusses only the details important to modeling them with CONTAM93 (1).

The electrostatic particulate filters selected for the study have a filter efficiency of 30% for fine particles (emitted by the combustion sources in these simulations) and 95% for coarse particles (associated with the elevated outdoor air concentrations). The filters will be modeled by replacing the standard furnace filters in the baseline HVAC systems with the electrostatic filters. The filter efficiency will be modeled as constant over time and impacts on airflow through the system will be neglected.

The second IAQ control retrofit is the installation of a heat recovery ventilator (HRV) in conjunction with the HVAC system. The HRV draws air from the return side of the forced-air system and replaces it with outdoor air drawn through the heat exchanger. The outdoor airflow rate supplied will be 44 L/s for the Miami 2-story house, 26 L/s for the Miami ranch house, 66 L/s for the Minneapolis 2-story house, and 52 L/s for the Minneapolis ranch house. The HRV will be modeled by setting the outdoor airflow rate for each HVAC system to the appropriate fraction of the total system supply airflow rate. Thus, the desired amount of outdoor air will be supplied whenever the HVAC system is operating. The HVAC systems will be operated on the same schedules determined for the baseline simulations based on thermal loads. Other possible control options (such as constant operation or demand control) will not be studied.

Other considerations in modeling the HRV include filtration of the incoming outdoor air and the HRV defrost cycle. A standard furnace filter (with efficiencies of 5% for fine particles and 90% for coarse particles) will be included in the outdoor air intake path of the HRV. The HRV employs a defrost cycle in cold weather which involves periodically closing the outdoor air damper. However, operation of the defrost cycle will be neglected in the simulations.

The third IAQ control retrofit is the installation of an outdoor air intake duct on the return side of the HVAC system, which draws outdoor air into the return side of the forced-air system whenever it is operating. This retrofit will be modeled similar to the HRV. The baseline HVAC system will be modified to include a constant fraction of outdoor air whenever the HVAC system is operating. The outdoor air supply airflow rates will be the same as listed above for the HRV, and a standard furnace filter will be included in the outdoor air intake path. The primary

difference between the outdoor air intake damper and the HRV is that the outdoor air intake damper does not include an exhaust duct. Therefore, the outdoor airflow will tend to pressurize the house. This effect will be modeled by reducing the HVAC return flows by an amount equal to the outdoor air supplied to the system.

Results of Preliminary Simulation of IAQ Control Retrofits

The baseline case selected for modification with the IAQ control retrofits was SIM1FLC, the Miami ranch house with typical airtightness in cold weather. The simulations with the electrostatic particulate filtration, the HRV, and the outdoor air intake damper are referred to as SIM1FLCF, SIM1FLCH, and SIM1FLCO, respectively.

The results of each simulation includes pollutant concentrations for up to 18 pollutants in each of the building zones for each 15 minute time step of the 24 hour simulation period. As was the case for the baseline simulations, the complete transient simulation results are not presented here but are available in spreadsheet files. Figures 17 through 20 show examples of the transient pollutant concentrations and Tables 25a through 27e of Appendix B present a complete summary of peak and 24-hour, 4-hour, and 1-hour average concentrations for the preliminary IAQ control retrofit simulations as described for the baseline simulations.

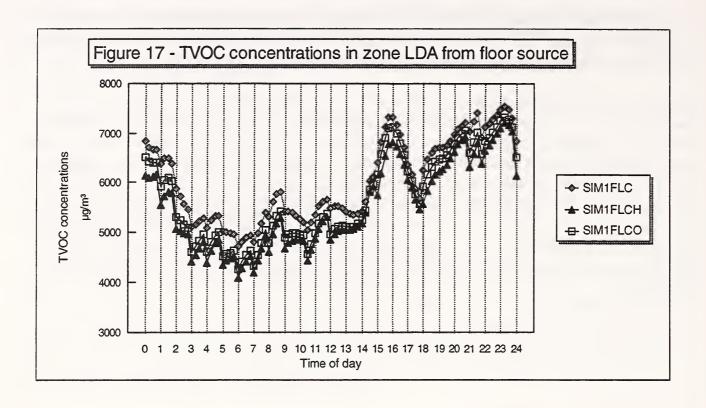
Figure 17 shows total volatile organic compound (TVOC) concentrations in Zone LDA resulting from the constant floor source (VOC2 of Tables 1, 26, and 27 of Appendix B) for SIM1FLC, SIM1FLCH, and SIM1FLCO. Since SIM1FLCF differs from SIM1FLC by improved particle filtration efficiency, all VOC concentrations in SIM1FLCF are identical to SIM1FLC and are not shown. Both outdoor air intake devices result in modest reductions in the TVOC concentrations in the zone, with the HRV having a slightly greater effect. The HRV may have a greater effect because it has a neutral effect on indoor pressure (compared to the outdoor air intake damper which pressurizes the building) resulting in a greater average air change rate. The 24-hour average TVOC concentration in Zone LDA is 6040 μ g/m³, 5545 μ g/m³, and 5720 μ g/m³ for SIM1FLCH, and SIM1FLCO, respectively (see Tables 1c, 26c, and 27c of Appendix B).

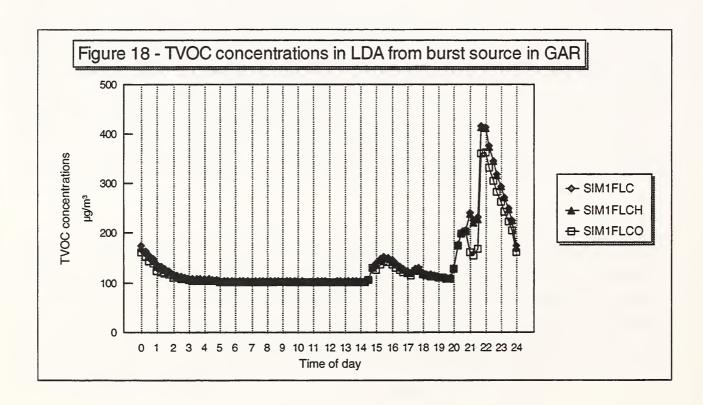
Figure 18 shows TVOC concentrations in Zone LDA resulting from a burst VOC source in the garage (VOC5 of Tables 1, 26, and 27 of Appendix B). The VOC concentrations for SIM1FLC and SIM1FLCH are nearly identical while the concentrations for SIM1FLCO are somewhat lower. The 24 hour average TVOC concentration in Zone LDA for this source is 141 μ g/m³, 140 μ g/m³, and 132 μ g/m³ for SIM1FLC, SIM1FLCH, and SIM1FLCO, respectively (see Tables 1c, 26c, and 27c of Appendix B). The slightly reduced concentrations for SIM1FLCO is due to the effect of the outdoor air pressurizing the interior of the house which reduces the transport of the contaminant from the garage.

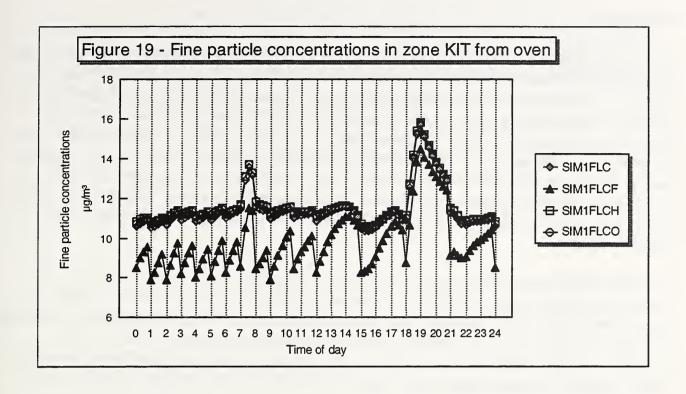
Figure 19 shows fine particle concentrations in the kitchen resulting from the oven source (PART.1 of Tables 1, 25, 26, and 27 of Appendix B). The improved filtration in case SIM1FLCF resulted in lower concentrations while the outdoor air intake devices had very little impact, possibly because the outdoor air particle concentration of 13 µg/m³ is close to the 24 hour

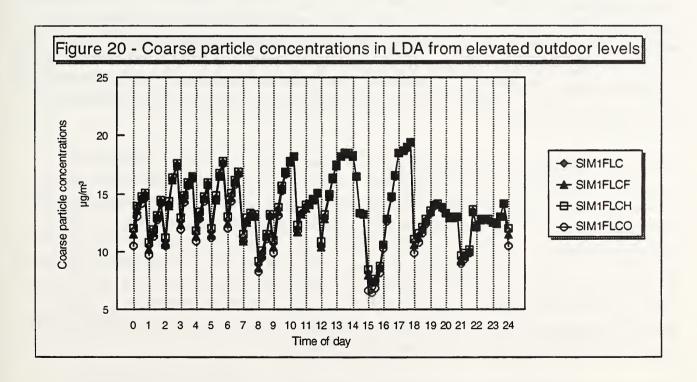
average baseline concentration. The 24 hour average fine particle concentration in Zone KIT is $11.4 \,\mu\text{g/m}^3$, $9.8 \,\mu\text{g/m}^3$, $11.6 \,\mu\text{g/m}^3$, and $11.6 \,\mu\text{g/m}^3$ for SIM1FLC, SIM1FLCF, SIM1FLCH, and SIM1FLCO, respectively (see Tables 1c, 25c, 26c, and 27c of Appendix B).

Figure 20 shows coarse particle concentrations in Zone LDA resulting from elevated outdoor levels (PART.3 of Tables 1, 25, 26, and 27 of Appendix B). None of the IAQ control retrofits resulted in a significant impact on the coarse particle concentrations. The 24 hour average coarse particle concentration in Zone LDA is 13.7 μg/m³, 13.6 μg/m³, 13.8 μg/m³, and 13.5 μg/m³ for SIM1FLCF, SIM1FLCH, and SIM1FLCO, respectively (see Tables 1c, 25c, 26c, and 27c of Appendix B). Possible explanations for the small changes include the relatively small increase in filtration efficiency for the electrostatic particulate filter (from 90% to 95%) and the inclusion of a standard filter in the outdoor air intake path for both the HRV and the outdoor air intake damper. The outdoor air intake filter limits the number of particles brought in with the outdoor air.









Summary

The National Institute of Standards and Technology (NIST) has completed Phase II.A of a project for the U.S. Consumer Product Safety Commission (CPSC) to study the impact of HVAC systems on residential indoor air quality and to assess the potential for using residential forced-air systems to control indoor pollutant levels. In this effort, NIST is performing whole building airflow and contaminant dispersal computer simulations with the program CONTAM93 to assess the ability of modifications of central forced-air heating and cooling systems to control pollutant sources relevant to the residential environment. During Phase II.A of this project, three major efforts were completed: baseline simulations of contaminant levels without IAQ controls, design of the IAQ control retrofits, and preliminary simulations of contaminant levels with the IAQ control retrofits.

It is important to note that the project is essentially a scoping study to conduct a preliminary assessment, using computer simulation, of the potential for using forced-air HVAC systems to improve residential IAQ. The project results are also limited by the lack of high quality input data for some simulation inputs and the lack of a thorough empirical evaluation of the model's predictive capability. Despite these limitations, the project is expected to identify key issues for further analysis and experimental work to meet the overall goal of cost-effective IAQ control in residential buildings.

This report described the input data used to model the baseline houses with CONTAM93 including the configuration of the building zones, the air leakage of the building envelopes and of interior partitions, wind pressure profile on the building envelope, pollutant source strengths and temporal profiles, heating and cooling system flows, furnace filter efficiency, pollutant sinks, pollutant decay or deposition, and ambient weather and pollutant concentrations. The results of the baseline simulations including transient pollutant concentrations for selected simulations and a summary of peak and average concentrations for all baseline simulations were also presented. It should be noted that the results for any one simulation may be counter-intuitive and should not be generalized to all cases.

Three indoor air quality control technologies were then selected for incorporation into the baseline house models to determine their effectiveness in controlling the modeled pollutant sources. The technologies selected include the following: an electrostatic particulate filter with efficiencies of 30% for fine particles and 95% for coarse particles, a heat recovery ventilator (HRV) providing an actual outdoor airflow of 0.35 ach, and an outdoor air intake damper on the forced-air system return also providing an actual outdoor airflow of 0.35 ach. The annual cost of the filters was estimated at \$90. The estimated installation and equipment costs of the HRV and of the outdoor air intake duct were \$700 to \$1200 and \$850 to \$1050, respectively. Detailed thermal modeling of the building and system would be required to determine the annual energy costs of these devices and is beyond the scope of this project.

Selected baseline cases were then modified to implement these IAQ control retrofits and preliminary simulations were performed to verify the ability of the program to model the control technologies. The results for the IAQ control retrofits are presented as examples only and are not

intended to be used to evaluate the effectiveness of the controls. In Phase II.B of the study, all of the baseline cases will be modified to incorporate each of the IAQ control retrofits. The Phase II.B simulation results will be compared to the baseline simulation results to determine the effectiveness of the IAQ control technologies at reducing contaminant levels in single-family residential buildings.

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Appendix A Airflow Modeling Results

CONTAM93 was used to analyze airflow in the houses using two approaches: simulated fan pressurization tests and directly calculated whole building air change rates under a range of wind speed and indoor - outdoor temperature differences.

Fan pressurization tests in the houses were simulated with CONTAM93 by including a constant flow element in the door of each house and adjusting the flow until a pressure differences of 4 and 50 Pa was achieved. The airflow rates at 50 Pa were divided by the interior volumes of the houses to determine the 50 Pa air change rates, and the 4 Pa flows were converted to effective leakage areas using Equation 27 in Chapter 23 of ASHRAE (3). The results of the fan pressurization simulations are shown in Table 1. The difference between the Miami and Minneapolis houses is due primarily to the existence of the basement in the Minneapolis houses. In terms of both measures of airtightness, the tight houses are about 66% tighter than the houses of typical leakage.

Table 1 - Fan pressurization simulation results

| House | ach ₅₀ (hr ⁻¹) | Leakage area (cm²) |
|-----------------------------|--|--------------------|
| Typical Miami ranch | 13.2 | 680 |
| Tight Miami ranch | 4.1 | 220 |
| Typical Minneapolis ranch | 6.6 | 720 |
| Tight Minneapolis ranch | 2.2 | 230 |
| Typical Miami 2 story | 12.9 | 1,120 |
| Tight Miami 2 story | 4.6 | 390 |
| Typical Minneapolis 2 story | 8.8 | 1,170 |
| Tight Minneapolis 2 story | 3.1 | 410 |

CONTAM93 was used to calculate whole building air change rates for wind speeds from 0 to 10 m/s and indoor-outdoor temperature differences from -10 to 30 °C. The wind direction was held constant throughout the simulations. These simulations were performed with the HVAC systems both on and off. Whole building air change rates were calculated by adding the airflow entering the conditioned space of the house through all leakage paths. The results of these airflow simulations are shown in Tables 2 through 9 for the system off.

Several general trends are shown by these tables. Using 'tight' values for the airflow elements vs. 'typical' or best estimate values reduced the whole building air change rate by up to a factor of four as compared to a factor of three for the fan pressurization results. Also, over the range considered here, the wind speed had a much greater impact on the whole building air change rate than the temperature difference. However, the tight airflow elements reduced the impact of the wind speed more than the impact of the temperature difference.

Table 2 - Whole house air change rate for typical Miamiranch house (ach)

| Tin - Tout (K) | - 10 | -5 | 0 | 5 | 10 | 15 | 20 | 25 | 30 |
|------------------|-------|------|------|------|------|------|------|------|------|
| Wind speed (m/s) | | | | | | | | | |
| 0 | 0.33 | 0.21 | 0.00 | 0.22 | 0.35 | 0.46 | 0.57 | 0.67 | 0.76 |
| 2 | 0.40 | 0.32 | 0.33 | 0.38 | 0.47 | 0.54 | 0.65 | 0.74 | 0.84 |
| 4 | 0.75 | 0.78 | 0.82 | 0.85 | 0.89 | 0.94 | 1.00 | 1.08 | 1.15 |
| 6 | 1.3 1 | 1.34 | 1.38 | 1.42 | 1.46 | 1.50 | 1.54 | 1.61 | 1.67 |
| 8 | 1.92 | 1.96 | 2.01 | 2.06 | 2.11 | 2.16 | 2.21 | 2.27 | 2.33 |
| 10 | 2.57 | 2.63 | 2.69 | 2.75 | 2.81 | 2.87 | 2.94 | 3.01 | 3.08 |

Table 3 - Whole house air change rate for tight Miamiranch house (ach)

| | | | | | | | • | | |
|------------------|------|------|------|-----------|------|------|------|------|------|
| Tin - Tout (K) | - 10 | -5 | 0 | 5 | 10 | 15 | 20 | 25 | 30 |
| Wind speed (m/s) | | | | - · · - · | | | | | |
| 0 | 0.10 | 0.07 | 0.00 | 0.07 | 0.11 | 0.14 | 0.17 | 0.20 | 0.23 |
| 2 | 0.11 | 0.09 | 0.08 | 0.10 | 0.14 | 0.17 | 0.20 | 0.23 | 0.26 |
| 4 | 0.18 | 0.18 | 0.19 | 0.21 | 0.22 | 0.24 | 0.26 | 0.28 | 0.31 |
| 6 | 0.30 | 0.31 | 0.32 | 0.33 | 0.34 | 0.36 | 0.38 | 0.39 | 0.42 |
| 8 | 0.44 | 0.46 | 0.47 | 0.48 | 0.49 | 0.51 | 0.53 | 0.54 | 0.57 |
| 10 | 0.60 | 0.61 | 0.63 | 0.64 | 0.65 | 0.67 | 0.69 | 0.71 | 0.73 |

Table 4 - Whole house air change rate for typical Minneapolis ranch house (ach)

| | | | | | | A | | ` | |
|------------------|------|------|------|------|------|------|------|------|------|
| Tin - Tout (K) | - 10 | -5 | 0 | 5 | 10 | 15 | 20 | 25 | 30 |
| Wind speed (m/s) | | | | | | | | | |
| 0 | 0.25 | 0.16 | 0.00 | 0.16 | 0.26 | 0.34 | 0.42 | 0.49 | 0.56 |
| 2 | 0.29 | 0.23 | 0.18 | 0.23 | 0.31 | 0.39 | 0.46 | 0.53 | 0.59 |
| 4 | 0.45 | 0.41 | 0.44 | 0.47 | 0.50 | 0.54 | 0.59 | 0.64 | 0.69 |
| 6 | 0.69 | 0.72 | 0.75 | 0.78 | 0.81 | 0.83 | 0.87 | 0.91 | 0.95 |
| 8 | 1.03 | 1.06 | 1.09 | 1.12 | 1.16 | 1.19 | 1.22 | 1.26 | 1.29 |
| 10 | 1.39 | 1.43 | 1.46 | 1.50 | 1.54 | 1.57 | 1.62 | 1.66 | 1.70 |

Table 5 - Whole house air change rate for tight Minneapolis ranch house (ach)

| Tin - Tout (K) | - 10 | -5 | 0 | 5 | 10 | 15 | 20 | 25 | 30 |
|------------------|------|------|------|------|------|------|------|------|------|
| Wind speed (m/s) | | | | | | | | | |
| 0 | 0.09 | 0.06 | 0.00 | 0.06 | 0.10 | 0.13 | 0.16 | 0.19 | 0.21 |
| 2 | 0.09 | 0.07 | 0.04 | 0.07 | 0.11 | 0.14 | 0.17 | 0.20 | 0.22 |
| 4 | 0.13 | 0.10 | 0.11 | 0.12 | 0.14 | 0.16 | 0.19 | 0.21 | 0.24 |
| 6 | 0.17 | 0.18 | 0.19 | 0.19 | 0.21 | 0.22 | 0.23 | 0.25 | 0.27 |
| 8 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 | 0.30 | 0.31 | 0.33 | 0.34 |
| 10 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 | 0.39 | 0.41 | 0.42 | 0.44 |

Table 6 - Whole house air change rate for typical Miami 2 story house (ach)

| Tin - Tout (K) | - 10 | - 5 | 0 | 5 | 10 | 15 | 20 | 25 | 30 |
|------------------|------|------------|-------|------|------|------|------|------|-------|
| Wind speed (m/s) | | | | | | | | | |
| 0 | 0.38 | 0.24 | 0.00 | 0.25 | 0.40 | 0.53 | 0.64 | 0.76 | 0.87 |
| 2 | 0.44 | 0.34 | 0.36 | 0.42 | 0.51 | 0.62 | 0.72 | 0.81 | 0.91 |
| 4 | 0.82 | 0.86 | 0.89 | 0.93 | 0.96 | 1.02 | 1.08 | 1.15 | 1.2 1 |
| 6 | 1.43 | 1.47 | 1.5 1 | 1.55 | 1.60 | 1.64 | 1.68 | 1.74 | 1.80 |
| 8 | 2.10 | 2.15 | 2.20 | 2.25 | 2.30 | 2.36 | 2.41 | 2.47 | 2.53 |
| 10 | 2.82 | 2.88 | 2.94 | 3.01 | 3.07 | 3.14 | 3.21 | 3.28 | 3.35 |

Table 7 - Whole house air change rate for tight Miami 2 story house (ach)

| Tin - Tout (K) | - 10 | -5 | 0 | 5 | 10 | 15 | 20 | 25 | 30 |
|------------------|------|------|------|------|------|------|------|------|------|
| Wind speed (m/s) | | | | | | | | | |
| 0 | 0.13 | 0.08 | 0.00 | 0.09 | 0.14 | 0.18 | 0.22 | 0.26 | 0.30 |
| 2 | 0.14 | 0.10 | 0.09 | 0.12 | 0.16 | 0.21 | 0.25 | 0.28 | 0.32 |
| 4 | 0.20 | 0.22 | 0.23 | 0.24 | 0.26 | 0.28 | 0.30 | 0.34 | 0.38 |
| 6 | 0.36 | 0.37 | 0.38 | 0.40 | 0.41 | 0.43 | 0.44 | 0.47 | 0.49 |
| 8 | 0.53 | 0.54 | 0.56 | 0.57 | 0.59 | 0.60 | 0.62 | 0.64 | 0.66 |
| 10 | 0.71 | 0.73 | 0.75 | 0.76 | 0.78 | 0.80 | 0.82 | 0.84 | 0.86 |

Table 8 - Whole house air change rate for typical Minneapolis 2 story house (ach)

| Tin - Tout (K) | - 10 | - 5 | 0 | 5 | 10 | 15 | 20 | 25 | 30 |
|------------------|------|------------|------|------|------|------|------|-------|------|
| Wind speed (m/s) | | | | | | | | | |
| 0 | 0.25 | 0.15 | 0.00 | 0.17 | 0.27 | 0.35 | 0.43 | 0.50 | 0.58 |
| 2 | 0.30 | 0.24 | 0.25 | 0.28 | 0.34 | 0.42 | 0.48 | 0.54 | 0.61 |
| 4 | 0.57 | 0.60 | 0.62 | 0.64 | 0.66 | 0.70 | 0.74 | 0.78 | 0.83 |
| 6 | 0.99 | 1.02 | 1.05 | 1.08 | 1.10 | 1.13 | 1.16 | 1.20 | 1.24 |
| 8 | 1.46 | 1.49 | 1.52 | 1.56 | 1.60 | 1.63 | 1.67 | 1.7 1 | 1.75 |
| 10 | 1.95 | 2.00 | 2.04 | 2.08 | 2.12 | 2.17 | 2.22 | 2.27 | 2.32 |

Table 9 - Whole house air change rate for tight Minneapolis 2 story house (ach)

| Tin - Tout (K) | -10 | -5 | 0 | 5 | 10 | 15 | 20 | 25 | 30 |
|------------------|------|------|------|------|------|------|------|------|------|
| Wind speed (m/s) | | | | | | | - | | |
| 0 | 0.09 | 0.06 | 0.00 | 0.06 | 0.09 | 0.12 | 0.15 | 0.18 | 0.20 |
| 2 | 0.10 | 0.07 | 0.06 | 0.08 | 0.11 | 0.14 | 0.17 | 0.19 | 0.21 |
| 4 | 0.14 | 0.15 | 0.16 | 0.17 | 0.18 | 0.19 | 0.21 | 0.23 | 0.26 |
| 6 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 | 0.30 | 0.31 | 0.33 | 0.34 |
| 8 | 0.37 | 0.38 | 0.39 | 0.40 | 0.41 | 0.42 | 0.44 | 0.45 | 0.47 |
| 10 | 0.50 | 0.51 | 0.53 | 0.54 | 0.55 | 0.56 | 0.58 | 0.59 | 0.61 |

Tables 10 through 17 present the results of the airflow simulations with the HVAC system on. Operation of the HVAC system increased the building air change rate as much as 0.31 ach at zero wind speed and temperature difference due to supply duct leakage in the attic. The effect of the system fan was less than 0.07 ach at high wind speeds (> 4 m/s) and temperature differences (> 10 °C).

Table 10 - Whole house air change rate for typical Miami ranch house with system on (ach)

| Tin - Tout (K) | -10 | -5 | 0 | 5 | 10 | 15 | 20 | 25 | 30 |
|------------------|------|------|------|------|------|------|------|------|------|
| Wind speed (m/s) | | | | | | | | - | |
| 0 | 0.45 | 0.38 | 0.31 | 0.39 | 0.52 | 0.63 | 0.73 | 0.83 | 0.93 |
| 2 | 0.59 | 0.52 | 0.41 | 0.50 | 0.63 | 0.74 | 0.84 | 0.93 | 1.03 |
| 4 | 0.86 | 0.81 | 0.85 | 0.89 | 0.95 | 102 | 1.10 | 1.17 | 1.24 |
| 6 | 1.34 | 1.37 | 141 | 145 | 149 | 1.55 | 161 | 1.67 | 173 |
| 8 | 1.95 | 199 | 2.04 | 2.09 | 2.14 | 2.19 | 2.25 | 2.30 | 2.38 |
| 10 | 2.60 | 2.66 | 2.72 | 2.78 | 2.84 | 2.91 | 2.97 | 3.04 | 3.11 |

Table 11- Whole house air change rate for tight Miami ranch house with system on (ach)

| Tin - Tout (K) | -10 | -5 | 0 | 5 | 10 | 15 | 20 | 25 | 30 |
|------------------|------|------|------|------|------|------|------|------|------|
| Wind speed (m/s) | | | | | | | | | |
| 0 | 0.29 | 0.29 | 0.30 | 0.30 | 0.30 | 0.31 | 0.31 | 0.33 | 0.37 |
| 2 | 0.30 | 0.30 | 0.30 | 0.30 | 0.30 | 0.31 | 0.32 | 0.36 | 0.39 |
| 4 | 0.37 | 0.36 | 0.34 | 0.33 | 0.31 | 0.32 | 0.36 | 0.41 | 0.44 |
| 6 | 0.46 | 0.45 | 0.44 | 0.43 | 0.41 | 0.40 | 0.42 | 0.46 | 0.49 |
| 8 | 0.56 | 0.55 | 0.53 | 0.52 | 0.53 | 0.55 | 0.57 | 0.58 | 0.61 |
| 10 | 0.65 | 0.64 | 0.64 | 0.66 | 0.69 | 0.71 | 0.73 | 0.75 | 0.77 |

Table 12 - Whole house air change rate for typical Minneapolis ranch house with system on (ach)

| Table II Whole I | COUC WI | omango i | | P | | | | | 011 (4411) |
|------------------|---------|----------|------|------|------|------|------|------|------------|
| Tin - Tout (K) | -10 | -5 | 0 | 5 | 10 | 15 | 20 | 25 | 30 |
| Wind speed (m/s) | | | | | | | | | |
| 0 | 0.24 | 0.16 | 0.00 | 0.15 | 0.25 | 0.33 | 0.41 | 0.48 | 0.55 |
| 2 | 0.28 | 0.22 | 0.18 | 0.22 | 0.30 | 0.38 | 0.45 | 0.52 | 0.58 |
| 4 | 0.44 | 0.41 | 0.44 | 0.47 | 0.50 | 0.53 | 0.59 | 0.64 | 0.68 |
| 6 | 0.69 | 0.72 | 0.75 | 0.78 | 0.80 | 0.83 | 0.87 | 0.91 | 0.94 |
| 8 | 1.03 | 1.06 | 1.09 | 1.12 | 1.16 | 1.19 | 1.22 | 1.26 | 1.29 |
| 10 | 1.39 | 1.42 | 1.46 | 1.50 | 1.53 | 1.57 | 1.61 | 1.65 | 1.70 |

Table 13 - Whole house air change rate for tight Minneapolis ranch house with system on (ach)

| Tin - Tout (K) | -10 | -5 | 0 | 5 | 10 | 15 | 20 | 25 | 30 |
|------------------|------|------|------|------|------|------|------|------|------|
| Wind speed (m/s) | | | | - | | | | | |
| 0 | 0.09 | 0.05 | 0.00 | 0.05 | 0.09 | 0.12 | 0.15 | 0.18 | 0.21 |
| 2 | 0.08 | 0.06 | 0.04 | 0.06 | 0.10 | 0.13 | 0.16 | 0.19 | 0.21 |
| 4 | 0.12 | 0.10 | 0.11 | 0.12 | 0.13 | 0.15 | 0.18 | 0.21 | 0.23 |
| 6 | 0.17 | 0.18 | 0.18 | 0.19 | 0.20 | 0.22 | 0.23 | 0.25 | 0.26 |
| 8 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 | 0.30 | 0.31 | 0.32 | 0.34 |
| 10 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 | 0.39 | 0.40 | 0.42 | 0.43 |

Table 14 - Whole house air change rate for typical Miami 2 story house with system on (ach)

| Tm - Tout (K) | -10 | -5 | 0 | 5 | 10 | 15 | 20 | 25 | 30 |
|------------------|------|------|------|------|------|------|------|------|------|
| Wind speed (m/s) | | | | | | | | | |
| 0 | 0.38 | 0.24 | 0.00 | 0.25 | 0.40 | 0.53 | 0.64 | 0.76 | 0.87 |
| 2 | 0.44 | 0.34 | 0.36 | 0.42 | 0.51 | 0.62 | 0.72 | 0.81 | 0.91 |
| 4 | 0.82 | 0.86 | 0.89 | 0.93 | 0.96 | 102 | 108 | 1.15 | 1.21 |
| 6 | 143 | 147 | 1.52 | 156 | 160 | 164 | 168 | 174 | 180 |
| 8 | 2.10 | 2.15 | 2.20 | 2.25 | 2.31 | 2.36 | 2.41 | 2.47 | 2.53 |
| 10 | 2.82 | 2.88 | 2.94 | 3.00 | 3.07 | 3.14 | 3.21 | 3.28 | 3.35 |

Table 15 - Whole house air change rate for tight Miami 2 story house with system on (ach)

| 30 |
|------|
| |
| |
| 0.30 |
| 0.32 |
| 0.38 |
| 0.49 |
| 0.66 |
| 0.87 |
| ((|

Table 16 - Whole house air change rate for typical Minneapolis 2 story house with system on (ach)

| | | | | • | | | | | |
|------------------|------|------|------|------|------|------|------|------|------|
| Tin - Tout (K) | -10 | -5 | 0 | 5 | 10 | 15 | 20 | 25 | 30 |
| Wind speed (m/s) | | | | | | | | | |
| 0 | 0.25 | 0.16 | 0.01 | 0.17 | 0.27 | 0.35 | 0.43 | 0.51 | 0.58 |
| 2 | 0.31 | 0.24 | 0.25 | 0.29 | 0.35 | 0.42 | 0.48 | 0.55 | 0.61 |
| 4 | 0.57 | 0.60 | 0.62 | 0.64 | 0.66 | 0.70 | 0.74 | 0.79 | 0.83 |
| 6 | 0.99 | 102 | 105 | 108 | 1.11 | 1.13 | 1.16 | 1.20 | 124 |
| 8 | 146 | 149 | 1.53 | 156 | 160 | 163 | 167 | 171 | 175 |
| 10 | 195 | 2.00 | 2.04 | 2.08 | 2.13 | 2.17 | 2.22 | 2.27 | 2.32 |

Table 17 - Whole house air change rate for tight Minneapolis 2 story house with system on (ach)

| Tin - Tout (K) | -10 | -5 | 0 | 5 | 10 | 15 | 20 | 25 | 30 |
|------------------|------|------|------|------|------|------|------|------|------|
| Wind speed (m/s) | | | | | | | | | |
| 0 | 0.09 | 0.06 | 0.00 | 0.06 | 0.09 | 0.12 | 0.15 | 0.18 | 0.20 |
| 2 | 0.10 | 0.07 | 0.06 | 0.08 | 0.11 | 0.14 | 0.17 | 0.19 | 0.21 |
| 4 | 0.15 | 0.15 | 0.16 | 0.17 | 0.18 | 0.19 | 0.21 | 0.23 | 0.26 |
| 6 | 0.26 | 0.26 | 0.27 | 0.28 | 0.29 | 0.30 | 0.31 | 0.33 | 0.34 |
| 8 | 0.38 | 0.38 | 0.39 | 0.40 | 0.41 | 0.42 | 0.44 | 0.45 | 0.47 |
| 10 | 0.50 | 0.51 | 0.53 | 0.54 | 0.55 | 0.56 | 0.58 | 0.59 | 0.61 |

Appendix B Baseline and Preliminary Simulation Results

Tables 1a through 24e of Appendix B summarize the results of all 24 baseline simulations. Tables 25a through 27e summarize the results of the 3 preliminary simulations of the IAQ control retrofits. Tables 1a through 27a show the overall peak concentrations (excluding the basement, attic, garage and closet zones), the location of that overall peak, and the whole house 24-hour average concentrations (excluding the basement, garage, and attic zones). Tables 1b through 27b show the individual zone peak concentrations for the main living space zones. Tables 1c through 27c show the individual zone 24-hour average concentrations. Tables 1d through 27d show the individual zone 4-hour average concentrations. The 4-hour average was calculated for the VOC burst sources from 7 p.m. to 11 p.m., for the oven from 6 p.m. to 10 p.m., and for the heater from 7 am to 11 am. No 4-hour average was calculated for either the floor VOC source or the outdoor air pollutants. Tables 1e through 27e show the individual zone 1-hour average CO concentrations. The 1-hour average was calculated for the oven from 7 p.m. to 8 p.m. and for the heater from 9 am to 10 am.

| | PART.3 | (µg/m³) | 14.63 | | | PART.3 | (µg/m³) | 8.89 | 22.93 | 16.59 | 26.34 | 23.95 | 19.44 | 33.43 | 35.53 |
|---|--------|----------------------|-----------|--|---|--------|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|
| | NO2.3 | (PPM) | 0.079 | | | NO2.3 | (PPM) | 0.104 | 0.165 | 0.107 | 0.166 | 0.140 | 0.132 | 0.191 | 0.210 |
| | CO.3 | (PPM) | 6.77 | | | CO.3 | (PPM) | 9.48 | 9.84 | 9.65 | 10.15 | 10.00 | 10.03 | 10.35 | 10.34 |
| | PART.2 | (μg/m³) | 10.75 | | | PART.2 | (µg/m³) | 10.40 | 11.47 | 10.41 | 11.86 | 11.57 | 11.18 | 12.14 | 12.14 |
| | N02.2 | mdd | 0.008 | | | N02.2 | (PPM) | 0.010 | 0.017 | 0.011 | 0.017 | 0.014 | 0.013 | 0.019 | 0.021 |
| | CO.2 | mdd | 1.60 | | | CO.2 | (PPM) | 2.25 | 2.35 | 2.30 | 2.46 | 2.41 | 2,42 | 2.51 | 2.51 |
| | PART.1 | (µg/m³) | 10.86 | | | PART.1 | (µg/m³) | 10.42 | 11.47 | 10.43 | 11.88 | 15.67 | 11.19 | 12.14 | 12.16 |
| | N02.1 | mdd | 0.026 | | | N02.1 | (PPM) | 0.056 | 0.047 | 0.046 | 0.083 | 1.434 | 0.089 | 0.054 | 0.045 |
| | CO.1 | mdd | 2.75 | | | CO.1 | (PPM) | 4.93 | 4.10 | 4.57 | 5.50 | 44.43 | 6.14 | 3.92 | 3.33 |
| | V0C9 | $(\mu g/m^3)$ | 205 | | | VOC9 | (µg/m³) | 281 | 234 | 4099 | 407 | 236 | 215 | 247 | 214 |
| | 800C8 | $(\mu g/m^3)$ | 217 | | | VOC8 | (µg/m³) | 13163 | 253 | 274 | 330 | 258 | 237 | 566 | 221 |
| | V0C7 | (µg/m³) | 219 | | | V0C7 | (mg/m ₃) | 347 | 271 | 354 | 296 | 255 | 258 | 9360 | 752 |
| | 9200 | (mg/m ₃) | 225 | | | 920A | (µg/m³) | 393 | 314 | 347 | 462 | 4332 | 482 | 312 | 256 |
| ntrations | VOCS | (µg/m³) | 117 | | SI | VOCS | (µg/m³) | 131 | 126 | 126 | 171 | 160 | 416 | 125 | 120 |
| vg conce | VOC4 | (μg/m³) | 183 | | entration | VOC4 | (µg/m³) | 232 | 197 | 506 | 303 | 274 | 1593 | 208 | 178 |
| 1 24-hr a | VOC3 | (μg/m³) | 218 | | seak con | VOC3 | (µg/m³) | 645 | 384 | 672 | 1630 | 297 | 337 | 293 | 2430 |
| C overal | VOC2 | (µg/m³) | 2909 | | C zone | VOC2 | (µg/m³) | 11815 | 9465 | 10907 | 1961 | 7974 | 7537 | 6409 | 6516 |
| Table 1a - SIM1FLC overall 24-hr avg concentrations | V0C1 | (µg/m³) | 265 | | Table 1b - SIM1FLC zone peak concentrations | VOCI | (µg/m³) | 303 | 185 | 164 | 333 | 141 | 138 | 142 | 155 |
| Table 1a | | | 24 hr avg | | Table 1b | | | BA2 | BR2 | BR3 | HAL | КП | LDA | MBA | MBR |

| Table BA2 BR2 BR3 HAL KIT | Table C - SIMIFLC zone 24-hr avg concentrations VOC1 VOC2 VOC3 VOC4 VOC5 VOC5 | FLC zone VOC2 (µg/m³) 8418 6422 8211 5249 5540 | 24-hr avg VOC3 (µg/m³) 255 172 252 316 | 2 concent VOC4 (µg/m³) 138 124 132 128 | rations VOC5 (μg/m³) 109 106 107 108 | VOC6 (µg/m³) 190 157 178 177 647 | VOC7 (μg/m³) 200 155 196 223 | VOC8 (µg/m³) 1915 149 165 155 | VOC9 (μg/m³) 160 137 727 145 | CO.1 (PPM) 2.38 2.09 2.30 2.32 6.59 | NO2.1 (PPM) 0.009 0.010 0.009 0.016 | PART.1 (μg/m³) 9.84 10.66 10.01 11.10 | CO.2 (PPM) 1.61 1.61 1.62 1.60 | NO2.2 (PPM) 0.005 0.007 0.005 0.009 | PART.2 (µg/m³) 9.78 10.62 9.96 11.04 | CO.3 (PPM) 6.80 6.81 6.82 6.77 | NO2.3 (PPM) 0.047 0.075 0.050 0.086 | PART.3 (µg/m³) 3.65 13.18 5.27 16.19 |
|-------------------------------------|--|---|--|--|--|----------------------------------|------------------------------|--|---|---|--|---------------------------------------|---|--|--------------------------------------|---|--|--------------------------------------|
| LDA | 901 | 6040 | 162 | 312 | 141 | 506 | 147 | 141 | 131 | 2.62 | 0.018 | 10.84 | 1.61 | 0.008 | 10.75 | 6.77 | 0.076 | 13.73 |
| MBA | 104 | 4130 | 136 | 116 | 103 | 136 | 1051 | 133 | 125 | 1.92 | 0.013 | 11.41 | 1.59 | 0.010 | 11.38 | 6.71 | 0.105 | 22.41 |
| MBR | 107 | 3982 | 345 | 113 | 103 | 129 | 256 | 127 | 122 | 1.85 | 0.012 | 11.54 | 1.59 | 0.011 | 11.52 | 6.72 | 0.108 | 24.49 |

| T.2 | m³) | | 2 | 0. | 22 | 6 | * | - 13 | 2 |
|-----------|---------------|-------|-------|-------|-------|----------|-------|-------|-------|
| PART.2 | (grl) | 10.1 | Ξ | 10.2 | 11.3 | 10.5 | 10.8 | 11.3 | 11.7 |
| NO2.2 | (PPM) | 0.007 | 0.012 | 0.007 | 0.012 | 0.011 | 0.010 | 0.013 | 0.015 |
| CO.2 | (PPM) | 1.55 | 1.66 | 1.54 | 1.65 | 1.60 | 1.59 | 1.64 | 1 69 |
| PART.1 | $(\mu g/m^3)$ | 9.50 | 10.23 | 9.75 | 10.98 | 13.06 | 10.85 | 11.30 | 11 33 |
| N02.1 | (PPM) | 0.015 | 0.012 | 0.015 | 0.036 | 0.515 | 0.046 | 0.013 | 0.012 |
| CO.1 | (PPM) | 3.51 | 2.93 | 3.36 | 4.21 | 23.65 | 5.09 | 2.59 | 2.47 |
| 620A | (µg/m³) | 504 | 167 | 1958 | 213 | 191 | 151 | 152 | 152 |
| VOC8 | (µg/m³) | 5479 | 175 | 130 | 200 | 170 | 160 | 159 | 150 |
| V0C7 | (µg/m³) | 274 | 202 | 249 | 394 | 168 | 164 | 3126 | 551 |
| 900V | (µg/m³) | 276 | 509 | 243 | 327 | 1808 | 325 | 174 | 45 |
| VOCS | (µg/m³) | 118 | 113 | 114 | 126 | 126 | 244 | 108 | 108 |
| VOC4 | (µg/m³) | 170 | 145 | 153 | 168 | 181 | 298 | 137 | 133 |
| | (µg/m³) | | | | | | | | |
| VOC2 | (µg/m³) | NA | NA | Ν | NA | Ν | ΑN | NA | Ϋ́ |
| VOCI VOC2 | (µg/m³) | 147 | 114 | 114 | 138 | <u>1</u> | 105 | 102 | 108 |
| | | BA2 | BR2 | BR3 | HAL | KIT | LDA | MBA | MBR |

| r avg concentrations | | | | | | HAL 3.54 1.66 | | | | |
|----------------------|------|-------|------|------|------|---------------|-------|------|------|------|
| C zone 1-n | CO.2 | (PPM) | 1.67 | 1.68 | 1.65 | 1.66 | 1.64 | 1.65 | 1.63 | 1.64 |
| e - SIMILLI | CO.1 | (PPM) | 2.54 | 2.52 | 2.58 | 3.54 | 33.72 | 3.87 | 2.55 | 2.52 |
| l able 1 | | | BA2 | BR2 | BR3 | HAL | KIT | LDA | MBA | MBR |

| VOCI | Burst - UCL | CO.1 | Oven |
|------|-------------|--------|-------------|
| VOC2 | Floor | N02.1 | Oven |
| VOC3 | Burst - MBR | PART.1 | Oven |
| V0C4 | Burst - LDA | CO.2 | Heater |
| VOCS | Burst - GAR | NO2.2 | Heater |
| 900A | Burst - KIT | PART.2 | Heater |
| VOC7 | Burst - MBA | CO.3 | Outdoor air |
| VOC8 | Burst - BA2 | NO2.3 | Outdoor air |
| VOC9 | Burst - BR3 | PART.3 | Outdoor air |

| Table 2a | - SIMIF | LM over | all 24-hr | LM overall 24-hr avg concentrations | entrations | | | | | | | | | | |
|-----------|-----------------------------|----------------|-----------|-------------------------------------|------------|---------------|---------|---------|----------------------|------|-------|---------------|------|-------|------------|
| | VOCI VOC2 V | VOC2 | VOC3 | V0C4 | VOCS | NOC6 | VOC7 | VOC8 | VOC9 | CO.1 | N02.1 | PART.1 | CO.3 | N02.3 | PART.3 |
| | (µg/m³) | μg/m³) (μg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | $(\mu g/m^3)$ | (µg/m³) | (µg/m³) | (mg/m ₃) | mdd | mdd | $(\mu g/m^3)$ | mdd | mdd | (µg/m³) |
| 24 hr avg | 24 hr avg 235 | 4899 | 165 | 152 | 86 | 506 | 189 | 218 | 183 | 2.50 | 0.025 | 11.41 | 89.9 | 0.086 | 18.45 |
| | | | | | | | | | | | | | | | |
| Table 2b | Table 2b - SIMIFLM zone pea | 'LM zone | peak cor | ncentratio | sus | | | | | | | | | | |
| | VOCI | VOC | 2 | VOC4 | VOCS | VOC6 | VOC7 | VOC8 | 600A | 20 | NO2 I | PART 1 | CO 3 | NO2 3 | NO23 PART3 |

| 1 able | 20 - SIMIL | LIM Zone | beak cor | centratio | us | | | | | | | | | | |
|--------|---------------|----------|----------|---------------|---------|---------|---------------|---------|---------|-------|-------|---------|-------|-------|---------|
| | VOCI VOC2 | VOC2 | | VOC4 | VOC5 | 900A | VOC7 | VOC8 | V0C9 | CO.1 | NO2.1 | PART.1 | CO.3 | N02,3 | PART.3 |
| | $(\mu g/m^3)$ | (µg/m³) | \sim | $(\mu g/m^3)$ | (µg/m³) | (µg/m³) | $(\mu g/m^3)$ | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| BA2 | 800 | 9379 | | 117 | 66 | 091 | 148 | 9702 | 134 | 2.72 | 0.022 | 12.12 | 11.12 | 0.177 | 29.63 |
| BR2 | 507 | 7813 | | 114 | 66 | 260 | 270 | 647 | 127 | 2.78 | 0.021 | 11.89 | 10.54 | 0.143 | 27.41 |
| BR3 | 325 | 9145 | | 113 | 66 | 193 | 198 | 403 | 3875 | 2.54 | 0.021 | 11.69 | 10.20 | 0.124 | 22.57 |
| HAL | 1408 | 9289 | 672 | 160 | 101 | 455 | 442 | 2077 | 197 | 3.53 | 0.053 | 12.29 | 11.02 | 0.198 | 35.18 |
| KIT | 276 | 7162 | | 129 | 101 | 3953 | 139 | 350 | 127 | 40.62 | 1.386 | 15.94 | 10.28 | 0.152 | 30.25 |
| LDA | 291 | 7014 | | 1400 | 108 | 477 | 147 | 369 | 121 | 6.04 | 0.106 | 12.03 | 10,38 | 0.139 | 25.94 |
| MBA | 147 | 5037 | | 115 | 66 | 151 | 8783 | 149 | 129 | 2.74 | 0.022 | 12.45 | 11.17 | 0.204 | 39.74 |
| MBR | 437 | 0869 | | 110 | 66 | 140 | 1232 | 321 | 123 | 2.52 | 0.021 | 12.28 | 10.42 | 0.201 | 34.94 |
| | | | | | | | | | | | | | | | |

| - SIMIF | Table 2c - SIM1FLM zone | CA) | g concent | trations | | | | | | | | | | |
|---------|-------------------------|-----|------------|----------|---------|---------|---------|---------|-------|-------|---------------|-------|-------|---------|
| | V0C2 | | V0C4 | VOC5 | 900A | V0C7 | VOC8 | VOC9 | CO.1 | NO2.1 | PART.1 | CO.3 | N02.3 | PART.3 |
| | (µg/m³) | _ | (mg/m_3) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | $(\mu g/m^3)$ | (PPM) | (PPM) | (µg/m³) |
| | 5128 | | 001 | 86 | Ξ | 112 | 1283 | 10 | 1.67 | 0.00 | 11.18 | 6.61 | 0.081 | 16.87 |
| | 5523 | 130 | 100 | 86 | 126 | 131 | 228 | 107 | 1.72 | 800.0 | 11.12 | 6.74 | 0.077 | 15.28 |
| | 9969 | | 001 | 86 | 122 | 125 | 151 | 737 | 1.72 | 0.007 | 10.85 | 6.72 | 990.0 | 12.77 |
| | 3811 | | 101 | 86 | 138 | 148 | 373 | 117 | 1.76 | 0.013 | 11.70 | 6.61 | 0.105 | 24.06 |
| | 4728 | | 101 | 86 | 689 | 104 | 153 | 105 | 6.77 | 0.125 | 11.92 | 99'9 | 0.089 | 19.02 |
| | 4874 | | 569 | 66 | 202 | 109 | 172 | 105 | 2.50 | 0.019 | 11.42 | 99.9 | 0.085 | 18.28 |
| | 3127 | | 66 | 86 | 103 | 1070 | 104 | 101 | 1.61 | 0.012 | 11.88 | 6.65 | 0.114 | 26.70 |
| | 4115 | 406 | 66 | 86 | 5 | 292 | 142 | 104 | 15 | 0.010 | 11.59 | 671 | 0.098 | 21 74 |

| Table 7d | - SIMIL | LIM Zone | 4-hr avg | concent | anons | | | | | | | |
|----------|----------------------|----------|----------|---------|----------------------|---------|---------|---------------|---------------|-------|-------|---------------|
| | V0C1 | V0C2 | VOC3 | VOC4 | VOC5 | 900A | V0C7 | VOC8 | VOC9 | C0.1 | NO2.1 | PART.1 |
| | (µg/m ₃) | (µg/m³) | (µg/m³) | (µg/m³) | (mg/m ₃) | (µg/m³) | (µg/m³) | $(\mu g/m^3)$ | $(\mu g/m^3)$ | (PPM) | (PPM) | $(\mu g/m^3)$ |
| BA2 | 581 | Ϋ́ | 66 | 86 | 86 | 100 | 901 | 3284 | 66 | 2.01 | 0.012 | 11.95 |
| BR2 | 293 | Ϋ́ | 105 | 86 | 86 | 104 | 105 | 358 | 113 | 2.20 | 0.011 | 11.48 |
| BR3 | 112 | ΝA | <u>8</u> | 86 | 86 | 103 | 104 | 112 | 2074 | 2.13 | 0.00 | 11.21 |
| HAL | 842 | VΑ | 104 | 86 | 86 | 103 | 108 | 1058 | 160 | 5.09 | 0.018 | 12.12 |
| KIT | 241 | VΑ | 901 | 66 | 86 | 1835 | 90 | 294 | 109 | 21.12 | 0.466 | 13.49 |
| LDA | 255 | VΑ | 101 | 631 | 86 | 330 | 101 | 311 | 110 | 4.93 | 0.052 | 11.73 |
| MBA | 66 | ΝA | 66 | 86 | 86 | 66 | 3306 | 66 | 66 | 2.03 | 0.012 | 11.93 |
| MBR | 370 | VΑ | 1131 | 86 | 86 | 901 | 489 | 271 | 108 | 2.10 | 0.00 | 11.43 |

| rations | | | | | | | | | |
|---|-------|------|------|------|------|-------|------|------|------|
| Fable 2e - SIM1FLM zone 1-hr avg concentrations | | | | | | | | | |
| M zone 1-hr | | | | | | | | | |
| CO.1 | (PPM) | 2.61 | 2.70 | 2.49 | 3.10 | 32.42 | 4.42 | 2.63 | 2.48 |
| Table 2e | | BA2 | BR2 | BR3 | HAL | KIT | LDA | MBA | MBR |

| LEGEND | _ | | | |
|--------|-------------|--------|-------------|---|
| V0C1 | Burst - UCL | CO.1 | Oven | _ |
| V0C2 | Floor | N02.1 | Oven | |
| VOC3 | Burst - MBR | PART.1 | Oven | |
| V0C4 | Burst - LDA | CO.2 | Heater | |
| VOCS | Burst - GAR | N02.2 | Heater | |
| 900A | Burst - KIT | PART.2 | Heater | |
| V0C7 | Burst - MBA | CO.3 | Outdoor air | |
| VOC8 | Burst - BA2 | N02.3 | Outdoor air | |
| VOC9 | Burst - BR3 | PART.3 | Outdoor air | |

| able 3a | - SIMIF | "H overa | Il 24-hr a | vg concer | ntrations | | | | | | | | | | |
|---------|----------------|----------|------------|-----------|-----------|---------|---------|---------|---------|------|-------|---------|------|-------|---------|
| | VOCI | VOC2 | VOC3 | V0C4 | | 900V | VOC7 | NOC8 | 6200 | CO.1 | NO2.1 | PART.1 | CO.3 | NO2.3 | PART.3 |
| | (µg/m³) (µg/m³ | (µg/m³) | (µg/m³) | (μg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (mg/m³) | mdd | mdd | (µg/m³) | mdd | mdd | (µg/m³) |
| hravg | 319 | 6289 | 195 | 199 | 191 | 196 | 201 | 198 | 198 | 2.54 | 0.023 | 8.93 | 6.97 | 0.078 | 7.52 |

| | 6. | <u>.</u> | | _ | | | | | | |
|------------|-----------|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|
| | PART | (µg/m³) | 11.05 | 15.21 | 16.14 | 15.70 | 7.45 | 17.28 | 10.81 | 12.49 |
| | NO2.3 | (PPM) | 0.153 | 0.162 | 0.167 | 0.157 | 0.149 | 0.164 | 0.151 | 0.140 |
| | CO.3 | (PPM) | 10.59 | 19.01 | 10.65 | 10.59 | 10.59 | 10.65 | 10.58 | 10.53 |
| | PART.1 | (µg/m³) | 9.71 | 10.24 | 10.35 | 10.14 | 11.81 | 10.49 | 89.6 | 9.81 |
| | NO2.1 | (PPM) | 0.157 | 0.142 | 0.145 | 0.190 | 0.932 | 0.133 | 0.149 | 0.132 |
| | CO.1 | (PPM) | 6.94 | 6.64 | 69.9 | 7.73 | 24.57 | 6.35 | 6.70 | 6.32 |
| | 620A | (mg/m ₃) | 522 | 429 | 2923 | 299 | 489 | 453 | 512 | 469 |
| | VOC8 | (µg/m³) | 7594 | 206 | 208 | 774 | 516 | 465 | 240 | 483 |
| | VOC7 | (µg/m³) | 470 | 456 | 459 | 529 | 420 | 429 | 6299 | 1062 |
| | 00C6 | (µg/m³) | 534 | 200 | 202 | 298 | 2923 | 477 | 524 | 469 |
| ns | VOC5 | (µg/ш ₃) | 292 | 569 | 271 | 336 | 338 | 498 | 291 | 282 |
| centration | VOC4 | (mg/m ₃) | 466 | 449 | 452 | 546 | 581 | 1327 | 464 | 438 |
| peak con | VOC3 | (µg/ш ₃) | 494 | 466 | 469 | 292 | 462 | 439 | 485 | 2037 |
| LH zone | VOC2 | (µg/m³) | 6896 | 8185 | 8101 | 8797 | 9684 | 8157 | 9804 | 9722 |
| - SIMIF | VOC1 VOC2 | (µg/m³) | 453 | 293 | 295 | 574 | 295 | 586 | 295 | 315 |
| Table 3b | | | BA2 | BR2 | BR3 | HAL | KIT | LDA | MBA | MBR |

| Table 3 | c - SIMIF | TH zone | 24-hr av | g concent | rations | | | | | | | | | | |
|---------|-----------|----------------------|----------|-----------|---------|---------|---------|---------|---------|-------|-------|---------------|-------|-------|---------|
| | VOC1 VOC2 | V0C2 | VOC3 | V0C4 | VOC5 | 9200 | V0C7 | VOC8 | 620A | CO.1 | NO2.1 | PART.1 | CO.3 | NO2.3 | PART.3 |
| | (µg/m³) | (mg/m ₃) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (m/grl) | (PPM) | (PPM) | $(\mu g/m^3)$ | (PPM) | (PPM) | (µg/m³) |
| BA2 | 232 | 6505 | 81 | 190 | 185 | 194 | 189 | 430 | 193 | 2.51 | 0.020 | 8.59 | 6.97 | 0.074 | 3.99 |
| BR2 | 186 | 5918 | 183 | 183 | 174 | 186 | 181 | 188 | 185 | 2.44 | 0.020 | 80.6 | 6.97 | 0.084 | 9.40 |
| BR3 | 187 | 2997 | 184 | 184 | 175 | 188 | 183 | 189 | 284 | 2.46 | 0.020 | 9.01 | 6.97 | 0.083 | 8.81 |
| HAL | 213 | 6197 | 196 | 194 | 188 | 198 | 193 | 203 | 198 | 2.53 | 0.022 | 8.94 | 96'9 | 0.079 | 7.64 |
| KIT | 194 | 6570 | 189 | 199 | 195 | 274 | 188 | 195 | 192 | 3.31 | 0.054 | 8.74 | 6.97 | 0.072 | 4.40 |
| LDA | 184 | 926 | 181 | 526 | 215 | 185 | 180 | 186 | 183 | 2.43 | 0.019 | 60'6 | 6.97 | 0.082 | 9.25 |
| MBA | 195 | 6510 | 130 | 189 | 184 | 193 | 406 | 195 | 192 | 2.49 | 0.020 | 8.61 | 96.9 | 0.074 | 4.37 |
| MBR | 203 | 6604 | 253 | 187 | 182 | 161 | 238 | 192 | 190 | 2.47 | 0.019 | 89.8 | 96.9 | 0.072 | 5.26 |

| | VOCI | VOC2 | VOC3 | VOC4 | VOCS | VOC6 | VOC7 | VOC8 | VOC9 | 000 | NO2 1 | PART |
|-----|---------|---------|---------|---------|---------|---------|---------|---------|---------|-------|-------|---------|
| | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| BA2 | 337 | NA | 322 | 318 | 224 | 334 | 320 | 1011 | 321 | 4.82 | 0.060 | 8.94 |
| BR2 | 240 | NA | 310 | 304 | 208 | 322 | 305 | 322 | 308 | 4.75 | 0.057 | 9.12 |
| BR3 | 242 | NA | 313 | 307 | 212 | 325 | 308 | 325 | 645 | 4.76 | 0.058 | 9.11 |
| HAL | 315 | NA | 345 | 331 | 236 | 350 | 338 | 368 | 334 | 4.95 | 0.067 | 9.20 |
| KIT | 249 | NA | 320 | 346 | 249 | 809 | 317 | 331 | 319 | 7.38 | 0.169 | 9.76 |
| LDA | 235 | NA | 303 | 447 | 305 | 318 | 298 | 313 | 301 | 4.63 | 0.054 | 9.24 |
| MBA | 249 | NA | 318 | 313 | 222 | 329 | 1019 | 328 | 317 | 4.73 | 0.058 | 9.05 |
| MBR | 267 | AN | 525 | 307 | 215 | 323 | 482 | 322 | 310 | 4.70 | 0.054 | 9.01 |

| Table 3e - SIM1FLH zone 1-hr avg concentrations | | | | | | | | | | |
|---|------|-------|------|------|------|------|-------|------|------|------|
| - SIMIFLE | CO.1 | (PPM) | 5.25 | 2.00 | 5.03 | 5.92 | 14.73 | 4.85 | 5.15 | 4.85 |
| Table 36 | | | BA2 | BR2 | BR3 | HAL | KIT | LDA | MBA | MBR |

| LEGEND | | | |
|--------|-------------|--------|-------------|
| V0C1 | Burst - UCL | CO.1 | Oven |
| VOC2 | Floor | N02.1 | Oven |
| VOC3 | Burst - MBR | PART.1 | Oven |
| VOC4 | Burst - LDA | CO.2 | Heater |
| VOC5 | Burst - GAR | N02.2 | Heater |
| 900A | Burst - KIT | PART.2 | Heater |
| VOC7 | Burst - MBA | CO.3 | Outdoor air |
| VOC8 | Burst - BA2 | NO2.3 | Outdoor air |
| VOC9 | Burst - BR3 | PART.3 | Outdoor air |

| CO.2 NO2.2 PART.2 CO.3 NO2.3 | (μg/m³) ppm ppm (μg/m³) (PPM) (PPM) (μg/m³) | 7000 0000 0000 | | CO.2 NO2.2 PART.2 CO.3 NO2.3 I | (PPM) (PPM) (μg/m³) (PPM) (PPM) | 1.94 0.006 7.72 7.84 0.050 | 1.95 0.008 8.56 7.98 0.071 | 1.92 0.005 7.64 7.81 0.047 | 8.68 2.02 0.008 8.57 8.23 0.064 8.40 | 2.03 0.007 8.53 8.17 0.058 | 2.11 0.012 8.16 8.14 0.056 | 2.07 0.007 9.37 8.47 0.073 | 2.06 0.009 9.50 8.47 0.092 |
|--|---|----------------|---|--------------------------------|---------------------------------|----------------------------|----------------------------|----------------------------|--------------------------------------|----------------------------|----------------------------|----------------------------|----------------------------|
| - | (gr) mdd | | | | | | | | 0.093 8.6 | | | | |
| CO.1 | ppm 4 63 | | | CO.1 | (PPM) | 6.93 | 5.78 | 60.9 | 8.69 | 55.25 | 99.9 | 6.25 | 5.17 |
| V0C9 | (µg/m³) 449 | | | VOC9 | (µg/m³) | 999 | 480 | 4999 | 700 | 480 | 442 | 495 | 412 |
| VOC8 | (μg/m³) 453 | | | VOC8 | (µg/m³) | 15042 | 518 | 550 | 735 | 517 | 476 | 535 | 445 |
| V0C7 | (µg/m³) 477 | | | V0C7 | (µg/m³) | 499 | 435 | 480 | 781 | 434 | 429 | 12243 | 1262 |
| 900A | (µg/m³) 460 | | | 9200 | (µg/m³) | 651 | 547 | 583 | 786 | 5238 | 575 | 267 | 468 |
| voc5 |) (μg/m³) (μ 181 | | ıs | VOC5 | (µg/m³) | 202 | 188 | 961 | 242 | 227 | 514 | 188 | 175 |
| vg conce VOC4 | (µg/m³) 407 | | entration | VOC4 | (µg/m³) | 473 | 403 | 427 | 595 | 564 | 2037 | 417 | 349 |
| VOC3 | (µg/m³) 451 | | peak con | VOC3 | (mg/m ₃) | 663 | 540 | 604 | 1664 | 528 | 206 | 543 | 3273 |
| VOC2 | (µg/m³) | | TC zone | VOC2 | (µg/m³) | 26616 | 24005 | 27100 | 21531 | 21679 | 22088 | 19220 | 18640 |
| Table 4a - SIMIFIC overall 24-hr avg concentrations VOC1 VOC2 VOC3 VOC4 VOC5 | (mg/m³) | 8 | Table 4b - SIM1FTC zone peak concentrations | VOCI | (µg/m³) | 745 | 506 | 263 | 295 | 245 | 241 | 245 | 304 |
| Table 4a | 24 hr avo | 9.11.12 | Table 4b | | | BA2 | BR2 | BR3 | HAL | KIT | LDA | MBA | MBR |

| l able 4 | C - SIMILE | IC Zone | 24-nr avg | concent | ranons | | | | | | | | | | | | | |
|----------|--------------------------|---------|---------------|---------------|---------------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|
| | VOC1 VOC2 VOC3 VOC4 VOC5 | VOC2 | VOC3 | V0C4 | VOC5 | 9000 | VOC7 | VOC8 | VOC9 | CO.1 | NO2.1 | PART.1 | CO.2 | N02.2 | PART.2 | CO.3 | l l | PART.3 |
| | $(\mu g/m^3)$ | (µg/m³) | $(\mu g/m^3)$ | $(\mu g/m^3)$ | $(\mu g/m^3)$ | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | | (µg/m³) |
| BA2 | 370 | 21831 | 435 | 332 | 167 | 423 | 397 | 5389 | 392 | 4.15 | 0.007 | 7.06 | 1.64 | 0.002 | 96.9 | 6.63 | | 1.17 |
| BR2 | 199 | 19345 | 360 | 287 | 154 | 361 | 337 | 355 | 336 | 3.64 | 0.007 | 7.76 | 1.63 | 0.003 | 7.68 | 6.63 | 0.031 | 4.72 |
| BR3 | 215 | 22228 | 425 | 320 | 163 | 407 | 387 | 336 | 1368 | 4.01 | 9000 | 7.05 | 1.64 | 0.002 | 96.9 | 6.62 | | 1.72 |
| HAL | 244 | 18147 | 559 | 310 | 164 | 393 | 453 | 382 | 362 | 4.01 | 0.011 | 8.08 | 1.65 | 0.003 | 7.98 | 69.9 | | 4.62 |
| KIT | 192 | 18356 | 347 | 332 | 691 | 1182 | 324 | 344 | 326 | 11.45 | 0.156 | 8.80 | 1.65 | 0.004 | 7.92 | 6.67 | | 5.42 |
| LDA | 195 | 19336 | 359 | 653 | 237 | 404 | 331 | 345 | 327 | 4.09 | 0.011 | 7.79 | 1.72 | 0.003 | 7.77 | 19.9 | | 4.36 |
| MBA | 184 | 16010 | 325 | 264 | 148 | 328 | 2220 | 322 | 307 | 3.46 | 0.00 | 8.52 | 1.63 | 0.005 | 8.44 | 6.70 | | 7.87 |
| MBR | 203 | 15191 | 782 | 241 | 141 | 296 | 579 | 291 | 777 | 3.17 | 0 008 | 8 80 | 1 63 | 0.005 | 8 74 | 699 | | 0 21 |

| l able 4 | d - SIMIL | I C zone | 4-hr avg | $\mathbf{\mathcal{Q}}$ | ations | | | | | | | | | | |
|----------|----------------|----------|----------|------------------------|------------|---------------|---------|---------|---------------|-------|-------|---------------|-------|-------|---------|
| | VOC1 VOC2 VOC3 | VOC2 | VOC3 | V0C4 | VOC5 | 900A | VOC7 | VOC8 | V0C9 | CO.1 | NO2.1 | PART.1 | CO.2 | NO2.2 | PART.2 |
| | (µg/m³) | (μg/m³) | (µg/m³) | $\overline{}$ | (mg/m^3) | $(\mu g/m^3)$ | (µg/m³) | (µg/m³) | $(\mu g/m^3)$ | (PPM) | (PPM) | $(\mu g/m^3)$ | (PPM) | (PPM) | (µg/m³) |
| BA2 | 409 | Ν | 534 | | 181 | 502 | 429 | 7730 | 450 | 4.26 | 0.010 | 19'9 | 1.47 | 0.004 | 7.42 |
| BR2 | 203 | ΝA | 421 | | 16 | 417 | 361 | 403 | 378 | 3.71 | 0.008 | 7.18 | 1.52 | 9000 | 8.34 |
| BR3 | 216 | ΑN | 495 | | 173 | 461 | 405 | 443 | 3063 | 3.95 | 0.008 | 6.64 | 1.46 | 0.003 | 7.42 |
| HAL | 264 | Ϋ́ | 926 | | 187 | 522 | 538 | 465 | 451 | 5.07 | 0.021 | 7.76 | 1.52 | 0.005 | 8.29 |
| KIT | 188 | ΥN | 392 | | 192 | 2859 | 336 | 387 | 363 | 37.17 | 0.675 | 11.35 | 1.50 | 0.002 | 8.13 |
| LDA | 190 | Ν | 390 | | 363 | 419 | 334 | 372 | 350 | 5.01 | 0.025 | 7.64 | 1.54 | 0.007 | 8.03 |
| MBA | 179 | Ν | 387 | | 156 | 382 | 5928 | 368 | 346 | 3.70 | 0.010 | 8.35 | 1.52 | 9000 | 8.52 |
| MBR | 208 | Ϋ́ | 1828 | | 148 | 339 | 882 | 328 | 310 | 3 34 | 0000 | 8 40 | 1.55 | 0.007 | 0.07 |

| I-hr avg concentrations | | | | | | HAL 3.25 1.56 | | | | |
|-------------------------|------|-------|------|------|------|---------------|-------|------|------|---|
| I.C zone | CO.2 | (PPM) | 1.52 | 1.55 | 1.51 | 1.56 | 1.54 | 1.61 | 1.55 | |
| e - SIMIF | CO.1 | (PPM) | 3.02 | 2.91 | 3.02 | 3.25 | 39.33 | 3.41 | 2.81 | |
| Table 4 | | | BA2 | BR2 | BR3 | HAL | KIT | LDA | MBA | 1 |

| | Oven | Oven | Oven | Heater | Heater | Heater | Outdoor air | Outdoor air | Outdoor air |
|--------|-------------|-------|-------------|--------|-------------|-------------|-------------|-------------|-------------|
| | CO.1 | N02.1 | PART.1 | CO.2 | NO2.2 | PART.2 | CO.3 | N02.3 | PART,3 |
| _ | Burst - UCL | Floor | Burst - MBR | | Burst - GAR | Burst - KIT | Burst - MBA | Burst - BA2 | Burst - BR3 |
| LEGEND | VOCI | V0C2 | VOC3 | V0C4 | VOCS | 900A | VOC7 | VOC8 | VOC9 |
| | | | | | | | | | |

| le 5a | able 5a - SIMIFTM | TM over | ıll 24-hr | avg conce | ntrations | | | | | | | | | | |
|--------|-------------------|---------|-----------|-----------|-----------|---------|---------|---------|---------|------|-------|---------|------|-------|---------|
| | VOCI | VOC2 | V0C3 | VOC4 | VOCS | 900A | VOC7 | VOC8 | VOC9 | CO.1 | NO2.1 | PART.1 | CO.3 | NO2.3 | PART.3 |
| | (µg/m³) | (μg/m³) | _ | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | mdd | mdd | (µg/m³) | mdd | mdd | (µg/m³) |
| Ir avg | 682 | 21165 | 485 | 407 | 136 | 525 | 207 | 202 | 510 | 4.18 | 0.025 | 9.23 | 6.94 | 0.039 | 7.32 |

| | ART.3 | (µg/m³) | 3.30 | 9.94 | 8.70 | 4.15 | 1.10 | 1.07 | 5.94 | 3.82 | |
|---|--------|---------|-------|-------|-------|-------|-------|-------|-------|-------|--|
| | ~ | (PPM) | | | | | | | | ĺ | |
| - | CO.3 | (PPM) | 9.23 | 8.79 | 8.52 | 10.22 | 8.75 | 8.88 | 9.19 | 8.60 | |
| | PART.1 | (μg/m³) | 10.39 | 88.6 | 9.50 | 11.39 | 15.24 | 10.26 | 10.73 | 10.04 | |
| | NO2.1 | (PPM) | 0.025 | 0.021 | 0.021 | 0.037 | 1.558 | 0.071 | 0.025 | 0.020 | |
| | CO.1 | (PPM) | 4.48 | 3.89 | 4.04 | 5.32 | 50.31 | 5.98 | 4.15 | 3.66 | |
| | VOC9 | (µg/m³) | 473 | 381 | 5598 | 276 | 394 | 369 | 403 | 328 | |
| | VOC8 | (μg/m³) | 16764 | 406 | 429 | 673 | 419 | 394 | 428 | 349 | |
| | VOC7 | (µg/m³) | 482 | 353 | 453 | 989 | 364 | 362 | 12871 | 985 | |
| | 900A | (µg/m³) | 535 | 426 | 482 | 640 | 5588 | 282 | 451 | 365 | |
| | VOC5 | (µg/m³) | 136 | 127 | 130 | 154 | 148 | 321 | 130 | 122 | |
| | VOC4 | (µg/m³) | 338 | 278 | 308 | 414 | 393 | 2126 | 293 | 244 | |
| | VOC3 | (µg/m³) | 889 | 423 | 288 | 1694 | 447 | 480 | 422 | 3333 | |
| | VOC2 | (µg/m³) | 33912 | 26965 | 33256 | 22311 | 22296 | 24215 | 17811 | 17054 | |
| | VOCI | (µg/m³) | 649 | 991 | 168 | 468 | 143 | 145 | 143 | 202 | |
| | | | BA2 | BR2 | BR3 | HAL | KIT | LDA | MBA | MBR | |

| | _ | _ | | _ | | | | | - | _ |
|------------|--------|---------|-------|-------|-------|---------------|-------|-------|-------|-------|
| | PART. | (µg/m³) | 91.9 | 5.94 | 4.88 | 13.40 | 7.31 | 7.09 | 10.40 | 8.23 |
| | NO2.3 | (PPM) | 0.037 | 0.034 | 0.028 | 0.062 | 0.040 | 0.038 | 0.052 | 0.043 |
| | CO.3 | (PPM) | 7.05 | 7.04 | 7.00 | 6.92 | 88.9 | 6.93 | 6.84 | 6.82 |
| | PART.1 | (µg/m³) | 8.98 | 8.79 | 8,37 | 9.93 | 10.26 | 9.25 | 9.76 | 9.31 |
| | NO2.1 | (PPM) | 0.005 | 0.004 | 0.004 | 0.008 | 0.163 | 0.012 | 9000 | 0.005 |
| | CO.1 | (PPM) | 2.50 | 2.41 | 2.51 | 2.51 | 14.24 | 4.01 | 2.20 | 2.19 |
| | VOC9 | (µg/m³) | 355 | 270 | 2356 | 290 | 250 | 257 | 222 | 199 |
| | VOC8 | (µg/m³) | 5792 | 285 | 320 | 325 | 259 | 271 | 229 | 504 |
| | V0C7 | (µg/m³) | 410 | 276 | 377 | 491 | 249 | 277 | 3606 | 209 |
| | 900V | (µg/m³) | 400 | 298 | 369 | 320 | 1948 | 452 | 237 | 211 |
| trations | VOC5 | (µg/m³) | 122 | 114 | 119 | 117 | 122 | 182 | 109 | 107 |
| g concen | VOC4 | (µg/m³) | 259 | 207 | 244 | 224 | 247 | 845 | 175 | 191 |
| : 24-nr av | VOC3 | (µg/m³) | 531 | 314 | 473 | 765 | 275 | 328 | 242 | 994 |
| · I M zone | VOC2 | (µg/m³) | 28144 | 21431 | 28226 | 18383 | 19565 | 21558 | 15095 | 14002 |
| - SIMIL | VOCI | (µg/m³) | 324 | 138 | 152 | HAL 186 18383 | 127 | 134 | 121 | 142 |
| I able 50 | | | BA2 | BR2 | BR3 | HAL | KIT | LDA | MBA | MBR |

| laore | I IMIC - DC | JIM ZOIIC | 4-III avg | CONCOR | attons | | | | | | | |
|-------|-------------|-----------|---------------|---------|---------|---------------|----------------------|---------|---------|---------|-------|---------|
| | VOCI | VOC2 | VOC3 | V0C4 | VOC5 | 900A | VOC7 | VOC8 | VOC9 | CO.1 | NO2.1 | PART.1 |
| | (μg/m³) | (µg/m³) | $(\mu g/m^3)$ | (µg/m³) | (µg/m³) | (µg/m³) | (mg/m ₃) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| BA2 | 346 | Ϋ́ | 617 | 258 | 124 | \$ | 422 | 11952 | 347 | 2.09 | 900.0 | 10.21 |
| BR2 | 137 | Ϋ́ | 318 | 205 | 911 | 290 | 280 | 273 | 263 | 2.13 | 0.004 | 9.49 |
| BR3 | 153 | Ϋ́ | 495 | 241 | 121 | 362 | 377 | 334 | 4424 | 2.14 | 0.004 | 9.10 |
| HAL | 184 | N A | 1277 | 255 | 121 | 462 | 207 | 286 | 316 | 2.03 | 0.00 | 11.21 |
| KIT | 122 | N A | 246 | 238 | 124 | 4094 | 223 | 228 | 222 | 35.41 | 0.623 | 13.13 |
| VO | 130 | Ϋ́ | 294 | 1637 | 232 | 420 | 253 | 242 | 234 | 5.23 | 0.039 | 10.05 |
| MBA | 115 | NA | 234 | 152 | 107 | 194 | 8311 | 188 | 184 | 2.10 | 900.0 | 10.17 |
| MBR | 142 | NA | 2236 | 150 | 107 | 188 | 703 | 181 | 179 | 2.08 | 0.004 | 9.38 |
| MAIN | 74. | 1 | 25.00 | 251 | 2 | 1 | 3 | | COV | 101 607 | (11) | 00.7 |

| able 6a. | SIMIF, | l'H overa | II 24-hr a | ivg concei | ntrations | | | | | | | | | | |
|----------|----------------|-----------|---------------|------------|-----------|---------|---------|---------|---------|------|-------|---------|------|-------|---------|
| | VOCI | VOC2 | VOC3 | V0C4 | VOC5 | 900A | V0C7 | VOC8 | V0C9 | CO.1 | N02.1 | PART.1 | CO.3 | NO2.3 | PART.3 |
| | (µg/m³) (µg/m³ | (µg/m³) | $(\mu g/m^3)$ | (µg/m³) | (µg/m³) | (μg/m³) | (µg/m³) | (μg/m³) | (µg/m³) | mdd | udd | (µg/m³) | mdd | mdd | (µg/m³) |
| 4 hr avg | 465 | 9517 | 239 | 243 | 507 | 237 | 249 | 237 | 240 | 2.91 | 0.022 | 7.55 | 66.9 | 0.056 | 4.57 |

| Table 6 | D - SIMIL | ·IH zone | peak con | centration | us | | | | | | | | | | |
|---------|-----------|---------------|----------|------------|---------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|
| | VOCI VOC2 | VOC2 | | VOC4 | VOC5 | 900A | VOC7 | VOC8 | VOC9 | CO.1 | NO2.1 | PART.1 | CO.3 | NO2.3 | PART.3 |
| | (µg/m³) | $(\mu g/m^3)$ | | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| BA2 | 450 | 13490 | | 538 | 069 | 593 | 533 | 8105 | 557 | 7.26 | 0.167 | 8.15 | 9.63 | 0.108 | 4.59 |
| BR2 | 303 | 12531 | | 206 | 671 | 534 | 464 | 533 | 519 | 6.74 | 0.147 | 8.17 | 9.63 | 0.110 | 6.50 |
| BR3 | 306 | 12882 | | 516 | 879 | 546 | 504 | 545 | 3081 | 6.84 | 0.150 | 8.14 | 9.63 | 0.111 | 6.77 |
| HAL | 357 | 12933 | | 209 | 728 | 099 | 574 | 629 | 635 | 7.93 | 0.197 | 8.54 | 9.63 | 0.110 | 9.25 |
| KIT | 304 | 13565 | | 631 | 737 | 3067 | 209 | 552 | 532 | 25.60 | 0.974 | 10.40 | 9.62 | 0.106 | 4.10 |
| LDA | 295 | 12422 | | 1409 | 870 | 210 | 475 | 209 | 200 | 6.48 | 0.136 | 8.39 | 9.65 | 0.114 | 8.85 |
| MBA | 305 | 13392 | 548 | 532 | 089 | 279 | 7217 | 278 | 543 | 7.05 | 0.160 | 8.24 | 9.64 | 0.109 | 2.00 |
| MBR | 325 | 13358 | | 505 | 699 | 531 | 1187 | 530 | 519 | 6.62 | 0.139 | 8.21 | 9.60 | 0.103 | 5.71 |

| Fable 6 | c - SIMIF | TH zone | 24-hr av | g concent | rations | | | | | | | | | | | |
|---------|---------------|---------|----------|---------------|------------|---------|---------|---------|---------------|-------|-------|---------------|-------|-------|---------|--|
| | VOC1 VOC2 | VOC2 | VOC3 | VOC4 | VOCS | 900A | V0C7 | VOC8 | V0C9 | CO.1 | NO2.1 | PART.1 | CO.3 | NO2.3 | PART.3 | |
| | $(\mu g/m^3)$ | (µg/m³) | (µg/m³) | $(\mu g/m^3)$ | (mg/m^3) | (µg/m³) | (µg/m³) | (µg/m³) | $(\mu g/m^3)$ | (PPM) | (PPM) | $(\mu g/m^3)$ | (PPM) | (PPM) | (µg/m³) | |
| BA2 | 298 | 9617 | 235 | 235 | 488 | 236 | 237 | 480 | 236 | 2.89 | 0.020 | 7.29 | 6.99 | 0.054 | 2.63 | |
| BR2 | 231 | 9354 | 230 | 229 | 468 | 230 | 231 | 230 | 230 | 2.84 | 0.019 | 7.55 | 86.9 | 0.057 | 4.83 | |
| BR3 | 233 | 9446 | 231 | 231 | 473 | 232 | 233 | 232 | 334 | 2.86 | 0.019 | 7.48 | 66.9 | 0.056 | 4.32 | |
| HAL | 248 | 9378 | 240 | 240 | 504 | 240 | 242 | 241 | 240 | 2.92 | 0.022 | 7.54 | 86.9 | 0.056 | 4.75 | |
| KIT | 235 | 9590 | 233 | 243 | 515 | 317 | 234 | 233 | 233 | 3.72 | 0.055 | 7.47 | 66.9 | 0.053 | 3.16 | |
| LDA | 225 | 9084 | 224 | 270 | 581 | 224 | 225 | 224 | 224 | 2.79 | 0.018 | 7.68 | 6.99 | 0.058 | 5.65 | |
| MBA | 237 | 9504 | 234 | 233 | 483 | 234 | 467 | 234 | 234 | 2.87 | 0.020 | 7.37 | 86.9 | 0.055 | 3.34 | |
| MBR | 251 | 9639 | 300 | 231 | 475 | 231 | 288 | 231 | 231 | 2.84 | 0.018 | 7.43 | 86.9 | 0.054 | 3.95 | |

| Table 60 | d - SIMIF | TH zone | 4-hr avg | concentra | utions | | | | | | | |
|----------|---------------|---------------|----------|---------------|---------|---------------|---------------|---------|---------|-------|-------|---------|
| | VOCI | V0C2 | VOC3 | VOC4 | VOC5 | 920A | V0C7 | VOC8 | VOC9 | CO.1 | NO2.1 | PART.1 |
| | $(\mu g/m^3)$ | $(\mu g/m^3)$ | (µg/m³) | $(\mu g/m^3)$ | (µg/m³) | $(\mu g/m^3)$ | $(\mu g/m^3)$ | (µg/m³) | (μg/m³) | (PPM) | (PPM) | (µg/m³) |
| BA2 | 368 | Y. | 382 | 376 | 489 | 385 | 376 | 1201 | 380 | 5.28 | 0.064 | 7.73 |
| BR2 | 254 | NA | 370 | 364 | 464 | 374 | 362 | 372 | 369 | 5.15 | 090'0 | 7.87 |
| BR3 | 257 | NA | 375 | 369 | 472 | 378 | 367 | 377 | 721 | 5.19 | 0.061 | 7.83 |
| HAL | 288 | Ν | 400 | 391 | 520 | 399 | 393 | 405 | 395 | 5.40 | 0.072 | 8.00 |
| KIT | 258 | NA | 376 | 404 | 533 | 664 | 368 | 377 | 374 | 7.89 | 0.177 | 8.11 |
| LDA | 247 | NA | 358 | 209 | 663 | 363 | 350 | 360 | 326 | 2.00 | 0.056 | 8.03 |
| MBA | 260 | NA | 376 | 371 | 480 | 380 | 1142 | 378 | 375 | 5.20 | 0.062 | 7.83 |
| MBR | 284 | Ϋ́ | 009 | 362 | 463 | 372 | 542 | 370 | 367 | 5.11 | 0.058 | 7.87 |

| cone 1-hr avg concentrations | | | | | | | | | | MBR 4.80 |
|------------------------------|------|-------|------|------|------|------|-------|------|------|----------|
| S-SIMIFIH | CO.1 | (PPM) | 5.33 | 4.95 | 5.02 | 00.9 | 15.11 | 4.77 | 5.20 | 4.80 |
| l able of | | | BA2 | BR2 | BR3 | HAL | KIT | LDA | MBA | MBR |

| LEGEND | ١. | | |
|------------|-------------|--------|-------------|
| 100 100 | Burst - OCL | | Oven |
| VOC2 | Floor | N02.1 | Oven |
| VOC3 | Burst - MBR | PART.1 | Oven |
| VOC4 | Burst - LDA | CO.2 | Heater |
| VOC5 | Burst - GAR | N02.2 | Heater |
| NOC6 | Burst - KIT | PART.2 | Heater |
| VOC7 | Burst - MBA | CO.3 | Outdoor air |
| VOC8 | Burst - BA2 | N02.3 | Outdoor air |
| 000 N | Burst - BR3 | PART.3 | Outdoor air |

| | CO.1 NO2.1 PART.1 CO.2 NO2.2 PART,2 CO.3 NO2.3 | (μg/m³) (PPM) (μg/m³) (PPM) (μg/m³) (PPM) (μg/m³) (PPM) (μg/m³) (144 2.01 0.020 10.23 1.84 0.018 10.58 6.70 0.102 14.46 | 2.01 0.020 10.23 1.84 0.018 10.58 6.70 0.102 | CO.1 NO2.1 PART.1 CO.2 NO2.2 PART.2 CO.3 NO2.3 I | (PPM) (PPM) (µg/m³) (PPM) (PPM) (µg/m³) (PPM) (PPM) | 5.27 0.108 9.84 3.37 0.112 11.96 10.02 0.129 | 4.33 0.081 11.16 2.85 0.083 12.23 10.87 0.198 | 4.81 0.092 10.36 3.15 0.096 11.94 10.12 0.139 | 4.56 0.082 11.42 2.98 0.082 12.04 10.59 0.170 | 14,70 0.544 11.41 3.12 0.095 12.02 10.26 0.180 | 5.28 0.112 10.66 3.09 0.095 12.02 10.24 0.168 | 294 4.78 0.095 11.38 3.08 0.097 12.16 10.46 0.216 33.26 | 0000 3011 3001 3000 300 1011 2000 000 |
|----------------|--|--|---|--|---|--|---|---|---|--|---|---|---------------------------------------|
| | VOC8 | µg/m³) (µg/m³) () 143 364 | 364 | VOC8 | (μg/m³) | 1237 | 924 | === | 963 | 1061 | 1065 | 6114 1034 | 988 |
| rations | 920A | (µg/m³) (145 | 145 | C5 VOC6 | (µg/m³) | 380 | 303 | 331 | 279 | 2864 | 413 | 201 308 (| 757 |
| r avg concent | VOC4 V | (µg/m³) (µ 140 1 | 140 oncentrations | VOC4 V | (µg/m³) | 342 | 276 | 300 | 252 | 280 | 1079 | 281 | 236 |
| C overall 24-h | VOC2 VOC3 | (μg/m³) (μg/m³) (μg/m³) (μg/m³) (μg/m³) 24 hr avg 182 2767 144 140 127 | 24 hr avg 182 2767 144 140 15 Table 7b - SIM1MLC zone peak concentrations | VOC2 VOC3 | | | | | | | | 2890 298 | |
| 7a - SIMIML | VOCI | (µg/m³) (µg/m²) (µg/m² | 'g 182 'b - SIM1ML | VOCI | _ | | | | | | | 86 | |
| Table | | 24 hr av | 24 hr avg Table 7b | | | BA2 | BR2 | BR3 | HAL | KIT | LDA | MBA | MRP |

| Table ; | 7c - SIMIR | ALC zone | 24-hr av | g concen | trations | | | | | | | | | | | | | |
|---------|--------------------------|----------------------|----------|----------|----------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|
| | VOC1 VOC2 VOC3 VOC4 VOC5 | VOC2 | VOC3 | VOC4 | VOCS | 900A | VOC7 | VOC8 | VOC9 | CO.1 | NO2.1 | PART.1 | CO.2 | NO2.2 | PART.2 | CO.3 | NO2.3 | PART.3 |
| | (µg/m³) | (mg/m ₃) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| BA2 | 86 | 3213 | 143 | 140 | 128 | 143 | 134 | 452 | 140 | 2.01 | 910.0 | 9,43 | 1.91 | 0.018 | 68.6 | 6.70 | 0.080 | 2.24 |
| BR2 | 86 | 2582 | 127 | 128 | 119 | 130 | 122 | 343 | 127 | 1.89 | 0.017 | 10.38 | 1.81 | 0.018 | 69.01 | 69.9 | 0.108 | 16.86 |
| BR3 | 86 | 3157 | 138 | 136 | 124 | 138 | 131 | 412 | 251 | 1.96 | 0.016 | 9.76 | 1.86 | 0.017 | 10.14 | 89.9 | 0.087 | 7.32 |
| HAL | 86 | 2741 | 159 | 128 | 121 | 130 | 144 | 347 | 128 | 1.91 | 0.016 | 10.35 | 1.84 | 0.017 | 69.01 | 6.72 | 0.103 | 15.64 |
| KIT | 86 | 2738 | 134 | 132 | 123 | 237 | 127 | 379 | 132 | 2.65 | 0.048 | 10.23 | 1.86 | 0.019 | 10.53 | 6.72 | 0.101 | 13.38 |
| LDA | 86 | 2719 | 135 | 165 | 142 | 140 | 128 | 379 | 132 | 1.97 | 0.018 | 10.12 | 1.86 | 0.020 | 10.51 | 69.9 | 0.099 | 12,39 |
| MBA | 86 | 2396 | 129 | 129 | 121 | 131 | 339 | 359 | 129 | 16.1 | 0.018 | 10.40 | 1.84 | 0.020 | 10.76 | 6.72 | 0.113 | 17.71 |
| MBR | 86 | 2166 | 179 | 122 | 117 | 124 | 155 | 301 | 122 | 1.85 | 0.017 | 10.87 | 1.79 | 0.019 | 11.16 | 6.72 | 0.125 | 24.87 |

| RT.2 | /m³) | 03 | 09 | 61 | 11.35 | 24 | 56 | 14 | - 19 |
|-----------|---------------|-------|-------|-------|-------|-------|-------|-------|-------|
| - | | | | | | | | | |
| N02.2 | (PPM | 0.062 | 0.047 | 0.054 | 0.047 | 0.054 | 0.053 | 0.054 | 0.044 |
| CO.2 | (PPM) | 2.98 | 2.52 | 2.79 | 2.63 | 2.78 | 2.73 | 2.71 | 2.45 |
| PART.1 | (µg/m³) | 9.15 | 10.33 | 9.59 | 6.67 | 89.6 | 9.76 | 9.87 | 10.50 |
| NO2.1 | (PPM) | 0.022 | 0.020 | 0.021 | 0.020 | 0.030 | 0.022 | 0.021 | 0.020 |
| CO.1 | (PPM) | 2.91 | 2.48 | 2.78 | 2.63 | 3.03 | 2.73 | 2.62 | 2.41 |
| VOC9 | (µg/m³) | 205 | 171 | 554 | 180 | 188 | 187 | 184 | 164 |
| VOC8 | (µg/m³) | 865 | 620 | 763 | 664 | 750 | 731 | 719 | 577 |
| V0C7 | (µg/m³) | 181 | 152 | 168 | 500 | 171 | 168 | 875 | 256 |
| VOC6 | (µg/m³) | 500 | 174 | 195 | 180 | 523 | 207 | 187 | 167 |
| VOC5 | (µg/m³) | 161 | 191 | 178 | 991 | 177 | 270 | 174 | 156 |
| VOC4 | (µg/m³) | 203 | 170 | 190 | 176 | 187 | 291 | 183 | 163 |
| VOC3 | | | | | | | | | |
| VOC2 | (µg/m³) | ٧ | ٧ | VV | Ϋ́ | Ν | VΑ | ۷V | ٧X |
| VOCI VOC2 | $(\mu g/m^3)$ | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 |
| | | BA2 | BR2 | BR3 | HAL | KIT | FDA | MBA | MBR |

| | CO.1 | CO.2 | CO.1 CO.2 |
|-----|-------|-------|-----------|
| | (PPM) | (PPM) | |
| BA2 | 4.46 | 1.73 | |
| BR2 | 3.87 | 1.70 | |
| BR3 | 4.09 | 1.73 | |
| HAL | 3.88 | 1.69 | |
| KIT | 12.99 | 1.69 | |
| LDA | 4.61 | 1.71 | |
| MBA | 4.18 | 1.67 | |
| MBR | 3.77 | 1.65 | |

| (PPM) | 1.73 | 1.70 | 1.73 | 1.69 | 1.69 | 1.71 | 1.67 | 1.65 |
|-------|------|------|------|------|-------|------|------|------|
| (PPM) | 4.46 | 3.87 | 4.09 | 3.88 | 12.99 | 4.61 | 4.18 | 3.77 |

| LECEND | | | |
|--------|-------------|--------|-------------|
| VOCI | Burst - UCL | CO.1 | Oven |
| VOC2 | Floor | NO2.1 | Oven |
| VOC3 | Burst - MBR | PART.1 | Oven |
| VOC4 | Burst - LDA | CO.2 | Heater |
| VOC5 | Burst - GAR | NO2.2 | Heater |
| 900A | Burst - KIT | PART,2 | Heater |
| VOC7 | Burst - MBA | CO.3 | Outdoor air |
| VOC8 | Burst - BMT | NO2.3 | Outdoor air |
| VOC9 | Burst - BR3 | PART.3 | Outdoor air |

| PART.3 (μg/m³) 18.68 | PART.3 (µg/m³) 16.43 45.70 47.60 40.18 24.40 44.53 21.86 32.30 | PART.3 (µg/m³) 4.72 24.28 25.98 19.41 10.09 24.12 7.02 12.51 | | |
|---|--|---|---|---|
| NO2.3 (PPM) 0.096 | NO2.3 (PPM) 0.118 0.205 0.225 0.185 0.133 0.213 | NO2.3 (PPM) 0.060 0.111 0.017 0.074 0.012 0.065 | | |
| CO.3 (PPM) 6.69 | CO.3 (PPM) 10.02 11.10 11.26 10.97 10.61 11.21 10.37 | CO.3 (PPM) 6.66 6.72 6.75 6.70 6.66 6.60 | | |
| PART.2 (μg/m³) 11.32 | PART.2 (μg/m³) 12.82 12.97 13.00 12.82 15.32 15.32 15.32 15.32 15.32 15.32 | РАКТ.2 (µg/m³) 10.39 11.45 11.45 11.41 10.94 11.86 10.55 | РАКТ.2 (µg/m³) 11.78 12.54 12.59 12.44 12.07 12.54 11.84 | |
| NO2.2 (PPM) 0.018 | NO2.2 (PPM) 0.076 0.052 0.052 0.068 0.064 0.134 0.072 | NO2.2 (PPM) 0.013 0.014 0.015 0.016 0.026 0.013 | NO2.2 (PPM) 0.028 0.022 0.022 0.021 0.025 0.026 | |
| CO.2 (PPM) 1.93 | CO.2 (PPM) 2.72 2.74 2.78 2.83 2.96 3.66 2.66 | CO.2 (PPM) 2.03 1.83 1.83 1.92 2.00 1.99 1.97 | CO.2 (PPM) 2.26 1.81 1.79 1.84 2.10 2.20 2.20 | Oven Oven Oven Heater Heater Heater Outdoor air Outdoor air |
| PART.1 (μg/m³) 10.85 | РАКТ.1 (µg/m³) 11.44 12.57 12.64 12.48 14.11 12.57 11.62 | PART.1 (μg/m³) 9.80 11.16 11.26 10.96 10.58 11.22 11.22 | РАКТ.1 (µg/m³) 10.98 12.24 12.31 12.14 11.66 12.20 11.16 | CO.1 NO2.1 PART.1 CO.2 NO2.2 PART.2 CO.3 NO2.3 |
| NO2.1 (PPM) 0.020 | NO2.1 (PPM) 0.045 0.037 0.038 0.119 1.042 0.039 0.050 | NO2.1 (PPM) 0.010 0.013 0.019 0.019 0.013 0.011 | NO2.1 (PPM) 0.016 0.016 0.016 0.019 0.060 0.018 | Burst - UCL Floor Burst - MBR Burst - LDA Burst - GAR Burst - KIT Burst - MBA Burst - BMT |
| CO.1 (PPM) 1.99 | CO.1 (PPM) 3.59 2.80 2.84 5.27 28.52 2.83 4.20 | CO.1 (PPM) 1.87 1.70 1.93 3.77 1.69 1.86 | CO.1 (PPM) 2.29 1.76 1.73 1.94 3.77 1.75 2.35 | LEGEND VOC1 VOC2 VOC3 VOC6 VOC6 VOC6 VOC6 VOC6 |
| VOC9 (µg/m³) 153 | VOC9 (µg/m³) 399 253 3319 986 301 264 427 | VOC9 (µg/m³) 152 115 289 175 116 114 114 153 162 | VOC9 (µg/m³) 214 124 409 237 149 123 222 | <u> </u> |
| VOC8 (µg/m³) 325 | VOC8 (µg/m³) 1012 693 693 723 896 755 971 | VOC8 (µg/m³) 476 285 276 308 391 430 354 | VOC8 (µg/m³) 471 225 217 242 369 243 420 | |
| VOC7 (µg/m³) 133 | VOC7 (µg/m³) 172 148 149 141 160 153 9352 | VOC7 (µg/m³) 111 104 103 105 107 103 103 636 134 | VOC7 (µg/m³) 118 105 104 105 112 105 165 | |
| VOC6 (μg/m³) 145 | VOC6 (µg/m³) 334 241 240 559 3773 253 320 | VOC6 (µg/m³) 139 112 112 136 112 112 113 | VOC6 (µg/m³) 178 123 120 148 555 121 172 | |
| VOCS (μg/m³) 176 | OC5 V/m³) 94 88 88 88 94 94 | 1 | | ations |
| VOC1 VOC2 VOC3 VOC4 VOC5 (μg/m³) (μg/m³) (μg/m³) (μg/m³) (μg/m³) (μg/m³) (μg/m³) (μg/m³) (μg/m³) (μg/m²) (μg/ | Centratio VOC4 (µg/m³) 341 243 241 625 596 1286 327 | g concent VOC4 (µg/m³) 143 115 114 114 157 174 174 140 | Concentry VOC4 (µg/m³) 186 124 121 166 215 223 182 | concentra |
| VOC3 (μg/m³) | yeak con VOC3 (μg/m³) 276 210 208 208 205 246 219 913 | 24-hr avg VOC3 (µg/m³) 122 109 108 110 115 115 171 | 4-hr avg VOC3 VOC3 150 117 115 118 134 116 252 | 1-hr avg |
| VOC2 (µg/m³) 3489 | LM zone VOC2 (µg/m³) 6676 5570 5680 6043 4923 6702 | LM zone VOC2 (µg/m³) 4709 2946 2755 3281 4031 2539 4537 | LM zone VOC2 (µg/m³) NA NA NA NA NA NA NA NA NA | LM zone CO.2 (PPM) 2.43 2.00 2.00 2.06 3.39 2.37 |
| VOC1 (µg/m³) 265 | - SIMIMLM zone peak concentrations VOC1 VOC2 VOC3 VOC4 V((µg/m³) (µg/m³) (µ | SIM1MI VOC1 (µg/m³) 107 99 99 99 99 101 | - SIMIMI VOCI (µg/m³) 100 98 99 99 99 99 | - SIM1MLM zone 1-hr avg concentrations CO.1 CO.2 (PPM) (PPM) 2.99 2.43 2.60 2.03 4.80 2.66 2.409 2.76 2.61 3.39 3.23 2.37 |
| 24 hr avg | Table 8b - BA2 BR3 BR3 HAL KIT LDA MBA | Table 8c - SIMIMLM zone 24-hr avg concentrations VOC1 VOC3 VOC3 VOC4 VOC5 VOC1 (VOC2 VOC3 VOC4 VOC5 VOC4 VOC5 VOC4 VOC5 BA2 (107 4709 122 H3) (µg/m³) (µg/m³) (µg/m³) (µg/m³) (µg/m³) (µg/m³) (µg/m³) (µg/m³) 107 4709 122 H3 169 125 H3 BR3 99 2755 108 114 122 HAL 104 3281 110 143 169 (µg/m³) (| Table 8d - SIMIMLM zone 4-hr avg concentrations VOC1 VOC2 VOC3 VOC4 VOC5 VOC1 VOC2 VOC3 VOC4 VOC5 (µg/m³) (µg/m³) | Table 8e - BA2 BR2 BR3 HAL KIT LDA MBA |

| Table 9a | - SIMIN | 1LH over | all 24-hr | avg conce | entrations | | | | | | | | | | |
|-----------|---------|----------|-----------|-----------|------------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|
| | VOCI | VOC2 | VOC3 | VOC4 | VOCS | 900A | VOC7 | VOC8 | V0C9 | CO.1 | NO2.1 | PART.1 | CO.3 | NO2.3 | PART.3 |
| | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (hg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (μg/m³) | (PPM) | (PPM) | (µg/m³) |
| 24 hr avg | 243 | 3171 | 132 | 137 | 131 | 136 | 128 | 333 | 141 | 1.94 | 0.020 | 10.59 | 19.9 | 0.099 | 23.44 |

| | NO2.1 PART.1 CO.3 NO2.3 I | (PPM) (PPM) (µg/m³) (PPM) (µg/m³) | 0.099 10.49 10.29 0.136 | 0.076 12.13 11.15 0.214 | 0.076 12.32 11.31 0.231 | 0.080 12.03 11.09 0.197 | 0.889 12.17 10.34 0.136 | 0.080 12.20 11.23 0.218 | 0.096 10.50 10.31 0.134 | 0.085 1130 1039 0.135 |
|------------|---------------------------|-----------------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-------------------------|-----------------------|
| | CO.3 | (PPM) | 10.29 | 11.15 | 11.31 | 11.09 | 10.34 | 11.23 | 10.31 | 10 39 |
| | PART.1 | (µg/m³) | 10.49 | 12.13 | 12.32 | 12.03 | 12.17 | 12.20 | 10.50 | 11 30 |
| | NO2.1 | (PPM) | 0.099 | 0.076 | 0.076 | 0.080 | 0.889 | 0.080 | 960.0 | 0.085 |
| | CO.1 | (PPM) | 4.91 | 4.12 | 4.05 | 4.39 | 23.57 | 4.20 | 4.87 | 4.63 |
| | VOC9 | (µg/m³) | 413 | 308 | 2211 | 739 | 375 | 329 | 411 | 491 |
| | VOC8 | (µg/m³) | 1285 | 938 | 947 | 1049 | 1230 | 1031 | 1273 | 1142 |
| | VOC7 | (µg/m³) | 242 | 199 | 197 | 509 | 229 | 506 | 6040 | 776 |
| | NOC6 | (µg/m³) | 369 | 294 | 293 | 300 | 2743 | 309 | 361 | 320 |
| ons | VOCS | (µg/m³) | 272 | 228 | 224 | 282 | 316 | 514 | 270 | 265 |
| ncentrativ | V0C4 | (µg/m³) | 365 | 290 | 586 | 336 | 394 | 946 | 326 | 328 |
| e peak co | | (µg/m³) | | | | | | | | 1556 |
| MLH zon | VOC2 | (µg/m³) | 8561 | 4467 | 3891 | 4786 | 7059 | 3559 | 6896 | 7578 |
| - SIMIN | VOC1 VOC2 | (µg/m³) | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 98 |
| Table 9 | | | BA2 | BR2 | BR3 | HAL | KIT | LDA | MBA | MRR |

| | RT.3 | (µg/m³) | .53 | .54 | 4 | .93 | .31 | 09: | .80 | .02 |
|----------------------|--------|---------------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | | | | | | | | | |
| | NO2.3 | (PPM) | 0.070 | 0.117 | 0.123 | 0.103 | 0.077 | 0.115 | 0.068 | 0.079 |
| | CO.3 | (PPM) | 87.9 | 6.63 | 19.9 | 6.63 | 6.73 | 6.63 | 6.81 | 6.71 |
| | PART.1 | $(\mu g/m^3)$ | 99.6 | 11.05 | 11.16 | 10.75 | 10.12 | 10.95 | 9.64 | 10.14 |
| | NO2.1 | (PPM) | 0.014 | 0.016 | 0.016 | 0.016 | 0.062 | 0.016 | 0.013 | 0.013 |
| | CO.1 | (PPM) | 1.94 | 1.75 | 1.73 | 1.81 | 3.10 | 1.76 | 1.94 | 1.87 |
| | VOC9 | (µg/m³) | 144 | 123 | 194 | 153 | 137 | 124 | 14 | 145 |
| | VOC8 | (µg/m³) | 445 | 287 | 279 | 316 | 399 | 300 | 436 | 374 |
| | VOC7 | (µg/m³) | 122 | 112 | Ξ | 114 | 119 | 112 | 324 | 145 |
| | NOC6 | (µg/m³) | 137 | 121 | 120 | 126 | 227 | 122 | 137 | 132 |
| trations | VOC5 | (µg/m³) | 134 | 116 | 115 | 125 | 137 | 4 | 134 | 129 |
| 'g concen | VOC4 | (μg/m³) | 140 | 122 | 121 | 130 | 140 | 149 | 140 | 135 |
| 24-hr av | VOC3 | (μg/m³) | 131 | 118 | 117 | 121 | 128 | 118 | 142 | 178 |
| 1LH zone | VOC2 | (µg/m³) | 4263 | 2533 | 2298 | 2839 | 3858 | 2271 | 4543 | 3920 |
| Table 9c - SIMIMLH z | VOCI | (µg/m³) | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 |
| Table 9c | | | BA2 | BR2 | BR3 | HAL | KIT | LDA | MBA | MBR |

| | VOCI | VOC2 | VOC3 | VOC4 | VOC5 | 900A | VOC7 | VOC8 | VOC9 | CO.1 | NO2.1 | PART.1 |
|------|---------|---------|---------|---------|---------|---------|---------------|---------|---------|-------|-------|---------|
| | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | $(\mu g/m^3)$ | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| 3A2 | 86 | × | 179 | 202 | 207 | 197 | 155 | 811 | 216 | 2.64 | 0.019 | 9.63 |
| BR2 | 86 | Ϋ́ | 147 | 158 | 156 | 157 | 132 | 498 | 163 | 2.19 | 0.018 | 11.05 |
| 3R3 | 86 | Ϋ́ | 143 | 154 | 152 | 152 | 129 | 465 | 394 | 2.12 | 0.018 | 11.23 |
| IAL | 86 | × | 152 | 186 | 161 | 170 | 135 | 534 | 260 | 2.30 | 0.019 | 10.81 |
| E | 86 | ٧N | 173 | 213 | 226 | 504 | 150 | 727 | 200 | 3.08 | 0.035 | 10.01 |
| ΡĄ | 86 | ž | 146 | 243 | 275 | 156 | 131 | 491 | 162 | 2.16 | 0.018 | 11.10 |
| /IBA | 86 | ΥN | 230 | 202 | 506 | 197 | 807 | 800 | 218 | 2.67 | 0.019 | 9.65 |
| ABR | 86 | Ž | 337 | 195 | 198 | 186 | 230 | 879 | 234 | 2.56 | 0.019 | 10.07 |

| ILH zone I-I | | |
|--|------|-------|
| Table 9e - SIMIMLH zone I-hr avg concentration | CO.1 | (PPM) |

| Table 20 Similaria cone in a 6 concent | | | | | | | | | | |
|--|------|------|------|------|------|------|-------|------|------|------|
| 2011 | CO.1 | (PPM | 3.92 | 3.48 | 3.46 | 3.77 | 17.02 | 3.54 | 3.85 | 3.73 |
| , acou | | | BA2 | BR2 | BR3 | HAL | KIT | LDA | MBA | MBR |

| LECEND | | | |
|--------|-------------|--------|-------------|
| VOC1 | Burst - UCL | CO.1 | Oven |
| VOC2 | Floor | N02.1 | Oven |
| VOC3 | Burst - MBR | PART.1 | Oven |
| VOC4 | Burst - LDA | CO.2 | Heater |
| VOC5 | Burst - GAR | NO2.2 | Heater |
| 00Ce | Burst - KIT | PART.2 | Heater |
| VOC7 | Burst - MBA | CO.3 | Outdoor air |
| VOC8 | Burst - BMT | N02.3 | Outdoor air |
| VOC9 | Burst - BR3 | PART.3 | Outdoor air |

| PART.3 (μg/m³) | 4.30 | PART.3 | (µg/m³) | 0.80 | 10.48 | 0.70 | 0.74 | 8 93 | 11.46 | 15.41 | | PART.3 | (µg/m³) | 0.71 | 0.00 | 2.59 | 5.55 4.38 | 4.32 | 5.75 | 9.05 | | | | | | | | | | | | | | | | | | | |
|--|-----------|--------------------------|---------|------------|--------------|-------|-------|-------|-------|-------|-----------|--------|---------------|-------|-------|--------------|--------------|---------------------------|-------|-------|-----------|--------|---------|-------|-------|-------|-------|------------|-----------------------|-----------|-------------|-------|-------------|-------------|-------------------|-------------|-------------|-------------|------|
| NO2.3 (PPM) | Cto.o | NO2.3 | (PPM) | 0.059 | 0.063 | 0.00 | 200.0 | 0.078 | 0.092 | 0.098 | | NO2.3 | (PPM) | 0.035 | 0.049 | 0.039 | 0.040 | 0.0 | 0.049 | 0.057 | | | | | | | | | | | | | | | | | | | |
| CO.3 (PPM) | | CO.3 | (PPM) | 8.24 | 8.30 | 0.00 | 9.34 | 8.35 | 8.35 | 8.72 | | CO.3 | (PPM) | 99.9 | 6.67 | 6,03 | 0.07 | 6.65 | 6.67 | 89.9 | | | | | | | | | | | | | | | | | | | |
| PART.2 (μg/m³) | 1.02 | PART.2 | (µg/m³) | 9.94 | 0.00 | 080 | 0.07 | 10.01 | 10.06 | 10.14 | | PART.2 | $(\mu g/m^3)$ | 7.18 | 7.75 | 7.54 | 7.58 | 7.61 | 7.73 | 8.11 | | PART.2 | (µg/m³) | 0.73 | 8.83 | 8.74 | 8.84 | 8.97 | 9.17 | | | | | | | | | | |
| NO2.2 (PPM) | 200 | NO2.2 | (PPM) | 0.128 | 0.107 | 0.10 | 0.102 | 0.115 | 0.121 | 0.102 | | N02.2 | (PPM) | 0.017 | 0.016 | 0.010 | 0.013 | 0.018 | 0.018 | 0.016 | | NO2.2 | (PPM) | 0.073 | 990'0 | 0.060 | 0.067 | 0.066 | 0.060 | | | | | | | | | | |
| CO.2 (PPM) | C+:7 | C0.2 | (PPM) | 3.06 | 5,90 4.11 | 4.11 | 4.10 | 4.07 | 4.13 | 3.93 | | CO.2 | (PPM) | 2.51 | 2.41 | 2.40 | 24.7 44.0 | 2.43 | 2.43 | 2.36 | | CO.2 | (PPM) | 3.30 | 3.43 | 3.39 | 3.45 | 3.40 | 3.25 | | Oven | Oven | Oven | Heater | Heater | Outdoor air | Outdoor air | Outdoor air | |
| PART.1 (μg/m³) | 600 | PART.1 | (µg/m³) | 0.01 | 6.32 | 737 | 21.8 | 7.39 | 7.71 | 8.33 | | PART.1 | (µg/m³) | 6.30 | 6.98 | 20.0 | 6.86 | 6.79 | 6.92 | 7.37 | | PART.1 | (µg/m³) | 6.12 | 6.43 | 6.43 | 6.45 | 6.61 | 7.00 | | CO.1 | N02.1 | PART.1 | CO.2 | PART 2 | CO.3 | | PART.3 | |
| NO2.1 (PPM) | 200 | N02.1 | (PPM) | 0.121 | 0.102 | 0.107 | 0.607 | 0.126 | 0.115 | 0.098 | | NO2.1 | (PPM) | 0.015 | 0.014 | 0.014 | 0.013 | 0.016 | 0.015 | 0.015 | | NO2.1 | (PPM) | 0.027 | 0.026 | 0.026 | 0.040 | 0.027 | 0.025 | | Burst - UCL | Floor | Burst - MBR | Burst - LDA | Burst - CAK | Burst - MBA | Burst - BMT | Burst - BR3 | |
| CO.1 (PPM) | 61.7 | CO.1 | (PPM) | 5.30 | 5.50 | 5.30 | 16.44 | 5.98 | 5.68 | 5.22 | | CO.1 | (PPM) | 2.80 | 2.66 | 47.7 CT C | 3.54 | 2.72 | 5.69 | 2.60 | | CO.1 | (PPM) | 3.90 | 4.09 | 4.12 | 4.53 | 40.4 | 3.86 | FGEND | VOCI | VOC2 | VOC3 | VOC4 | 000 000 000 | VOC7 | VOC8 | V0C9 | |
| VOC9 (µg/m³) | 001 | V0C9 | (µg/m³) | 363 | 3067 | 307 | 378 | 376 | 382 | 342 | | V0C9 | (µg/m³) | 183 | 169 | 505 170 | 175 | 171 | 173 | 164 | | V0C9 | (mg/m³) | 234 | 639 | 261 | 249 | 238 | 229 | _ | | | | | | | | | |
| VOC8 (µg/m³) | 07/ | VOC8 | (µg/m³) | 1447 | 1550 | 1523 | 1565 | 1485 | 1549 | 1402 | | VOC8 | (µg/m³) | 826 | 50/ | 753 | 756 | 726 | 739 | 999 | | VOC8 | (µg/m³) | 1101 | 1193 | 1173 | 1213 | 1139 | 1068 | | | | | | | | | | |
| VOC7 (µg/m³) | G C | V0C7 | (µg/m³) | 300 | 327 | 481 | 328 | 331 | 6987 | 1052 | | V0C7 | (μg/m³) | 02: | 158 | <u> </u> | 163 | 91 | 421 | 210 | | V0C7 | (µg/m³) | 200 | 219 | 254 | 221 | 217 | 363 | | | | | | | | | | |
| 1S VOC6 (μg/m³) | | 900A | (µg/m³) | 370 | 390 | 537 | 3104 | 420 | 394 | 348 | | 900A | (µg/m³) | 185 | 0 2 | 1/0 | 299 | 174 | 174 | 165 | | 900A | (µg/m³) | 236 | 249 | 270 | 631 | 242 | 231 | | | | | | | | | | |
| VOC5 (µg/m³) | | VOC5 | (µg/m³) | 300 | 423 | 455 | 433 | 762 | 426 | 392 | ntrations | VOC5 | (μg/m³) | 267 | 239 | 757 | 253 | 311 | 246 | 230 | trations | VOCS | (µg/m³) | 336 | 358 | 367 | 371 | 360 | 328 | rations | | | | | | | | | |
| voc4 (µg/m³) | ncentrati | VOC4 | (µg/m³) | 355 | 374 | 463 | 30, | 1182 | 381 | 334 | vg conce | V0C4 | (µg/m³) | 98: | 1/1 | 181 | 179 | 211 | 175 | 166 | g concen | VOC4 | (µg/m³) | 236 | 249 | 264 | 260 | 357 | 231 | g concen | ۵ | | | | | | | | |
| rall 24-h VOC3 (μg/m³) | e neak co | VOC3 | (µg/m³) | 360 | 380 | 623 | 378 | 380 | 392 | 2073 | e 24-hr a | V0C3 | (µg/m³) | 182 | 16/ | 5 20 | 173 | 169 | 172 | 241 | e 4-hr av | V0C3 | (µg/m³) | 231 | 244 | 292 | 247 | 250 | 473 | e 1-hr av | | | | | | | | | |
| MTC ove VOC2 (µg/m³) | MTC zon | VOC2 | (µg/m³) | 6328 | 6145 | 5983 | 9085 | 5581 | 5458 | 5135 | MTC zon | V0C2 | (µg/m³) | 5530 | 4967 | 2866 | 5206 | 4859 | 4923 | 4729 | MTC zon | V0C2 | (µg/m³) | Z Z | Ϋ́ | Ν | ×: | ₹ 2 | Y V | MTC zon | CO.2 | (PPM) | 2.13 | 2.08 | 2.12 | 2.08 | 2.16 | 2.06 | 2.02 |
| a - SIMII VOCI (μg/m³) | IMIS-C | V0C1 | (µg/m³) | 8 8 | 8 8 | 2 % | 2 8 | 86 | 86 | 86 | s - SIMII | V0C1 | $(\mu g/m^3)$ | 8 8 | 8 8 | 8 8 | 8 8 | 8 % | 86 | 98 | 1 - SIM11 | VOCI | (µg/m³) | 8 8 | 86 | 86 | 8 8 | 8 8 | 88 | s - SIMII | CO.1 | (PPM) | 4.67 | 4.24 | 4.33 | 14.42 | 4.81 | 4.54 | 4.14 |
| Table 10a - SIM1MTC overall 24-hr avg concentrations VOC1 VOC2 VOC3 VOC4 VOC5 VOC4 VOC6 VOC6 VOC6 VOC6 VOC6 VOC6 VOC6 VOC6 | Table 10 | VOC1 VOC2 VOC3 VOC4 VOC5 | | BA2 BD2 | BR3 | HAI | E | LDA | MBA | MBR | Table 100 | | | BA2 | BK2 | BRS | X | LDA 98 4859 169 211 311 1 | MBA | MBR | Table 100 | | DAJ | BR2 | BR3 | HAL | KIT. | MBA | MBR 98 NA 473 231 328 | Table 10k | CO.1 CO.2 | | BA2 | BR2 | HAI. | KT | LDA | MBA | MBK |

| CO.2 NO2.2 PART.2 CO.3 NO2.3 | 1 ³ (PPM) (PPM) (μg/n1 ³) (PPM) (PPM) (μg/m3) (2.79 0.012 8.91 6.72 0.041 6.67 | | CO.2 NO2.2 PART.2 CO.3 NO2.3 | (PPM) (PPM) (µg/m³) (PPM) (PPM) | 3.50 0.084 11.03 8.12 0.046 | 3.38 0.063 11.58 8.88 0.084 | 3.37 0.064 11.56 9.05 0.094 | 3.45 0.050 11.34 8.85 0.070 | 3.48 0.071 11.03 8.46 0.045 | 3.87 0.076 11.87 9.20 0.103 | 3.49 0.079 10.82 8.09 0.044 6.87 | 3 47 0 050 10 70 8 32 0 0 048 |
|------------------------------|---|-----------|------------------------------|---------------------------------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|-----------------------------|----------------------------------|-------------------------------|
| _ | (PPM) (μg/m³) 0.021 7.84 | | _ | | | | | | | | 0.060 8.42 | |
| C0.1 | (PPM) 2.85 | | CO.1 | (PPM) | 5.22 | 4.11 | 4.14 | 8.41 | 44.53 | 4.34 | 2.07 | 5 33 |
| VOC9 | (µg/m³) 270 | | V0C9 | (µg/m³) | 494 | 377 | 4320 | 801 | 425 | 406 | 454 | 210 |
| VOC8 | (μg/m³) 1144 | | VOC8 | (µg/m³) | 1944 | 1617 | 1603 | 1655 | 1833 | 1630 | 1917 | 1704 |
| VOC7 | (μg/m³) 231 | | VOC7 | (µg/m³) | 301 | 264 | 263 | 564 | 287 | 264 | 11599 | 1193 |
| | (μg/m³) 254 | | | _ | | | | | | | 448 | |
| VOC5 | (μg/m³) 295 | tions | VOCS | (µg/m³) | 427 | 351 | 348 | 290 | 604 | 959 | 408 | 424 |
| | (μg/m³) 257 | | VOC4 | (µg/m³) | 467 | 375 | 379 | 731 | 534 | 1721 | 450 | 430 |
| VOC3 | | ne peak c | VOC3 | (µg/m³) | 424 | 339 | 341 | 323 | 379 | 353 | 730 | 3046 |
| VOC2 | (μg/m³) 10674 | MTM zo | VOC2 | (µg/m³) | 14022 | 11897 | 12009 | 12553 | 13682 | 09111 | 14489 | 14684 |
| VOCI | (μg/m³) 526 | b - SIMI | VOCI | (µg/m³) | 316 | 611 | 119 | 267 | 126 | 123 | 131 | 108 |
| | 24 hr avg | Table 11 | | | BA2 | BR2 | BR3 | HAL | KIT | LDA | MBA | MRR |

| | - | _ | | | | | | | | |
|------------|----------------------------|---------|-------|-------|-------|-------|-------|-------|-------|-------|
| | PART. | (µg/m³) | 1.07 | 8.83 | 9.51 | 5.56 | 2.37 | 10.38 | 1.47 | 2.63 |
| | NO2.3 | (PPM) | 0.023 | 0.048 | 0.051 | 0.037 | 0.027 | 0.055 | 0.023 | 0.025 |
| | CO.3 | (PPM) | 6.72 | 6.72 | 6.74 | 6.72 | 6.71 | 6.74 | 6.70 | 6.68 |
| | PART.2 | (µg/m³) | 8.14 | 6.07 | 9.19 | 8.90 | 8.42 | 9.70 | 8.09 | 8.24 |
| | NO2.2 | (PPM) | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 | 0.017 | 0.010 | 0.008 |
| | CO.2 | (PPM) | 2.99 | 2.65 | 2.65 | 2.79 | 2.92 | 2.78 | 2.95 | 2.87 |
| | PART.1 | (µg/m³) | 6.90 | 8.15 | 8.27 | 7.84 | 19.7 | 8.46 | 6.89 | 7.15 |
| | NO2.1 | (PPM) | 0.009 | 0.008 | 0.00 | 0.019 | 0.113 | 0.009 | 0.008 | 0.010 |
| | CO.1 | (PPM) | 2.68 | 2.31 | 2.30 | 2.82 | 90.9 | 2.28 | 2.66 | 2.69 |
| | VOC9 | (µg/m³) | 262 | 208 | 544 | 290 | 238 | 199 | 259 | 265 |
| | VOC8 | (µg/m³) | 1397 | 1068 | 1050 | 1139 | 1297 | 1024 | 1380 | 1278 |
| | VOC7 | (µg/m³) | 192 | 991 | 164 | 172 | 183 | 091 | 1054 | 306 |
| | 900A | (µg/m³) | 246 | 200 | 197 | 246 | 280 | 195 | 244 | 241 |
| entrations | VOC5 | (µg/m³) | 288 | 230 | 227 | 292 | 312 | 352 | 283 | 284 |
| ovg conc | VOC4 | (µg/m³) | 254 | 202 | 504 | 254 | 566 | 302 | 252 | 249 |
| nc 24-nr | VOC3 | (µg/m³) | 219 | 185 | 183 | 192 | 202 | 177 | 275 | 435 |
| M I M 201 | VOC2 | (µg/m³) | 11788 | 9704 | 9391 | 10512 | 11433 | 8585 | 12025 | 12037 |
| c - SIMI | VOCI | (µg/m³) | 120 | 104 | 103 | 115 | 105 | 103 | 107 | Ξ |
| l able 11 | VOC1 VOC2 VOC3 VOC4 VOC5 V | | BA2 | BR2 | BR3 | HAL | KIT | LDA | MBA | MBR |
| | | | | | | | | | | |

| _ | d - SIMI | MTM zo. | | vg concer | ntrations | | | | | | | | | | |
|---|----------|-----------|------|-----------|---------------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|
| | VOCI | VOC1 VOC2 | VOC3 | VOC4 | VOCS | VOC6 | VOC7 | VOC8 | VOC9 | CO.1 | NO2.1 | PART.1 | CO.2 | NO2.2 | PART.2 |
| | (µg/m³) | (µg/m³) | | (µg/m³) | $(\mu g/m^3)$ | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| | 108 | N N | | 343 | 344 | 337 | 222 | 1344 | 368 | 4.04 | 0.023 | 8.07 | 2.99 | 0.033 | 9.47 |
| | 102 | ٧ | | 231 | 219 | 228 | 171 | 830 | 234 | 2.83 | 0.017 | 9.87 | 2.43 | 0.025 | 10.70 |
| | 102 | ٧ | | 224 | 214 | 221 | 168 | 961 | 933 | 2.76 | 0.017 | 10.07 | 2.40 | 0.025 | 10.90 |
| | <u>5</u> | N N | | 323 | 383 | 316 | 176 | 911 | 416 | 3.91 | 0.034 | 9.64 | 2.52 | 0.024 | 10.45 |
| | 104 | V. | | 373 | 435 | 1037 | 202 | 1160 | 293 | 9.51 | 0.137 | 9.29 | 2.81 | 0.029 | 9.85 |
| | 102 | ٧× | | 419 | 295 | 211 | 191 | 778 | 215 | 2.68 | 0.017 | 10.29 | 2.42 | 0.028 | 11.20 |
| | 107 | ٧ | | 340 | 332 | 334 | 2020 | 1357 | 363 | 4.06 | 0.021 | 7.81 | 2.98 | 0.030 | 9.15 |
| | 901 | ٧ | | 330 | 346 | 324 | 496 | 1152 | 379 | 4.16 | 0.025 | 8.45 | 2.75 | 0.024 | 9.44 |

| | CO.1 | CO.2 | |
|-----|-------|-------|-------------|
| | (PPM) | (PPM) | (PPM) (PPM) |
| BA2 | 2.67 | 3.03 | |
| BR2 | 2.43 | 2.76 | |
| BR3 | 2.46 | 2.73 | |
| HAL | 5.98 | 3.10 | |
| KIT | 34.20 | 3.08 | |
| LDA | 2.49 | 3.62 | |
| MBA | 2.46 | 3.01 | |
| MBR | 3.13 | 2.99 | |

|--|

| VOC5 | VOC4 | VOC4 |
|---------|---------|--------------------------|
| (µg/m³) | (μg/m³) | (μg/m³) |
| 205 | 232 | 232 |
| | | VOC3 (μg/m³) (227 |

| Table 1 | 2b - SIMI | MIH ZO | ne peak c | concentrat | lons | | | | | | | | | | |
|---------|---------------|---------|-----------|------------|---------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|
| | VOC1 VOC2 | VOC2 | | V0C4 | VOC5 | 900A | VOC7 | VOC8 | V0C9 | CO.1 | N02.1 | PART.1 | CO.3 | NO2.3 | PART.3 |
| | $(\mu g/m^3)$ | (µg/m³) | | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| BA2 | 86 | 17962 | | 476 | 296 | 491 | 414 | 2195 | 495 | 5.80 | 0.121 | 6.81 | 8.62 | 0.060 | 9.92 |
| BR2 | 86 | 12331 | | 423 | 273 | 435 | 381 | 1972 | 437 | 5.25 | 0.103 | 9.33 | 9.02 | 0.000 | 16.85 |
| BR3 | 86 | 11254 | | 423 | 272 | 435 | 380 | 1992 | 2863 | 5.26 | 0.104 | 9.79 | 9.18 | 0.100 | 18.47 |
| HAL | 86 | 12252 | | 467 | 326 | 464 | 391 | 2056 | 889 | 5.73 | 0.104 | 9.19 | 8.78 | 0.071 | 11.52 |
| KIT | 86 | 15709 | | 477 | 338 | 3169 | 406 | 2158 | 485 | 27.39 | 1.028 | 9.12 | 8.63 | 0.058 | 9.44 |
| LDA | 86 | 10416 | 431 | 1194 | 208 | 478 | 384 | 2024 | 455 | 5.70 | 0.120 | 10.16 | 9.31 | 0.107 | 20.27 |
| MBA | 86 | 20365 | | 471 | 294 | 485 | 7540 | 2188 | 489 | 5.73 | 0.118 | 6.75 | 8.59 | 0.058 | 9.74 |
| MBR | 86 | 17774 | | 440 | 292 | 451 | 1209 | 2105 | 459 | 5.43 | 0.104 | 7.04 | 8.56 | 0.054 | 10.02 |

| Table 1. | 2c - SIM1 | MTH 201 | ne 24-hr a | avg conce. | ntrations | | | | | | | | | | | |
|----------|---------------|---------|---------------|---------------|-----------|---------|---------|---------|---------------|-------|-------|---------|-------|-------|---------|--|
| | VOC1 VOC2 | VOC2 | Ι. | VOC4 | VOCS | 900A | VOC7 | VOC8 | VOC9 | CO.1 | NO2.1 | PART.1 | CO.3 | NO2.3 | PART.3 | |
| | $(\mu g/m^3)$ | (µg/m³) | $\overline{}$ | $(\mu g/m^3)$ | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | $(\mu g/m^3)$ | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | |
| BA2 | 86 | 10703 | | 247 | 506 | 244 | 224 | 1229 | 250 | 2.90 | 0.013 | 6.39 | 7.10 | 0.029 | 4.90 | |
| BR2 | 86 | 8615 | | 213 | 170 | 210 | 195 | 626 | 214 | 2.53 | 0.013 | 7.78 | 6.82 | 0.051 | 11.21 | |
| BR3 | 86 | 8217 | 202 | 209 | 991 | 207 | 192 | 930 | 318 | 2.48 | 0.013 | 7.95 | 6.77 | 0.055 | 12.03 | |
| HAL | 86 | 9052 | | 226 | 504 | 223 | 202 | 1019 | 244 | 2.67 | 0.014 | 7.42 | 6.83 | 0.040 | 7.48 | |
| KIT | 86 | 10245 | | 240 | 216 | 344 | 215 | 1144 | 239 | 4.27 | 0.068 | 6.93 | 6.99 | 0.031 | 5.35 | |
| LDA | 86 | 7433 | | 238 | 230 | 504 | 188 | 106 | 506 | 2.46 | 0.014 | 8.08 | 6.74 | 0.057 | 12.57 | |
| MBA | 86 | 11316 | | 252 | 207 | 249 | 484 | 1266 | 254 | 2.98 | 0.012 | 6.17 | 7.19 | 0.028 | 4.72 | |
| MPD | 80 | 10069 | | 243 | 206 | 230 | 276 | 1176 | 346 | 200 | 0.010 | 75 7 | 7.06 | 0000 | 4 0.7 | |

| Table 1 | 2d - SIMI | MTH zor | ne 4-hr av | 'g concen | trations | | | | | | | |
|---------|---------------|---------|------------|-----------|----------|---------|---------|---------|---------|-------|-------|---------|
| | V0C1 | VOC2 | VOC3 | VOC4 | V0C5 | 900A | V0C7 | VOC8 | VOC9 | CO.1 | NO2.1 | PART.1 |
| | $(\mu g/m^3)$ | (µg/m³) | (µg/m³) | (mg/m³) | (µg/m³) | (µg/m³) | (μg/m³) | (μg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| BA2 | 86 | Ϋ́ | 326 | 337 | 254 | 338 | 300 | 1598 | 349 | 4.16 | 0.026 | 6.41 |
| BR2 | 86 | NA | 287 | 295 | 218 | 297 | 265 | 1305 | 303 | 3.73 | 0.024 | 7.51 |
| BR3 | 86 | ΝA | 281 | 289 | 215 | 290 | 260 | 1268 | 629 | 3.65 | 0.024 | 7.71 |
| HAL | 86 | ΝA | 298 | 327 | 569 | 324 | 274 | 1362 | 388 | 3.98 | 0.027 | 7.11 |
| KIT | 86 | ΝA | 319 | 342 | 272 | 703 | 293 | 1527 | 343 | 4.83 | 0.047 | 6.67 |
| LDA | 86 | ΝA | 275 | 398 | 383 | 293 | 254 | 1230 | 293 | 3.61 | 0.025 | 7.89 |
| MBA | 86 | Ν | 355 | 339 | 251 | 340 | 1138 | 1604 | 349 | 4.19 | 0.026 | 6.34 |
| MBR | 86 | Ν | 581 | 335 | 251 | 336 | 476 | 1530 | 352 | 4.20 | 0.026 | 6.42 |

| Table 12e - SIM1MTH zone 1-hr avg concentrations | | | | | | | | | |
|--|------|-------|------|------|------|------|-------|------|------|
| 2e - SIMI | CO.1 | (PPM) | 4.15 | 3.81 | 3.84 | 4.31 | 19.10 | 4.12 | 4.06 |
| Table 1 | | | BA2 | BR2 | BR3 | HAL | КП | LDA | MBA |
| | | | | | | | | | |

| LEGEND | 0 | | |
|--------|-------------|--------|-------------|
| VOCI | Burst - UCL | CO.1 | Oven |
| VOC2 | Floor | NO2.1 | Oven |
| VOC3 | Burst - MBR | PART.1 | |
| V0C4 | Burst - LDA | CO.2 | |
| VOCS | Burst - GAR | NO2.2 | Heater |
| 900A | Burst - KIT | PART.2 | Heater |
| V0C7 | Burst - MBA | CO.3 | Outdoor air |
| VOC8 | Burst - BMT | NO2.3 | Outdoor air |
| VOC9 | Burst - BR3 | PART.3 | Outdoor air |

| | _ | | , | | _ | _ | | | _ | | | | | | | | | _, |
|-------------------|--------|------------------|------|--|--------|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | PART.3 | (µg/m³) | | | PART.3 | (mg/m ₃) | 8.28 | 1.51 | 30.38 | 32.69 | 37.53 | 35.29 | 31.87 | 33.37 | 30.18 | 27.91 | 7.17 | 17.67 |
| | NO2.3 | (PPM) | | | N02.3 | (PPM) | 0.120 | 0.127 | 0.200 | 0.179 | 0.217 | 0.226 | 0.196 | 0.193 | 0.182 | 0.191 | 0.120 | 0.131 |
| | CO.3 | (PPM) | | | CO.3 | (PPM) | 19.6 | 9.78 | 10.40 | 10.38 | 10.92 | 10.33 | 10.55 | 10.36 | 10.28 | 10.15 | 9.62 | 9.90 |
| | PART.2 | (µg/m³) | | | PART.2 | (µg/m³) | 10.65 | 10.61 | 11.88 | 11.99 | 12.28 | 12.13 | 11.74 | 11.98 | 11.99 | 11.88 | 10.63 | 11.21 |
| | N02.2 | (PPM) | | | NO2.2 | (PPM) | 0.014 | 0.015 | 0.020 | 0.018 | 0.022 | 0.023 | 0.023 | 0.019 | 0.021 | 0.019 | 0.014 | 0.014 |
| | CO.2 | (PPM) | | | CO.2 | (PPM) | 2.31 | 2.19 | 2.52 | 2.52 | 5.66 | 2.51 | 2.57 | 2.50 | 2.50 | 2.45 | 2.30 | 2.37 |
| | PART.1 | (µg/m³) 10.87 | | | PART.1 | (µg/m³) | 10.73 | 10.73 | 11.89 | 11.99 | 12.28 | 12.32 | 11.76 | 11.97 | 12.93 | 11.94 | 10.73 | 11.22 |
| | N02.1 | (PPM) 0.019 | | | N02.1 | (PPM) | 0.064 | 0.073 | 0.055 | 0.056 | 0.057 | 0.155 | 0.061 | 0.050 | 0.486 | 0.076 | 0.064 | 0.038 |
| į | C0.1 | (PPM) 2.26 | | | CO.1 | (PPM) | 4.22 | 3.78 | 3.35 | 3.39 | 3.47 | 7.21 | 5.45 | 2.00 | 15.55 | 5.73 | 3.92 | 4.49 |
| | VOC9 | (µg/m³) | | | VOC9 | (µg/m³) | 304 | 271 | 188 | 4046 | 235 | 167 | 203 | 632 | 178 | 168 | 279 | 377 |
| | VOC8 | (µg/m³) | | | VOC8 | (µg/m³) | 18 | 991 | 165 | 162 | 153 | 228 | 457 | 297 | 452 | 981 | 168 | 188 |
| | V0C7 | (µg/m³) | | | V0C7 | (µg/m³) | 11511 | 529 | 170 | 171 | 185 | 152 | 178 | 464 | 129 | 151 | 216 | 182 |
| | 900x | (µg/m³) | | | 900A | (µg/m³) | 325 | 320 | 244 | 257 | 566 | 629 | 434 | 373 | 1627 | 471 | 314 | 296 |
| entranons | VOCS | (µg/m³) 149 | | suc | VOCS | (µg/m³) | 412 | 700 | 146 | 153 | 234 | 211 | 1234 | 853 | 153 | 1525 | 372 | 548 |
| avg conc | VOC4 | (µg/m³) | 3 | Table 13b - SIM2FLC zone peak concentrations | V0C4 | (µg/m³) | 384 | 259 | 182 | 193 | 226 | 1912 | 855 | 90 | 465 | 1005 | 334 | 498 |
| C Overall 24-nr | VOC3 | (µg/m³) | | peak cor | VOC3 | (µg/m³) | 101 | 108 | 5 | 901 | 101 | 105 | 105 | 129 | 103 | 102 | 879 | 1529 |
| TC OVER | V0C2 | (µg/m³) | | FLC zone | V0C2 | (µg/m³) | 12014 | 14271 | 6456 | 6820 | 9859 | 8979 | 7662 | 6514 | 6064 | 8057 | 12781 | 8299 |
| able 13a - SIMZFL | V0C1 | (µg/m³) | | SIM2I | V0C1 | (µg/m³) | 461 | 120 | 901 | 801 | 8 | 108 | 154 | 126 | 105 | 118 | 114 | 116 |
| 1 able 1 35 | | 24 hr avo | 9.00 | Table 131 | | | BA2 | BA3 | BR2 | BR3 | BR4 | DR | ENT | HAL | ΚFΛ | E E | MBA | MBR |
| | | | | | | | | | | | | | | | | | | |

| | _ | | | | | | | | _ | | _ | | _ | _ |
|------------|--------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | PART.3 | (µg/m³) | 3.47 | 0.91 | 19.84 | 16.80 | 17.01 | 25.71 | 15.18 | 16.50 | 21.48 | 17.82 | 3.03 | 10.15 |
| | N02.3 | (PPM) | 0.056 | 0.050 | 0.101 | 0.093 | 0.095 | 0.114 | 0.087 | 0.092 | 0.104 | 0.092 | 0.053 | 690.0 |
| | CO.3 | (PPM) | 6.79 | 6.78 | 97.9 | 6.71 | 6.78 | 89.9 | 6.73 | 6.78 | 6.70 | 6.70 | 18.9 | 6.81 |
| | PART.2 | (µg/m³) | 10.13 | 69.6 | 11.33 | 11.18 | 11.21 | 11.65 | 11.13 | 11.21 | 11.48 | 11.29 | 10.05 | 10.70 |
| | NO2.2 | (PPM) | 900.0 | 0.005 | 0.010 | 0.000 | 0.010 | 0.011 | 0.009 | 0.009 | 0.011 | 0.009 | 0.005 | 0.00 |
| | CO.2 | (PPM) | 1.61 | 09:1 | 99.1 | 1.59 | 1.61 | 1.58 | 09.1 | 1.61 | 1.59 | 1.59 | 191 | 1.62 |
| | PART.1 | (µg/m³) | 10.17 | 9.74 | 11.35 | 11.20 | 11.23 | 11.72 | 11.17 | 11.24 | 11.62 | 11.35 | 10.09 | 10.74 |
| | N02.1 | (PPM) | 0.011 | 0.011 | 0.013 | 0.013 | 0.013 | 0.024 | 0.016 | 0.015 | 0.047 | 0.017 | 0.010 | 0.011 |
| | CO.1 | (PPM) | 2.22 | 2.24 | 1.87 | 1.90 | 1.92 | 2.33 | 2.20 | 2.10 | 3.04 | 2.24 | 2.20 | 2.12 |
| | VOC9 | (µg/m³) | 163 | 144 | 111 | 536 | 123 | Ξ | 111 | 173 | 113 | 113 | 158 | 163 |
| | VOC8 | (mg/m³) | 121 | 119 | 10 | 110 | 108 | 120 | 140 | 123 | 14 | 911 | 119 | 120 |
| | V0C7 | (µg/m³) | 1336 | 135 | 113 | 115 | 116 | 108 | 113 | 126 | 110 | 0 = | 128 | 119 |
| | 900A | (µg/m³) | 191 | 174 | 128 | 133 | 134 | 189 | 169 | 153 | 569 | 176 | 163 | 153 |
| trations | VOCS | (mg/m³) | 8 | 129 | 108 | 8 | 911 | 9 | 506 | 171 | 108 | 218 | 154 | 172 |
| g concen | V0C4 | (µg/m³) | 16 | 145 | 116 | 118 | 122 | 237 | 200 | 173 | 129 | 210 | 158 | 169 |
| : 24-hr av | V0C3 | (mg/m³) | 101 | 101 | 8 | 8 | 8 | 66 | 8 | 10 | 66 | 66 | 189 | 228 |
| -LC zone | V0C2 | (µg/m³) | 1728 | 8222 | 4375 | 4681 | 4581 | 3657 | 4991 | 4770 | 4010 | 4726 | 8309 | 6353 |
| c - SIM2 | V0C1 | (µg/m³) | 285 | 011 | 103 | 103 | 104 | 101 | 901 | 101 | 102 | 103 | 108 | 901 |
| Table 13 | | | BA2 | BA3 | BR2 | BR3 | BR4 | DR | ENT | HAL | ΚĿΛ | LR | MBA | MBR |
| | | | | | | | | | | | | | | |

| Table | 3d - SIM2 | FLC zone | e 4-hr avg | g concent | rations | | | | | | | | | | | |
|-------|-----------|----------|------------|-----------|---------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|---|
| | VOCI | V0C2 | VOC3 | VOC4 | VOCS | 900x | VOC7 | VOC8 | VOC9 | C0.1 | N02.1 | PART.1 | CO.2 | NO2.2 | PART.2 | _ |
| _ | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | _ |
| BA2 | 377 | × | 103 | 258 | 272 | 221 | 4308 | 153 | 246 | 3.72 | 0.023 | 9.94 | 2.17 | 0.005 | 9.80 | _ |
| BA3 | 112 | ٧ | 103 | 169 | 157 | 208 | 144 | 140 | 156 | 3.63 | 0.023 | 90.6 | 2.12 | 0.003 | 8.92 | _ |
| BR2 | 102 | ٧V | 101 | 128 | 113 | 149 | 117 | 126 | 125 | 2.63 | 0.018 | 11.23 | 2.06 | 0.009 | 11.18 | _ |
| BR3 | 102 | ٧X | 101 | 128 | 115 | 155 | 121 | 124 | 1585 | 2.63 | 0.018 | 11.33 | 2.03 | 0.009 | 11.27 | _ |
| BR4 | 103 | ٧X | 101 | 126 | 911 | 150 | 120 | 118 | 128 | 2.76 | 0.019 | 11.22 | 2.10 | 0.00 | 11.16 | _ |
| DR | 101 | ٧ | 8 | 228 | 115 | 420 | Ξ | 191 | 115 | 5.11 | 890.0 | 11.85 | 86:1 | 0.011 | 11.52 | _ |
| ENT | 104 | ٧X | 8 | 430 | 447 | 295 | 112 | 255 | 911 | 4.27 | 0.037 | 11.19 | 2.07 | 800.0 | 10.97 | _ |
| HAL | <u>10</u> | ٧X | 103 | 347 | 364 | 239 | 129 | 981 | 310 | 3.88 | 0.030 | Ξ.Ξ | 2.10 | 0.008 | 10.93 | |
| ΚFΛ | 101 | ٧X | 8 | 129 | Ξ | 692 | 113 | 258 | 117 | 8.07 | 0.163 | 12.00 | 2.01 | 0.010 | 11.34 | _ |
| Z. | 101 | Ϋ́ | 8 | 478 | 465 | 339 | 9 | 136 | 114 | 4.51 | 0.043 | 11.43 | 2.05 | 0.009 | 11.18 | |
| MBA | 601 | × | 404 | 232 | 246 | 504 | 132 | 142 | 226 | 3.51 | 0.020 | 9.82 | 2.18 | 0.004 | 9.70 | _ |
| MBR | 105 | ٧X | 512 | 315 | 337 | 216 | 117 | 9 | 275 | 3.65 | 0.021 | 10.56 | 2.17 | 9000 | 10.42 | _ |
| | | | | | | | | | | | | | | | | |

| 1-nr avg concenuations | | | BA2 3.36 1.76 | | |
|------------------------|------|-------|---------------|------|-----|
| TLC ZONE | CO.2 | (PPM) | 1.76 | 1.71 | 071 |
| e - 51M2 | CO.1 | (PPM) | 3.36 | 3.52 | , , |
| l anic 13 | | | BA2 | BA3 | 200 |

| Table 13e - SIMZFLC zone 1-hr avg concentrations | , | | | | | | | | | | | | | | |
|--|------|-------|------|------|------|------|------|----------|------|------|-------|----------|------|------|--|
| -LC zone | CO.2 | (PPM) | 1.76 | 1.77 | 1.68 | 1.68 | 1.70 | 1.66 | 1.71 | 1.71 | 1.68 | 1.70 | 1.75 | 1.73 | |
| 3e - SIM21 | CO.1 | (PPM) | 3.36 | 3.52 | 3.14 | 3.16 | 3.27 | 4.98 | 3.40 | 3.23 | 11.90 | 3.56 | 3.27 | 2.94 | |
| apic | | | BA2 | BA3 | BR2 | BR3 | BR4 | DK DK | ENT | HAL | ΚFΛ | ~ | MBA | MBR | |

| VOC1 | Burst - CLO | CO.1 | Oven |
|------------|-------------|--------|-------------|
| V0C2 | Floor | N02.1 | Oven |
| VOC3 | Burst - MBR | PART.1 | Oven |
| V0C4 | Burst - DR | CO.2 | Heater |
| VOC5 | Burst - L.R | N02.2 | Heater |
| 900x | Burst - KFA | PART.2 | Heater |
| V0C7 | Burst - BA2 | CO.3 | Outdoor air |
| 000 000 | Burst - GAR | N02.3 | Outdoor air |
| 000 | Burst - BR3 | PART.3 | Outdoor air |

| Fable 14 | a - SIM2i | FLM ove | rall 24-hr | avg con | centralion | ns | | | | | | | | | |
|-----------|-----------|---------|------------|---------|------------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|
| | VOCI | V0C2 | V0C3 | V0C4 | VOCS | 900A | V0C7 | 800x | 6207 | CO.1 | NO2.1 | PART.1 | CO.3 | N02.3 | PART. |
| | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| 24 hr avg | 189 | 7974 | 135 | 137 | 134 | 145 | 167 | 8 | 153 | 1.94 | 0.017 | 11.22 | 09'9 | 0.092 | 20.38 |

Table 14b - SIM2FLM zone peak concentrations

| _ | _ | _ | _ | | | | | _ | _ | | _ | _ | |
|--------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|----------|-------|-------|
| PART.3 | (µg/m³) | 33.01 | 3.77 | 31.16 | 36.96 | 48.18 | 35.67 | 40.48 | 43.68 | 34.16 | 28.72 | 37.42 | 35.81 |
| NO2.3 | (PPM) | 0.189 | 0.092 | 0.186 | 0.185 | 0.259 | 0.203 | 0.219 | 0.238 | 0.184 | 0.157 | 0.213 | 0.206 |
| CO.3 | (PPM) | 11.20 | 7.93 | 10.73 | 10.13 | 11.92 | 10.56 | 11.56 | 11.56 | 9.53 | 11.08 | 19.11 | 11.62 |
| PART.1 | (µg/m³) | 12.22 | 10.33 | 12.13 | 12.21 | 12.69 | 12.20 | 12.42 | 12.53 | 12.47 | 12.02 | 12.42 | 12.40 |
| NO2.1 | (PPM) | 0.078 | 0.000 | 0.064 | 990.0 | 0.067 | 0.071 | 0.063 | 0.056 | 0.539 | 0.049 | 0.078 | 0.039 |
| CO.1 | (PPM) | 3.19 | 3.50 | 2.86 | 2.95 | 2.96 | 3,43 | 2.89 | 2.86 | 16.60 | 2.94 | 3.18 | 2.87 |
| VOC9 | (µg/m³) | 139 | 140 | 203 | 4174 | 811 | 244 | 471 | 542 | 155 | 360 | 137 | 991 |
| VOC8 | (µg/m³) | 102 | 102 | 101 | 101 | 102 | 102 | 112 | 105 | 011 | 101 | 102 | 102 |
| 7007 | (µg/m³) | 8926 | 141 | 238 | 157 | 911 | 358 | 543 | 648 | 260 | 428 | 123 | 126 |
| 00Ce | (µg/m³) | 151 | 176 | 142 | 143 | 133 | 145 | 136 | 159 | 1685 | 132 | 148 | 123 |
| V0C5 | (µg/m³) | 112 | 611 | 110 | 110 | 108 | 841 | 132 | 119 | 453 | 1347 | 112 | 114 |
| V0C4 | (µg/m³) | 126 | 138 | 121 | 121 | 911 | 2301 | 130 | 118 | 740 | 132 | 124 | 113 |
| V0C3 | (µg/m³) | 113 | 111 | 221 | 148 | 601 | 325 | 529 | 621 | 231 | 396 | 114 | 1323 |
| V0C2 | (mg/m³) | 8960 | 21975 | 6493 | 7895 | 5537 | 8080 | 7190 | 6320 | 11894 | 7409 | 1116 | 7527 |
| V0C1 | (mg/m³) | 278 | 979 | 108 | 601 | 801 | 8 | 500 | 132 | 182 | <u>8</u> | 126 | 123 |
| | | BA2 | BA3 | BR2 | BR3 | BR4 | DR | ENT | HAL | KFA | LR | MBA | MBR |

| (µg/m²) (µg/m²) <t< th=""><th></th><th>-</th><th>V0C7</th><th>800x</th><th>VOC9</th><th>CO.1</th><th>NO2.1</th><th>PART.1</th><th>CO.3</th><th>N02.3</th><th>PART.3</th></t<> | | - | V0C7 | 800x | VOC9 | CO.1 | NO2.1 | PART.1 | CO.3 | N02.3 | PART.3 |
|---|---------|-----|--------------|---------|---------|------------|-------|---------|-------|-------|---------|
| 152 116 102 104 103 104 104 104 105 104 105 | (µg/m³) | _ | (µg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (ug/m³) |
| 388 13935 106 114 102 4340 120 102 102 4705 108 102 102 103 105 105 105 105 105 105 105 105 105 105 | 2 | | 1270 | 8 | 107 | 1.72 | 0.012 | 11.31 | 6.58 | 0.089 | 18.41 |
| 102 4340 120 102 102 4705 108 102 101 2719 100 100 143 4960 135 268 159 3933 136 104 106 3449 138 103 154 4700 138 105 | | 126 | 122 | 8 | 114 | 1.88 | 0.007 | 86.8 | 6.53 | 0.032 | 2.11 |
| 102 4705 108 102 101 2719 100 100 143 4906 135 268 159 3933 136 104 106 138 103 103 134 6617 126 211 154 4700 138 105 | 102 | | 134 | 83 | 113 | 1.67 | 0.011 | 11.59 | 99'9 | 0.099 | 21.35 |
| 101 2719 100 100 143 4966 135 268 159 3933 136 104 106 3449 138 103 154 4700 138 105 | 102 | | 113 | 8 | 713 | 1.67 | 0.011 | 11.48 | 6.65 | 960.0 | 21.07 |
| 143 4960 135 268 159 3933 136 104 106 3449 138 103 134 6617 126 211 154 4700 138 105 | 001 | | 102 | 8 | 101 | <u>2</u> . | 0.015 | 12.09 | 95'9 | 0.131 | 33.23 |
| 159 3933 136 104 106 3449 138 103 134 6617 126 211 154 4700 138 105 | 268 | | 157 | 8 | 811 | 1.75 | 0.012 | 11.46 | 6.65 | 0.089 | 17.98 |
| 106 3449 138 103 134 6617 126 211 154 4700 138 105 | 2 | | 191 | 8 | 130 | 1.67 | 0.013 | 11.77 | 6.59 | 0.110 | 25.79 |
| 134 6617 126 211 154 4700 138 105 | 103 | | 170 | 8 | 138 | 1.65 | 0.014 | 11.89 | 6.58 | 0.118 | 29.31 |
| 154 4700 138 105 | 211 | | 1 | 90 | 113 | 3.21 | 0.046 | 11.13 | 6.72 | 0.072 | 13.93 |
| | 105 | | <u>8</u> | 8 | 126 | 1.69 | 0.011 | 11.54 | 6.62 | 0.091 | 18.31 |
| , 108 4838 103 103 | 103 | | 90 | 8 | 901 | 1.70 | 0.012 | 11.43 | 6.57 | 0.095 | 20.56 |
| 4239 205 102 | 102 | | 105 | 8 | 107 | 1.64 | 0.011 | 11.63 | 6.57 | 0.09 | 22.15 |

| | V0C1 | V0C2 | V0C3 | V0C4 | VOCS | 00C6 | V0C7 | 800x | VOC9 | CO.1 | NO2.1 | PART |
|-----|----------|---------|----------|---------|---------|----------|---------|---------|---------|-------|-------|---------|
| | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| BA2 | 90 | ٧X | 8 | 8 | 8 | 9 | 3223 | 86 | 8 | 2.00 | 0.012 | 12.0 |
| BA3 | <u>1</u> | ٧X | <u>5</u> | 110 | 105 | 120 | 119 | 8 | Ξ | 1.83 | 0.002 | 8.26 |
| BR2 | 8 | ٧ | 174 | 8 | 8 | 8 | 161 | 86 | 101 | 2.07 | 0.010 | 11.7 |
| BR3 | 8 | ٧V | 133 | 8 | 8 | <u>8</u> | 143 | 86 | 2006 | 2.05 | 0.009 | 11.3 |
| BR4 | 86 | ٧X | 86 | 86 | 86 | 8 | 8 | 86 | 86 | 1:90 | 0.015 | 12.4 |
| DR | 184 | Ν | 238 | 443 | 380 | 9 | 277 | 86 | 105 | 2.11 | 0.008 | 11.4 |
| ENT | 201 | ٧× | 237 | 8 | 8 | 8 | 262 | 86 | 901 | 1.95 | 0.014 | 12.2 |
| HAL | 8 | ٧× | 241 | 8 | 8 | 8 | 300 | 86 | 001 | 1.92 | 0.014 | 12.3 |
| KFA | 174 | ٧× | 196 | 480 | 320 | 697 | 218 | 8 | 113 | 8.79 | 0.175 | Ξ |
| ۳ | 193 | ۷× | 544 | 8 | 346 | 8 | 162 | 86 | 102 | 2.05 | 0.010 | 11.8 |
| MBA | 9 | × | 8 | 83 | 8 | 8 | 8 | 86 | 8 | 1.96 | 0.014 | 12.2 |
| MBR | 8 | < Z | 377 | 8 | 8 | 8 | 8 | 86 | 8 | 1 97 | 0.013 | 12.2 |

| f zone 1-hr avg concentratio | | |
|------------------------------|------|--------|
| FLM zone | | |
| 14e - SIM2FLM | 1.00 | (Anna) |
| Table | | |

| 3 | (PPM) | 2.62 | 1.84 | 2.56 | 2.40 | 2.64 | 2.49 | 5.66 | 2.62 | 13.76 | 5.66 | 5.69 |
|---|-------|------|------|------|------|------|------|------|------|-------|----------|------|
| | | BA2 | BA3 | BR2 | BR3 | BR4 | DR | ENT | HAL | KFA | <u> </u> | MBA |
| | | | | | | | | | | | | |

| V0C1 | Burst - CLO | CO.1 | Oven |
|------|-------------|-------|-------------|
| V0C2 | Floor | N02.1 | Oven |
| VOC3 | Burst - MBR | _ | Oven |
| V0C4 | Burst - DR | CO.2 | Heater |
| VOCS | Burst - LR | _ | Heater |
| 00C | Bursi - KFA | _ | Heater |
| VOC7 | Burst - BA2 | _ | Outdoor air |
| VOC8 | Burst - GAR | | Outdoor als |
| 0000 | Burst - BR3 | | Outdoor air |

| | NOCI | VOC2 | VOC3 | VOC4 | VOCS | 900x | VOC7 | 800x | 000 000 | CO.1 | NO2.1 | PART.1 | CO.3 | NO2.3 | PAR |
|--------|---------|---------|---------|---------|----------|---------|---------|---------|------------|-------|-------|---------|-------|-------|---------|
| | (mg/m³) | (µg/m³) | (µg/m³) | (hg/m³) | (µg/nr³) | (mg/m³) | (mg/m³) | (µg/m³) | (hg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| hr ave | 4 | 13042 | 186 | 178 | 178 | 181 | 189 | 102 | 185 | 2.37 | 9100 | 8,49 | 6.93 | 0.063 | 7.9 |

| | NOCI | VOC2 | VOC3 | VOC4 | VOC5 | 900A | VOC7 | 800x | 6007 | CO.1 | NO2.1 | PART.1 | CO.3 | NO2.3 | PART.3 |
|------|---------|---------|---------|---------|---------|---------|---------|---------|------------|-------|-------|---------|-------|-------|---------|
| | (µg/m³) | (mg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m²) | (PPM) | (PPM) | (µg/m³) |
| BA2 | 203 | 13237 | \$ | 404 | 373 | 426 | 1771 | 124 | 394 | 5.82 | 0.123 | 9.46 | 10.00 | 0.119 | 12.20 |
| BA3 | 227 | 13888 | 459 | 436 | 397 | 489 | 469 | 124 | 420 | 6.30 | 0.138 | 9.04 | 9.93 | 0.102 | 1.05 |
| BR2 | 188 | 12399 | 375 | 379 | 341 | 410 | 393 | 123 | 379 | 5,54 | 0.111 | 9.65 | 68.6 | 0.103 | 13.36 |
| BR3 | 261 | 13589 | \$ | 360 | 366 | 438 | 424 | 123 | 3161 | 2.60 | 0.113 | 9.30 | 68.6 | 0.103 | 10.62 |
| BR4 | 188 | 13277 | 403 | 397 | 365 | 437 | 422 | 122 | 382 | 5.30 | 0.107 | 9.82 | 10.00 | 0.131 | 16.86 |
| DR. | 220 | 12860 | 381 | 1799 | 702 | 398 | 418 | 121 | 412 | 5.46 | 0.099 | 10.09 | 10.00 | 0.114 | 15.55 |
| I:NT | 307 | 11544 | 414 | 381 | 343 | 411 | 485 | 129 | 472 | 5.47 | 0.108 | 89:01 | 10.32 | 0.168 | 26.90 |
| IM | 981 | 12202 | 294 | 356 | 328 | 381 | 632 | 120 | 6 0 | 5,14 | 0.097 | 10.06 | 90.01 | 0.140 | 17.84 |
| KFA | 215 | 13914 | 388 | 169 | 553 | 1289 | 410 | 130 | 403 | 11.40 | 0.377 | 9.71 | 9.94 | 0.103 | 9.48 |
| L.R | 246 | 12010 | 383 | 373 | 1402 | 398 | 425 | 121 | 420 | 5.47 | 0.097 | 10.51 | 10.02 | 0.135 | 22.72 |
| MBA | 187 | 13071 | 400 | 389 | 368 | 420 | 429 | 124 | 387 | 5.71 | 0.120 | 9.76 | 10.06 | 0.129 | 14.65 |
| MBR | 167 | 10972 | 1472 | 324 | 286 | 345 | 329 | 911 | 323 | 4.86 | 0.081 | 10.23 | 10 29 | 0 148 | 16.88 |

| | VOCI | VOC2 | VOC3 | VOC4 | VOCS | VOC6 | V0C7 | VOC8 | 0000 | CO.1 | NO2.1 | PART.1 | CO.3 | NO2.3 | PART.3 |
|------|---------|----------------------|---------|---------|---------|---------|----------|---------|---------|-------|-------|---------|-------|-------|---------|
| | (µg/m²) | (µg/n ¹) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (hg/m²) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (mg/m³) |
| BA2 | 191 | 9417 | 185 | 182 | 175 | 187 | 460 | 103 | 186 | 2.44 | 0.016 | 8.22 | 7.00 | 0.058 | 4.18 |
| BA3 | 178 | 1000 | 193 | 189 | 182 | 195 | 198 | 103 | 194 | 2.52 | 0.016 | 7.87 | 7.03 | 0.050 | 0.55 |
| BR2 | 191 | 9223 | 182 | 179 | 172 | 184 | 187 | 103 | 182 | 2.40 | 0.015 | 8.39 | 86.9 | 0.061 | 00.9 |
| BR3 | 165 | 9845 | 187 | 184 | 171 | 681 | 192 | 103 | 312 | 2.45 | 0.015 | 8.08 | 6.9 | 0.053 | 3.16 |
| BR4 | 163 | 9490 | 184 | 180 | 174 | 185 | 188 | 103 | 184 | 2.41 | 0.015 | 8.28 | 6.9 | 0.058 | 5.11 |
| DR | 182 | 9450 | 185 | 225 | 504 | 184 | <u>8</u> | 103 | 981 | 2.43 | 0.015 | 8.43 | 7.03 | 0.058 | 16'5 |
| ENI. | 213 | 8485 | 184 | 173 | 991 | 178 | 188 | 103 | 184 | 2.35 | 0.016 | 8.86 | 6.9 | 0.073 | 10.88 |
| HAL | 156 | 8820 | 161 | 172 | 991 | 171 | 661 | 102 | 195 | 2.33 | 0.014 | 8.69 | 6.97 | 0.065 | 7.86 |
| ΚFΛ | 183 | 9966 | 188 | 504 | 195 | 516 | 193 | 8 | 189 | 2.76 | 0.027 | 8.19 | 7.04 | 0.051 | 3.23 |
| ¥. | 187 | 8980 | 183 | 176 | 516 | 181 | 188 | 103 | 184 | 2.39 | 0.015 | 8.67 | 7.03 | 0.065 | 8.55 |
| MBA | 162 | 8816 | 182 | 179 | 173 | 184 | 187 | 103 | 183 | 2.41 | 0.016 | 8.34 | 6.9 | 0.000 | 4.89 |
| MBR | 147 | 7850 | 226 | 191 | 156 | 165 | 167 | 102 | 20 | 2.23 | 0.014 | 9.25 | 96.9 | 0.075 | 12.09 |

| 3.42 | VOC1 (µg/m³) 172 | VOC2 (µg/m³) NA | VOC3 (µg/m²) 273 | VOC1 VOC2 VOC3 VOC4 (µg/m²) (µg/m²) (µg/m²) (µg/m²) A2 172 NA 273 281 | VOC5 (µg/m²) 253 | VOC6 (µg/m²) 297 | VOC7 (µg/m³) 1173 | VOC8 (µg/m²) 101 | VOC9 (µg/n²) 290 | CO.1 (PPM) 4.30 | 200 | NO2.1 (PPM) 0.047 |
|------|------------------------|-----------------------|------------------------|---|------------------------|------------------------|-------------------------|------------------------|------------------------|-----------------------|------|-------------------------|
| BA3 | 161 | ž | 290 | 300 | 268 | 317 | 312 | <u>=</u> | 309 | 4.57 | õ | 150 |
| 3R2 | 167 | ž | 263 | 272 | 244 | 288 | 282 | 10 | 280 | 4.24 | ŏ | 72 |
| 383 | 172 | ź | 274 | 282 | 254 | 297 | 262 | <u>=</u> | 685 | 4.27 | 0.0 | 45 |
| 3R4 | 691 | ž | 565 | 272 | 246 | 586 | 282 | 8 | 281 | 4.08 | Ö | £3 |
| × | 197 | ž | 277 | 432 | 347 | 290 | 596 | 101 | 294 | 4.31 | 0.0 | 43 |
| .K | 244 | ź | 588 | 263 | 236 | 278 | 300 | 8 | 306 | 4.10 | 0.0 | Ê |
| Į, | 191 | ź | 316 | 526 | 231 | 270 | 326 | 8 | 330 | 3.98 | 0.0 | 9 |
| KFA | 961 | × | 281 | 351 | 313 | 403 | 305 | <u></u> | 300 | 5.33 | 0.0 | 84 |
| × | 207 | ź | 278 | 267 | 404 | 284 | 297 | <u>=</u> | 295 | 4.23 | 0.0 | 12 |
| MBA | 169 | ź | 267 | 275 | 247 | 290 | 285 | 8 | 283 | 4.21 | Ó. | 9 |
| JARR | 153 | ×Z | ASK | 233 | 1110 | 246 | 146 | 201 | 220 | 37.6 | 0.02 | |

| 0.1 | PM) | 53 | 8 | 33 | 39 | 21 | 91 | 22 |
|-----|------|---------------|--------------------------|-------------------------------------|---|---|---|---|
| O | 5 | BA2 4. | BA3 4. | BR2 4. | BR3 4. | BR4 4. | DR 4. | ENT 4. |
| | CO.1 | CO.1 (PPM) | CO.1 (PPM) N2 4.53 | CO.1 (PPM) V2 4.53 V3 4.90 | CO.1 (PPM) (A2 4.53 (A3 4.90 (A2 4.33 | CO.1 (PPM) N2 4.53 N3 4.90 N3 4.39 N3 4.39 | CO.1 (PPM) (PPM) (12 4.33 (2 4.33 (3 4.39 (4 4.21 | CO.1 (PPM) BA.2 4.33 BA.3 4.90 BR.2 4.33 BR.3 4.39 BR.4 4.11 DR.4 4.16 |

| VOCI | Burst - CLO | C0.1 | Oven |
|-------|-------------|--------|-------------|
| X0C2 | Floor | NO2.1 | Oven |
| VOC3 | Burst - MBR | PART.1 | Oven |
| VOC4 | Burst - DR | CO.2 | Heater |
| VOCS | Burst - 1.R | NO2.2 | Heater |
| 9.00 | Burst - KFA | PART.2 | Heater |
| VCX7 | Burst - BA2 | CO.3 | Outdoor air |
| X.X.X | Burst - GAR | NO2.3 | Outdoor air |
| VCKY | Burd - BR1 | PART.3 | Outdox air |

| Table | JC - 311112 | TELL CORE I'll avg concentiations | CEOCIAD |
|-------|-------------|-----------------------------------|----------------|
| | CO.1 | | VOC1 Burst - |
| | (PPM) | | VOC2 Flox |
| BA2 | 4.53 | | VOC3 Burst - 1 |
| BA3 | 4.90 | | VOC4 Burst - |
| BR2 | 4.33 | | VOC5 Burst- |
| BR3 | 4.39 | | VCC Burst |
| BR4 | 4.21 | | VCX7 Burst B |
| J.K | 4.16 | | V(X'N Burst |
| ENT | 4.22 | | VCKW Burd. |
| IV. | 3.99 | | |
| KI:A | 7.74 | | |
| E. | 4.11 | | |
| MBA | 4.46 | MBA 4.46 | |
| MBR | 3.76 | | |
| | | | |

| | PART.3 | (µg/m³) | 5.24 |
|------------|--------|---------|-----------|
| | NO2.3 | (PPM) | 0.034 |
| | CO.3 | (PPM) | 6.49 |
| | PART.2 | (µg/m³) | 7.82 |
| | N02.2 | (PPM) | 0.004 |
| | CO.2 | (PPM) | 1.62 |
| | PART.1 | (µg/m³) | 7.89 |
| | N02.1 | (PPM) | 0.017 |
| | CO.1 | (PPM) | 3.41 |
| | V0C9 | (µg/m³) | 300 |
| | VOC8 | (µg/m³) | 504 |
| | V0C7 | (µg/m³) | 278 |
| ns | 00Ce | (µg/m³) | 325 |
| centration | VOC5 | (µg/m³) | 322 |
| r avg con | V0C4 | (µg/m³) | 337 |
| rall 24-h | VOC3 | (µg/m³) | 214 |
| PTC ove | V0C2 | (µg/m³) | 30356 |
| 5a - SIM | VOCI | (µg/m³) | 2600 |
| Table 16 | | | 24 hr avg |

| | _ | - | | _ | | _ | _ | _ | _ | | | _ | | |
|-----------|--------|---------|-------|-------|-------|-------|-------|-------|-------|----------|-------|-------|-------|-------|
| | PART.3 | (µg/m³) | 2.08 | 0.48 | 12.26 | 12.10 | 15.85 | 15.10 | 14.88 | 11.93 | 10.06 | 9.16 | 2.42 | 4.78 |
| | NO2.3 | (PPM) | 0.045 | 0.049 | 0.088 | 0.071 | 0.095 | 0.104 | 0.093 | 0.073 | 0.073 | 0.073 | 0.045 | 0.046 |
| | CO.3 | (PPM) | 7.76 | 1.67 | 8.33 | 8.37 | 8.69 | 8.27 | 8.55 | 8.26 | 8.20 | 7.99 | 1.77 | 7.87 |
| | PART.2 | (µg/m³) | 7.81 | 7.88 | 9.26 | 9.24 | 89.6 | 9.50 | 9.11 | 00.6 | 9.14 | 8.85 | 7.81 | 8.02 |
| | N02.2 | (PPM) | 9000 | 0.007 | 0.009 | 0.007 | 0.010 | 0.010 | 0.014 | 600.0 | 0.010 | 800.0 | 9000 | 0.005 |
| | CO.2 | (PPM) | 1.96 | 1.95 | 2.05 | 5.06 | 2.11 | 5.06 | 2.31 | 2.08 | 5.09 | 2.00 | 1.95 | 1.98 |
| | PART.1 | (µg/m³) | 7.97 | 8.07 | 9.27 | 9.25 | 9.64 | 9.58 | 8.77 | 8.94 | 10.22 | 8.87 | 7.98 | 8.10 |
| | N02.1 | (PPM) | 0.065 | 0.075 | 0.054 | 0.056 | 0.056 | 0.076 | 0.052 | 0.045 | 0.595 | 0.038 | 0.065 | 0.034 |
| | CO.1 | (PPM) | 5.56 | 2.98 | 4.60 | 4.75 | 4.82 | 8.07 | 5.34 | 4.62 | 19.92 | 5.44 | 5.47 | 4.26 |
| | V0C9 | (µg/ш³) | 430 | 432 | 328 | 2008 | 361 | 291 | 360 | 989 | 307 | 300 | 411 | 405 |
| | VOC8 | (µg/m³) | 586 | 288 | 247 | 761 | 564 | 262 | 96 | 426 | 225 | 273 | 280 | 273 |
| | V0C7 | (µg/m³) | 13893 | 451 | 320 | 340 | 349 | 283 | 342 | 169 | 300 | 288 | 396 | 351 |
| | 900A | (µg/ш³) | 210 | 242 | 401 | 434 | 443 | 300 | 456 | 69 | 5096 | 451 | 205 | 385 |
| ons | VOCS | (µg/m³) | 401 | 328 | 282 | 298 | 311 | 949 | 1380 | <u>8</u> | 419 | 2373 | 366 | 579 |
| ncentrati | V0C4 | (µg/m³) | 420 | 431 | 339 | 361 | 371 | 3198 | 834 | 879 | 993 | 1089 | 410 | 374 |
| e peak co | VOC3 | (µg/m³) | 224 | 230 | 188 | 961 | 201 | 175 | 197 | 351 | 181 | 178 | 745 | 2050 |
| FIC zon | V0C2 | (µg/m³) | 26390 | 27089 | 19706 | 19400 | 18977 | 20469 | 20894 | 20719 | 19654 | 23040 | 27016 | 25423 |
| b - SIM2 | VOCI | (µg/m³) | 288 | 138 | 119 | 121 | 122 | 125 | 233 | 157 | 122 | 142 | 140 | 147 |
| Table 16 | | | BA2 | BA3 | BR2 | BR3 | BR4 | DR | ENT | HAL | KFA | LR | MBA | MBR |
| | | | | | | | | | | | | | | |

| | | - | | _ | _ | | _ | _ | _ | _ | | _ | | _ |
|-----------|--------|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | PART.3 | (µg/m³) | 0.57 | 0.24 | 7.42 | 6.15 | 91.9 | 9.47 | 5.23 | 4.97 | 7.01 | 5.35 | 99.0 | 2.72 |
| | N02.3 | (PPM) | 0.019 | 0.020 | 0.043 | 0.039 | 0.040 | 0.049 | 0.035 | 0.034 | 0.041 | 0.034 | 0.019 | 0.023 |
| | CO.3 | (PPM) | 6.57 | 6.55 | 6.65 | 99.9 | 9.70 | 19.9 | 6.59 | 6.64 | 6.62 | 6.58 | 6.57 | 0.90 |
| | PART.2 | (µg/m³) | 7.14 | 7.11 | 8.50 | 8.34 | 8.36 | 8.74 | 8.16 | 8.11 | 8.54 | 8.15 | 7.14 | 7.45 |
| | NO2.2 | (PPM) | 0.002 | 0.002 | 0.004 | 0.004 | 0.004 | 0.005 | 0.004 | 0.004 | 0.004 | 0.004 | 0.002 | 0.002 |
| | CO.2 | (PPM) | 2. | 1.64 | 1.63 | 1.64 | 1.65 | 1.64 | 1.71 | 1.66 | 1.69 | 29.1 | 20.1 | 1.65 |
| | PART.1 | (µg/m³) | 7.18 | 7.16 | 8.53 | 8.38 | 8.40 | 8.82 | 8.10 | 8.12 | 8.76 | 8.18 | 7.18 | 7.47 |
| | N02.1 | (PPM) | 0.00 | 0.010 | 0.00 | 0.00 | 0.00 | 0.015 | 0.00 | 800.0 | 0.056 | 0.00 | 800.0 | 9000 |
| | CO.1 | (PPM) | 3.35 | 3.45 | 2.87 | 2.97 | 2.97 | 3.43 | 3.06 | 3.00 | 5.24 | 3.15 | 3.31 | 3.04 |
| | 6000 | (mg/m³) | 596 | 287 | 529 | 1034 | 237 | 211 | 241 | 340 | 516 | 526 | 588 | 298 |
| | 800x | (µg/ш ₂) | 206 | 202 | 174 | 178 | 171 | 185 | 273 | 213 | 247 | 161 | 202 | 200 |
| | V0C7 | (µg/m³) | 2335 | 275 | 218 | 526 | 227 | 203 | 227 | 276 | 210 | 216 | 267 | 254 |
| | 900A | (hg/m³) | 326 | 337 | 259 | 569 | 268 | 314 | 284 | 276 | 515 | 230 | 320 | 287 |
| trations | VOCS | (µg/m³) | 287 | 277 | 519 | 224 | 225 | 303 | 443 | 331 | 564 | 269 | 280 | 304 |
| g concen | V0C4 | (µg/ш³) | 303 | 310 | 242 | 249 | 249 | 584 | 323 | 295 | 327 | 429 | 30 | 290 |
| 24-hr av | V0C3 | (mg/m³) | 170 | 171 | 148 | 151 | 151 | 141 | 152 | 174 | 4 | 147 | 283 | 459 |
| TC zone | V0C2 | (µg/m³) | 20782 | 20431 | 15821 | 16388 | 16266 | 15286 | 17436 | 17474 | 16002 | 17655 | 21096 | 20388 |
| : - SIM2l | V0C1 | (µg/m³) | 194 | 120 | Ξ | 112 | 113 | 112 | 125 | 119 | 112 | 115 | 124 | 122 |
| Table 16c | | | BA2 | BA3 | BR2 | BR3 | BR4 | DR | ENT | HAL | KFA | LR | MBA | MBR |
| | | | | | | | | _ | | | | | | |

| VOC | _ | | VOC4 | VOCS | 00Ce | V0C7 | VOC8 | 6000 | CO.1 | NO2.1 | PART.1 | CO.2 | NO2.2 | PART.2 |
|---------|----|-----|---------|---------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|
| n/gu) | _ | _ | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| | | | 329 | 346 | 367 | 7259 | 241 | 343 | 3.94 | 0.019 | 6.70 | 1.93 | 0.001 | 6.65 |
| | | | 328 | 305 | 393 | 302 | 240 | 316 | 4.24 | 0.022 | 6.59 | 1.92 | 0.001 | 6.52 |
| | | | 238 | 221 | 278 | 526 | 187 | 236 | 3.31 | 910.0 | 8.41 | 1.96 | 0.004 | 8.37 |
| | | | 239 | 222 | 285 | 231 | 189 | 2892 | 3.38 | 0.017 | 8.52 | 1.96 | 0.004 | 8.47 |
| | | | 234 | 218 | 279 | 228 | 185 | 237 | 3.44 | 0.017 | 8.56 | 2.01 | 0.004 | 8.50 |
| | | | 1455 | 339 | 528 | 201 | 221 | 500 | 5.97 | 0.049 | 8.90 | 1.96 | 0.004 | 8.60 |
| √T 123 | ٧N | 146 | 555 | 881 | 317 | 219 | 472 | 230 | 3.70 | 0.018 | 7.88 | 2.04 | 0.003 | 7.91 |
| | | | 391 | 280 | 295 | 304 | 304 | 200 | 3.51 | 0.015 | 7.76 | 2.01 | 0.003 | 1.77 |
| KFA 110 | | | 365 | 569 | 1251 | 210 | 410 | 218 | 13.89 | 0.230 | 9.45 | 2.04 | 0.004 | 8.36 |
| | | | 817 | 1235 | 329 | 211 | 213 | 220 | 4.07 | 0.020 | 7.96 | 1.95 | 0.003 | 7.88 |
| _ | | | 314 | 319 | 358 | 284 | 229 | 325 | 3.83 | 0.018 | 69.9 | 1.92 | 0.001 | 6.64 |
| _ | | | 324 | 427 | 204 | 150 | 230 | 360 | 375 | 1100 | 200 | 100 | 000 | 200 |

| - SIM2FTC zone 1-hr avg concentrations | | | | |
|--|------|-------|------|------|
| TC zone | C0.2 | (PPM) | 1.54 | 1.54 |
| e - SIM2F | CO.1 | (PPM) | | 3.67 |
| Table 16 | | | BA2 | BA3 |

| 7.00 | (PPM) | 1.54 | 1.54 | 1.56 | 1.54 | 1.53 | 1.56 | 09:1 | 1.56 | 1.58 | 1.56 | 1.53 | 1 53 |
|------|-------|------|------|------|------|------|------|------|------|-------|------|------|------|
| 2.03 | (PPM) | 3.46 | 3.67 | 3.13 | 3.18 | 3.23 | 3.70 | 3.13 | 3.07 | 13.79 | 5.96 | 3.44 | 100 |
| | | BA2 | BA3 | BR2 | BR3 | BR4 | DR | ENT | HAL | KFA | LR | MBA | MAD |
| | | | | | | | | | | | | | |

| 70CI | Burst - CLO | CO.1 | Oven |
|------|-------------|--------|------------|
| V0C2 | Floor | N02.1 | Oven |
| VOC3 | Burst - MBR | _ | Oven |
| V0C4 | Burst - DR | _ | Heater |
| VOCS | Burst - L.R | _ | Heater |
| 90C | Burst - KFA | | Heater |
| V0C7 | Burst - BA2 | _ | Outdoor at |
| 00C8 | Burst - GAR | N02.3 | Outdoor at |
| 000 | Burst - BR3 | PART.3 | Outdoor at |

| 2 | VOCI | VOC2 | VOC3 | VOC4 | VOCS | 920A | V0C7 | VOC8 | V0C9 | 00.1 | N02.1 | PART.1 | CO.3 | N02.3 | PART.3 |
|--------|---------|---------|---------|---------|---------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|
| | (µg/m³) | (hg/m³) | (mg/m²) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m²) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (mg/m³) |
| hr ave | 1828 | 23498 | 213 | 222 | 228 | 211 | 282 | 901 | 272 | 2.59 | 0.015 | 9.13 | 6.78 | 0.044 | 8.64 |

| Table 1 | 7b - SIM2 | | | | | | | | | | | | | | |
|----------|-----------|---------|---------|---------|---------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|
| | VOCI | V0C2 | VOC3 | VOC4 | VOCS | 900A | V0C7 | VOC8 | V0C9 | C0.1 | NO2.1 | PART.1 | CO.3 | NO2.3 | PART.3 |
| | (mg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m²) | (µg/m³) | (µg/m³) | (µg/m²) | (PPM) | (PPM) | (hg/m²) | (PPM) | (PPM) | (µg/m²) |
| BA2 | 236 | 21076 | 173 | 238 | 208 | 235 | 12903 | 124 | 249 | 3.87 | 0.078 | 10.69 | 9.43 | 0.097 | 15.49 |
| BA3 | 888 | 36409 | 197 | 281 | 243 | 279 | 298 | 124 | 297 | 4.18 | 0.090 | 8.47 | 7.22 | 0.033 | 1.31 |
| BR2 | 150 | 17017 | 216 | 216 | 161 | 215 | 252 | 117 | 246 | 3.32 | 0.062 | 10.02 | 8.78 | 0.082 | 11.93 |
| BR3 | 150 | 18630 | 991 | 223 | 196 | 221 | 232 | 811 | 5374 | 3.43 | 990:0 | 9.87 | 8.47 | 0.074 | 14.95 |
| BR4 | 148 | 16245 | 155 | 202 | 181 | 202 | 500 | 118 | 211 | 3.42 | 990.0 | 99:11 | 10.11 | 0.133 | 24.68 |
| DK CK | 287 | 18201 | 387 | 2777 | 984 | 250 | 345 | 120 | 321 | 3.29 | 0.053 | 6.67 | 8.96 | 0.087 | 14.37 |
| ENT | 328 | 19333 | 179 | 213 | 283 | 202 | 553 | 171 | 443 | 3.39 | 0.060 | 11.37 | 10.12 | 0.113 | 19.59 |
| HAL | 207 | 18377 | 934 | 187 | 202 | 981 | 638 | 14 | 69 | 3.19 | 0.051 | 09:11 | 10.22 | 0.133 | 22.69 |
| KFA | 264 | 25048 | 529 | 860 | 228 | 1911 | 309 | 155 | 280 | 19.69 | 0.591 | 10.07 | 8.29 | 0.067 | 11.83 |
| Z, | 303 | 18320 | 201 | 224 | 1953 | 681 | 41 | 120 | 346 | 3.10 | 0.042 | 10.41 | 9.37 | 0.059 | 8.94 |
| MBA | 991 | 20691 | 182 | 223 | 196 | 520 | 556 | 122 | 235 | 3.87 | 0.078 | 11.73 | 10.52 | 0.140 | 22.45 |
| MBR | 168 | 18961 | 1698 | 174 | 179 | 168 | 224 | 122 | 282 | 2.98 | 0.038 | 11.72 | 10.54 | 0.135 | 21.07 |

| | NOCI | VOC2 | VOC3 | VOC4 | VOCS | VOC6 | VOC7 | VOC8 | VOC9 | CO.1 | NO2.1 | PART.1 | CO.3 | NO2.3 | PART.3 |
|-----|---------|---------|---------|---------|---------|---------|---------|----------|---------|-------|-------|---------|-------|-------|---------|
| | (µg/m³) | (µg/m³) | (mg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (mg/m³) |
| 2 | 156 | 14281 | 139 | 154 | 120 | 152 | 3166 | 90 | 175 | 2.23 | 8000 | 9.22 | 6.97 | 0.043 | 2.80 |
| 3 | 557 | 26445 | 891 | 504 | 193 | 203 | 236 | Ξ | 227 | 2.55 | 9000 | 6.88 | 6.55 | 0.013 | 69.0 |
| BR2 | 127 | 14220 | 165 | 145 | 141 | 4 | 161 | 5 | 165 | 2.11 | 0.007 | 9.26 | 88.9 | 0.043 | 7.99 |
| 3 | 129 | 15092 | 140 | 120 | 145 | 149 | 171 | 105 | 1655 | 2.13 | 0.007 | 6.07 | 97.9 | 0.042 | 8.05 |
| 4 | 119 | 9904 | 122 | 132 | 130 | 131 | 143 | 103 | 140 | 2.00 | 0.009 | 10.27 | 98.9 | 0.067 | 14.55 |
| | 229 | 15696 | 225 | 203 | 388 | 156 | 244 | <u>8</u> | 185 | 2.24 | 9000 | 10.6 | 6.95 | 0.032 | 5.29 |
| _ | 268 | 12081 | 797 | 143 | 154 | 137 | 281 | 91 | 192 | 2.07 | 800.0 | 9.87 | 6.97 | 0.054 | 10.45 |
| _ | 135 | 10890 | 259 | 136 | 139 | 133 | 288 | 901 | 228 | 2.03 | 800.0 | 80.01 | 6.94 | 0.061 | 13.05 |
| _ | 210 | 19163 | 161 | 416 | 306 | 228 | 224 | 112 | 193 | 5.28 | 0.054 | 8.54 | 6.78 | 0.024 | 3.70 |
| | 252 | 14696 | 254 | 155 | 410 | 145 | 270 | 9 | 188 | 2.14 | 0.005 | 9.24 | 10.7 | 0.033 | 5.02 |
| < | 131 | 11236 | 135 | 139 | 137 | 138 | 156 | 105 | 156 | 2.10 | 600.0 | 9.94 | 6.97 | 0.057 | 11.47 |
| 2 | 130 | 10736 | 343 | 130 | 132 | 128 | 151 | 25 | 150 | 1 98 | 8000 | 10.07 | 809 | 0.058 | 11 \$6 |

| | VOCI | V0C2 | VOC3 | V0C4 | VOCS | 00C6 | V0C7 | 800x | 6000 | 1.00 | NO2.1 | PART.1 |
|-----|---------|---------|----------|---------|---------|---------|---------|-------------|---------|-------|-------|---------|
| | (µg/m³) | (µg/m³) | (µg/m²) | (µg/m³) | (µg/ш²) | (µg/m³) | (µg/m²) | (µg/nr³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| BA2 | 120 | ×z | 14 | 120 | 611 | 120 | 7479 | 101 | 128 | 2.07 | 0.007 | 10.52 |
| BA3 | 864 | ٧X | 9 | 193 | 182 | 26 | 223 | 801 | 216 | 2.11 | 0.001 | 6.45 |
| BR2 | 113 | ٧ | 8 | 120 | 811 | 611 | 196 | <u>=</u> | 132 | 2.05 | 0.002 | 9.74 |
| BR3 | 111 | ٧ | 142 | 128 | 125 | 127 | 155 | <u>-</u> 01 | 3786 | 2.03 | 0.004 | 9.18 |
| BR4 | 5 | Ý | 2 | 101 | 92 | 101 | 91 | 8 | 801 | 2.07 | 0.00 | 11.21 |
| DR | 281 | × | 312 | 1001 | 770 | 611 | 282 | <u>10</u> | 143 | 2.07 | 0.002 | 9.43 |
| EM, | 316 | × | 202 | 101 | 801 | 101 | 4 | 8 | 1117 | 2.11 | 0.008 | 11.17 |
| HAL | 901 | Ý | 254 | 105 | 105 | 105 | 467 | 8 | 113 | 2.08 | 0.000 | 11.41 |
| KFA | 260 | Ϋ́ | 504 | 753 | 447 | 1189 | 222 | 5 | 174 | 13.18 | 0.226 | 9.12 |
| LR | 298 | × | 415 | 114 | 825 | 112 | 355 | <u>.</u> | 130 | 2.14 | 0.004 | 10.23 |
| MBA | 107 | ¥ | <u>8</u> | 101 | 101 | 101 | Ξ | 8 | Ξ | 2.08 | 0.010 | 11.54 |
| MBR | 90 | Ž | 697 | 103 | 12 | 20 | 101 | 8 | 103 | 3.00 | 0000 | 11 53 |

| Table 1 /e - SIMZF I M ZORE I III avg concentration | | | | | | | | | | | | | | |
|---|------|-------|------|------|------|------|------|------|------|------|-------|------|------|------|
| /e - SIM12F | CO.1 | (PPM) | 2.29 | 2.12 | 2.13 | 2.11 | 2.41 | 06:1 | 2.43 | 2.45 | 15.11 | 2.11 | 2.52 | 2.52 |
| 1 anne 1 | | | BA2 | BA3 | DR2 | BR3 | BR4 | DR | ENT | HAL | KFA | LR | MBA | MBR |

| | | Burst - (| | 盈 | | | | | Burst - (| |
|---|--------|-----------|------|------|------|------|-----|------|-----------|------|
| 1 | CECEND | 100x | VOC2 | VOC3 | V0C4 | VOCS | 00C | V0C7 | 00C8 | VOC9 |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | ons | | | | | | | | | |

| = | Burst - CLO | | |
|------|-------------|--------|------|
| Ş | Floor | | |
| S | Burst - MBR | PART.1 | Oven |
| 2 | Burst - DR | | |
| SS | Burst - LR | | |
| 200 | Burst - KFA | | |
| 23 | Burst - BA2 | | _ |
| VOC8 | Burst - GAR | | _ |
| වූ | Burst - BR3 | | _ |

| Table 18 | a - SIM2l | TH over | all 24-hr | avg conc | entration | S | | | | | | | | | |
|-----------|-----------|---------|-----------|----------|----------------------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|
| | VOCI | V0C2 | VOC3 | V0C4 | VOC5 | 900A | V0C7 | 00C8 | V0C9 | CO.1 | N02.1 | PART.1 | CO.3 | N02.3 | PART,3 |
| | (mg/m³) | (µg/m³) | (µg/m³) | (hg/m³) | (µg/ш ₃) | (µg/m³) | (µg/m³) | (hg/m³) | (hg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| 24 hr avg | 3979 | 39385 | 370 | 329 | 360 | 329 | 369 | 122 | 367 | 3.92 | 0.015 | 4.94 | 7.00 | 0.024 | 5.89 |

| | VOCI | VOC2 | VOC3 | VOC4 | VOCS | 9000 | V0C7 | VOC8 | VOC9 | CO.1 | N02.1 | PART.1 | CO.3 | NO2.3 | PART. |
|-----|---------|---------|---------|---------|---------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|
| | (µg/m³) | (hg/m³) | (µg/m³) | (µg/m³) | (mg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| Λ2 | 312 | 34060 | 899 | 624 | 583 | 993 | 8491 | 891 | 613 | 6.70 | 0.136 | 5.57 | 8.16 | 0.044 | 4.12 |
| A3 | 339 | 34237 | 615 | 638 | 296 | 069 | 662 | 168 | 628 | 7.03 | 0.147 | 5.34 | 8.16 | 0.035 | 0.28 |
| R2 | 311 | 33445 | 579 | 286 | 263 | 619 | 613 | 991 | 289 | 6.41 | 0.121 | 5.48 | 8.12 | 0.036 | 3.88 |
| 83 | 312 | 34488 | 294 | 919 | 579 | 638 | 630 | 99 | 3636 | 6.44 | 0.124 | 5.56 | 8.11 | 0.036 | 3.17 |
| R4 | 311 | 34373 | 594 | 615 | 579 | 637 | 679 | 165 | 605 | 6.36 | 0.123 | 5.84 | 8.14 | 0.046 | 4.98 |
| × | 337 | 33619 | 579 | 2102 | 626 | 265 | 99 | 168 | 583 | 6.29 | 0.105 | 5.75 | 8.15 | 0.039 | 5.26 |
| M | 518 | 32782 | 297 | 299 | 292 | 613 | 632 | 187 | 910 | 6.49 | 0.121 | 6.54 | 8.37 | 0.072 | 12.24 |
| AL | 304 | 33496 | 174 | 579 | 547 | 866 | 820 | 163 | 808 | 6.20 | 0.108 | 6.03 | 8.29 | 0.051 | 5.75 |
| FΛ | 331 | 34270 | 582 | 826 | 732 | 1464 | 909 | 180 | 287 | 12.35 | 0.399 | 5.95 | 8.14 | 0.035 | 2.93 |
| 2 | 326 | 32917 | 579 | 579 | 1773 | 595 | 09 | 170 | 585 | 6.31 | 0.102 | 91.9 | 8.16 | 0.045 | 8.50 |
| MBA | 310 | 33730 | 280 | 614 | 572 | 655 | 979 | 168 | 604 | 6.57 | 0.132 | 6.12 | 8.37 | 0.055 | 5.89 |
| IBR | 200 | 32125 | 1739 | \$28 | 506 | 545 | 538 | 158 | 523 | 577 | 0.00 | 6 53 | 8 55 | 0.057 | 633 |

| RT.3 | /m3) | 24 | 4 | 8 | 68 | 1.36 | 63 | 3 | 12 | 88 | 28 | 9 | 90 |
|------------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| PA | gr/) | = | 0 | T | 0 | - | - | 4.0 | 2. | 0 | 2. | Ĩ | · |
| N02.3 | (PPM) | 0.00 | 0.017 | 0.021 | 0.018 | 0.020 | 0.020 | 0.028 | 0.022 | 0.017 | 0.033 | 0.022 | 5000 |
| CO.3 | (PPM) | 7.17 | 7.18 | 7.16 | 7.18 | 7.18 | 7.18 | 7.15 | 7.16 | 7.18 | 7.17 | 7.16 | |
| PART.1 | (µg/m³) | 4.55 | 4.38 | 4.61 | 4.47 | 4.55 | 4.65 | 5.03 | 4.82 | 4.55 | 4.81 | 4.72 | 6 24 |
| N02.1 | (PPM) | 0.015 | 0.016 | 0.014 | 0.014 | 0.014 | 0.013 | 0.015 | 0.013 | 0.027 | 0.013 | 0.015 | |
| CO.1 | (PPM) | 4.18 | 4.24 | 4.15 | 4.20 | 4.17 | 4.14 | 4.04 | 4.06 | 4.50 | 4.10 | 4.11 | ,0,0 |
| 000 000 | (µg/m³) | 387 | 393 | 384 | 524 | 386 | 384 | 375 | 396 | 388 | 379 | 379 | 250 |
| 000 000 | (ug/m²) | 125 | 125 | 124 | 125 | 125 | 125 | 126 | 124 | 126 | 125 | 124 | |
| V0C7 | (µg/m³) | 879 | 397 | 388 | 393 | 330 | 388 | 379 | 388 | 392 | 383 | 383 | 250 |
| 000 V | (µg/m²) | 384 | 391 | 382 | 386 | 384 | 380 | 368 | 372 | 416 | 375 | 377 | 030 |
| VOC5 | (hg/m³) | 374 | 380 | 371 | 376 | 373 | 405 | 358 | 362 | 396 | 425 | 366 | 240 |
| VOC4 | (hg/m³) | 380 | 386 | 377 | 382 | 379 | 426 | 364 | 368 | 405 | 370 | 372 | 2110 |
| VOC3 | (µg/m³) | 386 | 393 | 384 | 389 | 386 | 383 | 375 | 368 | 388 | 379 | 379 | 107 |
| V0C2 | (µg/m³) | 29482 | 29983 | 29446 | 29938 | 29667 | 29545 | 28088 | 28835 | 30058 | 29031 | 28852 | 23111 |
| 100A | (µg/m³) | 290 | 566 | 286 | 290 | 288 | 305 | 340 | 280 | 306 | 300 | 284 | 2770 |
| | | 3A2 | 3A3 | 3R2 | 3R3 | BR4 | J.R | ENT | TVF | KFA | .R | MBA | 007 |

| | VOCI | VOC2 | VOC3 | V0C4 | VOCS | VOC6 | VOC7 | VOC8 | VOC9 | CO.1 | N02.1 | PART.1 |
|------|---------|---------|---------|---------|---------|---------|---------|---------|---------|-------|-------|---------|
| | (µg/m³) | (µg/m³) | (hg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| 3.72 | 294 | ž | 478 | 483 | 458 | 495 | 1448 | 126 | 490 | 5.63 | 0.053 | 5.15 |
| BA3 | 308 | Ϋ́ | 491 | 496 | 470 | 208 | 208 | 126 | 503 | 5.78 | 0.056 | 4.92 |
| 3R2 | 162 | ž | 469 | 475 | 449 | 487 | 486 | 125 | 481 | 5.56 | 0.050 | 5.13 |
| 3R3 | 295 | ž | 477 | 483 | 457 | 495 | 464 | 126 | 936 | 5.59 | 0.051 | 2.09 |
| 3R4 | 292 | ž | 473 | 478 | 453 | 490 | 489 | 125 | 484 | 5.53 | 0.050 | 5.25 |
| JR. | 319 | ٧ | 473 | 949 | 265 | 485 | 490 | 126 | 484 | 5.53 | 0.047 | 5.04 |
| INI | 374 | ¥ | 485 | 466 | 4 | 478 | 498 | 125 | 493 | 5.47 | 0.050 | 5.35 |
| ١٧٢ | 283 | ž | 534 | 457 | 433 | 469 | 533 | 125 | 531 | 5.35 | 0.046 | 5.47 |
| ΈĀ | 318 | ź | 478 | 552 | 225 | 286 | 464 | 127 | 489 | 6.57 | 0.091 | 5.07 |
| æ, | 328 | Ϋ́ | 473 | 467 | 645 | 480 | 489 | 126 | 483 | 5.49 | 0.046 | 5.13 |
| MBA | 288 | ž | 466 | 471 | 446 | 482 | 481 | 125 | 417 | 5.51 | 0.052 | 5.39 |
| MBR | 267 | ź | 999 | 423 | 400 | 434 | 432 | 123 | 427 | 5.03 | 0.041 | 86.5 |

| _ | | BA2 | BA3 | 500 |
|---|-------|------|------|-------|
| | (PPM) | 5.11 | 5.37 | 7 0 7 |
| | | | | |
| | | | | |

| CO.1 (PPM) | 5.11 | 5.37 | 4.84 | 4.91 | 4.85 | 4.55 | 4.80 | 4.53 | 8.39 | 4.51 | 5.02 |
|---------------|------|------|------|------|------|------|------|------|------|------|------|
| | BA2 | BA3 | BR2 | BR3 | BR4 | DR | ENT | HAL | ΚFΛ | LR. | MBA |

| 2 2 2 | Burst - CLO | 00 | Oven |
|-------------|-------------|--------|-------------|
| V0C2 | Floor | N02.1 | Oven |
| VOC3 | Burst - MBR | PART.1 | Oven |
| VOC4 | Burst - DR | CO.2 | Heater |
| VOCS | Burst - LR | N02.2 | Heater |
| 900A | Burst - KFA | PART.2 | Heater |
| V0C7 | Burst - BA2 | CO.3 | Outdoor air |
| VOC8 | Burst - GAR | N02.3 | Outdoor air |
| 2002 | Burst - BR3 | PART.3 | Outdoor air |

| Table 19 | a - S1M2 | MI.C ove | rall 24-hr | avg conc | entration | S | | | | | | | | | | | | |
|-----------|----------|-----------|------------|----------|-----------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|
| | VOCI | VOC2 | VOC3 | VOC4 | VOCS | VOC6 | VOC7 | VOC8 | 40C9 | CO.1 | NO2.1 | PART.1 | CO.2 | NO2.2 | PART.2 | CO.3 | NO2.3 | PART.3 |
| | (µg/m³) | (m/grl) (| ug/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (hg/m³) | (µg/m³) | (hg/m³) | (PPM) | (PPM) | (mg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (mg/m³) |
| 24 hr avg | 248 | 3586 | 115 | 126 | 124 | 128 | 116 | 141 | 121 | 1.86 | 0.018 | 10.67 | 1.76 | 0.019 | 10.92 | 6.73 | 0.114 | 16.48 |

| PART.3 | (mg/m³) | 9.57 | 1.85 | 34.86 | 24.45 | 21.04 | 40.54 | 34.30 | 31.13 | 32.26 | 33.88 | 7.44 | 20.45 |
|------------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| NO2.3 | (PPM) | 0.161 | 0.163 | 0.188 | 0.183 | 0.179 | 0.241 | 0.229 | 0.213 | 0.222 | 0.229 | 0.159 | 0.173 |
| CO.3 | (PPM) | 10.70 | 10.70 | 10.93 | 10.71 | 10.77 | 11.36 | 11,36 | 11.23 | 10.94 | 11.37 | 10.68 | 10.90 |
| PART.2 | (µg/m³) | 12,31 | 12.38 | 12,38 | 12.28 | 12.29 | 12.48 | 12.45 | 12.40 | 12.58 | 12.48 | 12.31 | 12.27 |
| NO2.2 | (PPM) | 0.110 | 0.114 | 0.093 | 0.102 | 0.100 | 0.075 | 0.077 | 0.079 | 0.083 | 0.071 | 0.110 | 0.082 |
| C0.2 | (PPM) | 3.18 | 3.20 | 2.91 | 3.09 | 3.05 | 2.79 | 2.79 | 2.75 | 2.76 | 2.79 | 3.18 | 2.84 |
| PART.1 | (µg/m³) | 10.48 | 10.45 | 11.83 | 11.23 | 11.12 | 12.06 | 11.67 | 11.51 | 11.73 | 11.84 | 10.46 | 11.20 |
| N02.1 | (PPM) | 0.082 | 980.0 | 0.071 | 0.077 | 0.076 | 0.128 | 0.071 | 890.0 | 0.271 | 0.079 | 0.082 | 0.063 |
| CO:1 | (PPM) | 4.46 | 4.52 | 4.12 | 4.35 | 4.33 | 5.31 | 4.00 | 4.04 | 8.91 | 4.18 | 4.46 | 3.98 |
| 000 000 | (mg/m³) | 300 | 308 | 265 | 1593 | 278 | 225 | 241 | 339 | 242 | 218 | 300 | 292 |
| 00C8 | (µg/m³) | 313 | 314 | 276 | 308 | 316 | 326 | 330 | 383 | 620 | 273 | 312 | 316 |
| V0C7 | (mg/m³) | 3491 | 506 | 185 | 240 | 586 | 164 | 167 | 669 | 173 | 162 | 214 | 374 |
| 00C | (µg/m³) | 320 | 330 | 281 | 303 | 301 | 407 | 303 | 285 | 758 | 322 | 320 | 271 |
| VOCS | (µg/m³) | 596 | 304 | 761 | 295 | 307 | 222 | 444 | 404 | 238 | 683 | 596 | 305 |
| V0C4 | (µg/m³) | 308 | 317 | 272 | 298 | 302 | 861 | 401 | 320 | 247 | 484 | 308 | 285 |
| VOC3 | (µg/m³) | 229 | 234 | 506 | 217 | 214 | 180 | 183 | 981 | 161 | 175 | 231 | 742 |
| VOC2 | (µg/m³) | 3319 | 3448 | 2903 | 3285 | 3133 | 2134 | 2188 | 2472 | 2407 | 2171 | 3548 | 2845 |
| VOCI | (µg/m³) | 993 | 1001 | 845 | 943 | 916 | 999 | 710 | 751 | 748 | 649 | 993 | 801 |
| | | BA2 | BA3 | BR2 | BR3 | BR4 | DR | ENT | HAL | KFA | 1.R | MBA | MBR |

| | RT.3 | /m³) | 22 | 1.38 | 11: | 16 | 64 | .55 | .04 | .47 | .83 | 41 | 11 | 8 |
|-----------|--------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | L | _ | | | | | | | | | | | | |
| | NO2. | (PPM | 0.09 | 0.097 | 0.116 | 0.107 | 0.107 | 0.137 | 0.127 | 0.118 | 0.124 | 0.132 | 0.09 | 0.105 |
| | CO3 | (PPM) | 6.75 | 6.75 | 6.75 | 91.9 | 6.75 | 6.73 | 6.71 | 6.72 | 6.74 | 6.72 | 6.75 | 6.73 |
| | PART.2 | (µg/m³) | 10.47 | 10.38 | 10.98 | 10.77 | 10.77 | 11.52 | 11.33 | 11.18 | 11.30 | 11.44 | 10.44 | 10.90 |
| | NO2.2 | (PPM) | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.021 | 0.021 | 0.020 | 0.022 | 0.019 | 0.020 | 0.018 |
| | CO.2 | (PPM) | 1.81 | 1.83 | 1.78 | 1.80 | 1.79 | 1.73 | 1.74 | 1.75 | 1.77 | 1.72 | 1.82 | 1.77 |
| | PART.1 | (µg/m³) | 10.14 | 10.03 | 10.70 | 10.46 | 10.47 | 11.31 | 11.08 | 10.92 | 11.05 | 11.24 | 10.10 | 10.62 |
| | NO2.1 | (PPM) | 0.015 | 0.016 | 0.016 | 0.016 | 0.016 | 0.021 | 0.017 | 0.016 | 0.029 | 0.019 | 0.015 | 0.015 |
| | CO.1 | (PPM) | 1.85 | 98.1 | 18.1 | 1.84 | 1.83 | 1.85 | 1.78 | 1.79 | 2.05 | 1.80 | 1.86 | 1.81 |
| | VOC9 | (µg/m³) | 123 | 124 | 118 | 194 | 120 | 113 | 114 | 119 | 115 | 113 | 123 | 120 |
| | VOC8 | (µg/m³) | 142 | 142 | 133 | 139 | 140 | 135 | 145 | 144 | 9 | 129 | 141 | 140 |
| | VOC7 | (mg/m³) | 588 | 112 | 9 | 112 | 114 | 106 | 107 | 132 | 107 | 106 | 113 | 121 |
| | VOC6 | (µg/m³) | 128 | 129 | 121 | 125 | 125 | 126 | 121 | 122 | 148 | 122 | 129 | 123 |
| ntralions | VOCS | (µg/m³) | 125 | 126 | 119 | 122 | 123 | 113 | 130 | 127 | 91 | 138 | 125 | 124 |
| vg conce | VOC4 | (µg/m³) | 127 | 127 | 120 | 123 | 124 | 145 | 126 | 125 | 117 | 131 | 127 | 124 |
| c 24-hr a | VOC3 | (µg/m³) | 13 | 114 | 011 | 112 | 112 | 107 | 108 | 8 | 801 | 107 | 911 | 140 |
| MLC zon | VOC2 | (µg/m³) | 2761 | 2700 | 2306 | 2517 | 2528 | 1787 | 1988 | 2222 | 2018 | 1942 | 2862 | 2624 |
| e - SIM2 | VOCI | (µg/m³) | 303 | 320 | 260 | 285 | 282 | 218 | 233 | 243 | 239 | 219 | 310 | 261 |
| Table 19 | | | BA2 | BA3 | BR2 | BR3 | BR4 | DR | ENT | HAI. | KI:V | 1.1. | MBA | MBR |

| VOCT VOCZ VOCZ <th< th=""><th>Table 1</th><th>7MIS - DK</th><th>MLC ZOI</th><th>ne 4-nr av</th><th>g concent</th><th>trations</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></th<> | Table 1 | 7MIS - DK | MLC ZOI | ne 4-nr av | g concent | trations | | | | | | | | | | |
|---|---------|-----------|---------|------------|-----------|----------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|
| (lig/m ¹) (lig/m ² | | VOC1 | VOC2 | VOC3 | VOC4 | VOCS | VOC6 | VOC7 | VOC8 | VOC9 | C0.1 | NO2.1 | PART.1 | CO.2 | NO2.2 | PART.2 |
| 644 NA 142 176 172 181 531 251 165 305 0.033 675 NA 143 178 174 184 139 250 168 3.09 0.034 554 NA 135 178 174 184 139 250 168 3.09 0.034 619 NA 138 174 172 179 145 249 340 3.02 0.032 426 NA 138 174 172 179 145 249 340 3.02 0.032 426 NA 125 216 142 178 152 242 139 2.99 0.034 434 NA 125 170 175 152 282 140 2.71 0.032 440 NA 129 170 175 162 200 274 144 2.71 0.031 482 NA 124 186 198 163 121 211 138 2.76 0.034 618 NA 124 186 198 163 121 211 138 2.76 0.034 618 NA 124 186 198 163 121 211 138 2.76 0.034 618 NA 128 177 173 182 140 249 165 385 0.033 618 NA 128 177 144 2.85 0.033 | | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| 675 NA 143 178 174 184 139 250 168 309 0034 554 NA 143 163 159 167 131 220 155 2.84 0030 596 NA 138 174 175 172 176 151 259 130 0.032 426 NA 128 174 172 176 151 229 130 2.99 0.032 436 NA 125 176 172 172 242 139 2.99 0.032 460 NA 128 170 176 152 282 140 2.71 0.032 440 NA 129 170 175 162 200 274 144 2.71 0.031 445 NA 129 152 149 123 125 144 2.71 0.031 445 NA 124 186 | BA2 | 644 | ž | 142 | 176 | 172 | 181 | 531 | 251 | 165 | 3.05 | 0.033 | 86.6 | 1.84 | 0.022 | 10.50 |
| 554 NA 135 163 159 167 131 220 155 284 0.000 619 NA 140 175 179 145 249 340 302 0.032 596 NA 138 174 172 179 145 249 140 2.99 0.042 436 NA 125 216 142 178 122 242 139 2.99 0.044 460 NA 128 170 175 162 200 274 144 2.71 0.031 482 NA 128 170 175 162 200 274 144 2.77 0.031 482 NA 128 170 175 162 200 274 144 2.77 0.031 483 NA 128 198 163 153 357 146 3.85 0.074 484 NA 145 | BA3 | 675 | ž | 143 | 178 | 174 | 184 | 139 | 250 | 168 | 3.09 | 0.034 | 9.87 | 1.83 | 0.021 | 10.39 |
| 619 NA 140 175 172 179 145 249 340 3.02 0.032 356 NA 138 174 172 176 151 254 160 2.99 0.032 426 NA 138 174 172 176 151 254 160 2.99 0.032 434 NA 125 170 175 152 282 140 2.71 0.032 460 NA 128 170 175 162 200 274 144 2.77 0.031 482 NA 129 132 149 232 125 357 146 3.85 0.077 415 NA 124 186 198 163 121 211 138 2.76 0.034 164 NA 124 186 198 163 124 211 138 2.76 0.034 175 185 180 180 180 180 180 180 180 180 180 180 | BR2 | 554 | ž | 135 | 163 | 159 | 167 | 131 | 220 | 155 | 2.84 | 0.030 | 10.45 | 1.79 | 0.021 | 10.11 |
| 596 NA 138 174 172 176 151 254 160 2.99 0.032 426 NA 125 216 142 178 122 242 139 2.99 0.034 434 NA 125 170 176 159 122 140 2.71 0.032 480 NA 128 170 175 162 200 274 144 2.77 0.031 415 NA 129 152 149 232 125 357 146 3.85 0.071 415 NA 124 186 198 163 121 211 138 2.76 0.034 516 NA 208 169 167 164 248 151 285 0.009 | BR3 | 619 | ž | 140 | 175 | 172 | 179 | 145 | 249 | 340 | 3.02 | 0.032 | 10.06 | 1.80 | 0.021 | 10.89 |
| 426 NA 125 216 142 178 122 242 139 2.99 0.044 434 NA 125 170 175 152 282 140 2.71 0.032 446 NA 128 170 175 162 200 274 144 2.77 0.031 482 NA 129 152 149 2.32 125 357 146 3.85 0.077 415 NA 124 186 198 163 121 211 138 2.76 0.034 648 NA 144 177 173 182 140 249 166 3.06 0.033 156 NA 208 169 167 164 248 151 2.85 0.029 | BR4 | 296 | ž | 138 | 174 | 172 | 176 | 151 | 254 | 991 | 2.99 | 0.032 | 10.17 | 1.81 | 0.022 | 10.86 |
| 434 NA 125 170 176 159 122 282 140 2.71 0.002 460 NA 128 170 175 162 200 274 144 2.77 0.031 482 NA 129 122 149 232 125 357 146 3.85 0.077 415 NA 124 186 198 163 121 211 138 2.76 0.034 648 NA 145 177 173 182 140 249 165 306 0.033 516 NA 208 169 167 164 248 151 2.85 0.029 | DR | 426 | ž | 125 | 216 | 142 | 178 | 122 | 242 | 139 | 2.99 | 0.044 | 11.15 | 1.85 | 0.027 | 11.68 |
| 460 NA 128 170 175 162 200 274 144 2.77 0.031 482 NA 129 152 149 232 125 357 146 3.85 0.077 415 NA 124 186 198 163 121 211 138 2.76 0.034 648 NA 145 177 173 182 140 249 166 3.06 0.033 516 NA 208 168 169 167 164 248 151 2.85 0.029 | ENT | 434 | × | 125 | 170 | 176 | 129 | 122 | 282 | 140 | 2.71 | 0.032 | 11.05 | 1.92 | 0.032 | 11.51 |
| 482 NA 129 152 149 232 125 357 146 3.85 0.077 415 NA 124 186 198 163 121 211 138 2.76 0.034 648 NA 145 177 173 182 140 249 166 3.06 0.033 516 NA 208 169 167 164 248 151 2.85 0.029 | HAL | 460 | ٧ | 128 | 170 | 175 | 162 | 200 | 274 | 144 | 2.77 | 0.031 | 10.85 | 1.90 | 0.029 | 11.31 |
| 415 NA 124 186 198 163 121 211 138 2.76 0.034 (648 NA 145 177 113 182 140 249 165 306 0.033 151 NA 208 169 167 164 248 151 2.85 0.029 | ΚFΛ | 482 | × | 129 | 152 | 149 | 232 | 125 | 357 | 146 | 3.85 | 0.077 | 10.86 | 1.95 | 0.035 | 11.67 |
| 648 NA 145 177 173 182 140 249 166 3.06 0.033 151 816 NA 208 168 169 167 164 248 151 2.85 0.029 | × | 415 | ٧ | 124 | 186 | 861 | 163 | 121 | 211 | 138 | 2.76 | 0.034 | 11.16 | 1.83 | 0.024 | 11.50 |
| NA 208 168 169 167 164 248 151 2.85 0.029 | MBA | 648 | × | 145 | 111 | 173 | 182 | 140 | 249 | 991 | 3.06 | 0.033 | 9.94 | 1.83 | 0.021 | 10.46 |
| | MBR | 516 | ٧X | 208 | 168 | 691 | 167 | 164 | 248 | 151 | 2.85 | 0.029 | 10.50 | 1.86 | 0.024 | 10.97 |

| | CO.1 | CO.2 | |
|-----|-------|-------|--|
| | (PPM) | (PPM) | |
| BA2 | 4.00 | 1.89 | |
| BA3 | 4.12 | 1.88 | |
| BR2 | 3.70 | 1.80 | |
| BR3 | 3.92 | 1.81 | |
| BR4 | 3.90 | 1.83 | |
| DR | 4.71 | 1.78 | |
| ENT | 3.69 | 1.89 | |
| HAL | 3.67 | 1.88 | |
| ΚFΛ | 7.57 | 1.87 | |
| LR | 3.91 | 1.79 | |
| MBA | 3.99 | 1.89 | |
| MBR | 3.60 | 1.90 | |

| 100A | Burst - BMT | CO.1 | Oven |
|-------|-------------|--------|-------------|
| VOC2 | Floor | N02.1 | Oven |
| VOC3 | Burst - MBR | PART.1 | Oven |
| VOC4 | Burst - DR | | Heater |
| VOCS | Burst - LR | | Heater |
| 000 V | Burst - KFA | | Heater |
| VOC7 | Burst - BA2 | | Outdoor air |
| VOC8 | Burst - GAR | | Outdoor air |
| VOC9 | Burst - BR3 | | Outdoor als |

| Table 20a | - SIM2 | MLM ove | erall 24-h | r avg con | centration | JS | | | | | | | | | | | | |
|-----------|---------|---------|------------|-----------|------------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|
| | VOCI | VOC2 | VOC3 | VOC4 | VOCS | 900x | V0C7 | 80C8 | VOC9 | CO.1 | NO2.1 | PART.1 | CO.2 | NO2.2 | PART.2 | CO.3 | N02.3 | PART.3 |
| | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (μg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| 24 hr avg | 269 | 6490 | 129 | 125 | 911 | 136 | 127 | 159 | 126 | 1.88 | 0.017 | 10.76 | 1.82 | 0.017 | 11.12 | 9.90 | 0.095 | 19.19 |

| | VOCI | VOC2 | VOC3 | VOC4 | VOC5 | 900x | V0C7 | 800x | VOC9 | CO.1 | N02.1 | PART.1 | CO.2 | N02.2 | PART.2 | CO.3 | N02.3 | PART.3 |
|-----|---------|---------|---------|---------|---------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|
| | (µg/m³) | (μg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| BA2 | 1046 | 4254 | 246 | 247 | 793 | 280 | 3371 | 334 | 277 | 3.13 | 0.037 | 11.51 | 3.03 | 0.098 | 13.39 | 9.84 | 0.122 | 20.92 |
| BA3 | 1093 | 7502 | 251 | 260 | 267 | 396 | 251 | 308 | 293 | 3.21 | 0.039 | 10.68 | 3.10 | 0.101 | 13.20 | 68.6 | 0.130 | 3.28 |
| BR2 | 852 | 5415 | 257 | 218 | 253 | 246 | 199 | 271 | 242 | 2.87 | 0.034 | 12.27 | 2.85 | 0.087 | 13.46 | 10.93 | 0.191 | 37.26 |
| BR3 | 905 | 5851 | 244 | 225 | 251 | 257 | 543 | 282 | 4128 | 2.96 | 0.035 | 11.94 | 2.87 | 0.088 | 13.42 | 10.67 | 0.156 | 27.11 |
| BR4 | 820 | 3792 | 215 | 222 | 228 | 250 | 233 | 245 | 248 | 2.90 | 0.037 | 12.56 | 2.86 | 0.086 | 13.40 | 11.59 | 0.243 | 46.16 |
| DR | 823 | 5659 | 504 | 2591 | 344 | 633 | 506 | 320 | 229 | 3.60 | 0.056 | 12.45 | 2.68 | 0.068 | 12.97 | 10.91 | 0.171 | 40.51 |
| ENT | 1005 | 3797 | 252 | 178 | 241 | 216 | 804 | 515 | 195 | 2.73 | 0.035 | 12.61 | 2.72 | 0.088 | 14.33 | 11.08 | 0.241 | 50.78 |
| HAL | 630 | 3798 | 410 | 176 | 416 | 681 | 1610 | 287 | 189 | 2.87 | 0.030 | 12.46 | 2.87 | 0.083 | 14.22 | 11.61 | 0.266 | 45.96 |
| KFA | 802 | 4961 | 504 | 213 | 215 | 1731 | 203 | 1337 | 235 | 15.68 | 0.501 | 12.54 | 4.01 | 0.131 | 14.54 | 10.54 | 0.128 | 19.57 |
| LR | 735 | 3666 | 213 | 238 | 876 | 203 | 916 | 353 | 187 | 2.79 | 0.034 | 12.62 | 2.77 | 0.050 | 13.03 | 11.25 | 0.226 | 46.09 |
| MBA | 1010 | 6354 | 362 | 247 | 254 | 281 | 238 | 292 | 278 | 3.14 | 0.037 | 11.68 | 2.94 | 0.093 | 13.27 | 9.92 | 0.122 | 24.00 |
| MBR | 641 | 5708 | 1704 | 178 | 188 | 208 | 248 | 223 | 195 | 2.64 | 0.029 | 12.42 | 2.60 | 0.059 | 13.14 | 10.67 | 0.172 | 30 04 |

| | I DOW | 2007 | 2023 | NOON | NOCE | NOOR | 1007 | 0007 | 0007 | 5 | - COIN | DADT | 000 | NO33 | DADE |
|----------|---------|---------|---------|---------|---------|---------|---------|---------|---------|-------|--------|---------|-------|-------|---------|
| | 3 | 725 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 1.70 | L. LYW. | 7.00 | NO2.2 | FAK1.2 |
| | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| BA2 | 430 | V | 117 | 119 | 175 | 124 | 487 | 183 | 122 | 2.27 | 0.014 | 10.82 | 1.96 | 0.022 | 10.20 |
| BA3 | 999 | Ν | 165 | 170 | 169 | 061 | 991 | 501 | 182 | 2.59 | 0.014 | 10.06 | 1.92 | 0.019 | 9.82 |
| BR2 | 432 | ΥN | 133 | 131 | 152 | 140 | 275 | 180 | 136 | 2.15 | 0.015 | 11.58 | 2.01 | 0.028 | === |
| BR3 | 458 | Ν | 136 | 134 | 152 | 44 | 249 | 179 | 547 | 2.21 | 0.015 | 11.44 | 1.98 | 0.025 | 10.75 |
| BR4 | 394 | Ϋ́ | 128 | 130 | 134 | 138 | 147 | 155 | 135 | 2.20 | 0.017 | 11.75 | 1.84 | 0.020 | 11.14 |
| DK DK | 412 | ž | 126 | 475 | 178 | 139 | 130 | 178 | 134 | 2.18 | 0.015 | 11.67 | 1.96 | 0.024 | 10.60 |
| ENT | 536 | Ν | 100 | 601 | 011 | 112 | 119 | 225 | Ξ | 1.92 | 0.017 | 12.22 | 2.31 | 0.062 | 12.60 |
| HAL | 390 | ΥN | 122 | 115 | 148 | 611 | 335 | 176 | 118 | 1.95 | 0.017 | 12.17 | 2.12 | 0.044 | 12.26 |
| KFA | 384 | Ϋ́ | 131 | 142 | 135 | 395 | 132 | 909 | 141 | 6.32 | 0.146 | 11.55 | 2.83 | 0.078 | 12.38 |
| ۳ | 374 | N | 8 | 60 | 193 | 112 | 115 | 176 | Ξ | 1.97 | 0.017 | 12.25 | 1.88 | 0.022 | 11.37 |
| MBA | 443 | ¥ | 207 | 145 | 145 | 157 | 148 | 162 | 152 | 2.25 | 0.014 | 10.91 | 16.1 | 0.019 | 10.04 |
| MBR | 220 | ٧X | 111 | 911 | 117 | 120 | 128 | 124 | 0 | 200 | 9100 | 11 96 | 1 03 | 0.03 | 11 12 |

| | CO.1 | CO.2 | CO.1 CO.2 |
|-----|-------|-------|-----------|
| | (PPM) | (PPM) | |
| BA2 | 2.44 | 2.17 | |
| BA3 | 2.50 | 2.15 | |
| BR2 | 2.59 | 2.23 | |
| BR3 | 5.60 | 2.21 | |
| BR4 | 2.66 | 1,92 | |
| DR | 5.64 | 2.20 | |
| ENT | 2.40 | 2.57 | |
| HAL | 2.47 | 2.27 | |
| ΚFΛ | 13.01 | 3.52 | |
| LR | 2.55 | 1.95 | |
| MBA | 2.45 | 2.12 | |
| MBR | 2 52 | 200 | |

| | | | | _ | | | air | air | -i- |
|------|-------------|-------|-------------|------------|-------------|-------------|-------------|-------------|-------------|
| | | | | | | | Outdoor air | _ | _ |
| | CO.1 | N02.1 | PART.1 | CO.2 | N02.2 | PART.2 | CO.3 | N02.3 | PART.3 |
| _ | Burst - BMT | Floor | Burst - MBR | Burst - DR | Burst - L.R | Burst - KFA | Burst - BA2 | Burst - GAR | Burst - BR3 |
| EGEN | V0C1 | V0C2 | VOC3 | VOC4 | VOCS | 00C6 | V0C7 | VOC8 | 800A |
| _ | | | | | | | | | |

| | VOCI | VOC2 | VOC3 | VOC4 | VOCS | VOC6 | VOC7 | 800x | 0000 | CO.1 | N02.1 | PART.1 | CO.3 | N02.3 | PART.3 |
|----------|---------|---------|---------|---------|---------|----------------------|---------|---------|---------|-------|-------|---------|-------|-------|---------|
| | (ug/m³) | (ug/m³) | (mg/m³) | (µg/m³) | (µg/m³) | (µg/n ²) | (µg/m²) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (mg/m³) | (PPM) | (PPM) | (µg/m³) |
| 4 hr ave | 284 | 7364 | 123 | 125 | 134 | 127 | 128 | 132 | 123 | 1.87 | 0.017 | 10.73 | 6.71 | 0.00 | 17.87 |

| | VOCI | V0C2 | VOC3 | VOC4 | VOCS | VOC6 | V0C7 | VOC8 | 6200 | CO.1 | NO2.1 | PART.1 | CO.3 | NO2.3 | PART.3 |
|------|---------|---------|---------|---------|---------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|
| | (µg/m³) | (hg/m²) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| BA2 | 1022 | 9242 | 253 | 268 | 323 | 282 | 10646 | 272 | 289 | 4.19 | 690.0 | 10.58 | 10.45 | 0.134 | 16.10 |
| BA3 | 9901 | 17117 | 197 | 576 | 334 | 167 | 234 | 500 | 297 | 4.33 | 0.074 | 10.44 | 10.44 | 0.138 | 2.13 |
| BR2 | 976 | 6416 | 233 | 242 | 288 | 253 | 373 | 280 | 260 | 3.86 | 0.058 | 11.50 | 10.55 | 0.148 | 23.34 |
| DR3 | 943 | 7141 | 238 | 244 | 262 | 257 | 366 | 276 | 3512 | 3.94 | 0.061 | 11.34 | 10.53 | 0.138 | 22.21 |
| DR4 | 924 | 6545 | 236 | 239 | 285 | 251 | 413 | 276 | 257 | 3.89 | 090.0 | 11.59 | 10.58 | 0.146 | 25.75 |
| DR | 308 | 1816 | 500 | 9061 | 879 | 231 | 194 | 516 | 237 | 3.69 | 0.052 | 11.86 | 10.77 | 0.157 | 30.02 |
| ENT | 787 | 3931 | 171 | 184 | 212 | 161 | 164 | 474 | 194 | 3.14 | 0.048 | 12.34 | 11.57 | 0.268 | 49.47 |
| HAL | 799 | 4200 | 251 | 500 | 231 | 506 | 1479 | 418 | 211 | 3,31 | 0.044 | 12.06 | 11.13 | 0.229 | 43.53 |
| KI:V | 885 | 9414 | 221 | 451 | 295 | 1576 | 210 | 908 | 252 | 14.55 | 0.481 | 1.64 | 10.56 | 0.130 | 12.44 |
| LR | 268 | 5276 | 172 | 179 | 1503 | 981 | 163 | 504 | 061 | 3.12 | 0.043 | 12.38 | 11.28 | 0.223 | 45.09 |
| MBA | 166 | 10210 | 899 | 268 | 323 | 282 | 227 | 253 | 289 | 4.19 | 0.069 | 10.93 | 10.48 | 0.134 | 16.37 |
| MBR | 819 | 5028 | 1430 | 161 | 222 | 8 | 176 | 961 | 204 | 3.27 | 0.044 | 12.08 | 10.88 | 0.192 | 36.85 |

| | NO2.1 PART.1 CO.3 NO2.3 | (PPM) (µg/m²) (PPM) (PPM) | 0.011 10.17 6.81 0.072 | 0.010 9.06 7.27 0.057 1.22 | 0.012 10.76 6.78 0.089 | 0.011 10.55 6.77 0.081 | 0.012 10.78 6.73 0.090 | 0.012 10.91 6.80 0.091 | 0.016 11.72 6.73 0.143 | 0.014 11.43 6.68 0.122 | 0.039 10.34 6.85 0.067 | 0.014 11.71 6.65 0.128 | 0.011 10.27 6.75 0.072 | 0.013 11.39 6.67 0.113 |
|--------------|-------------------------|---------------------------|------------------------|----------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|
| | | | | 2.08 0.010 | | | | | | | | | | |
| | | _ | | 133 | | | | | | | | | | |
| | | _ | | 128 148 | | | | | | | | | | |
| SL | | _ | | 136 | | | | | | | | | | |
| ncentration | | _ | | 145 | | | | | | | | | | |
| 24-hr avg co | | _ | | 127 131 | | | | | | | | | | |
| ALH zone 2- | | _ | | 7162 12 | | | | | | | | | | ı |
| IC - SIMZN | | _ | | 517 | | | | | | | | | | |
| Table 2 | | | DA2 | DA3 | BR2 | BR3 | BR4 | DR | ENT | HVL | ΚFΛ | I.R | MBA | MBR |

| | VOCI | VOC2 | VOC3 | VOC4 | VOCS | NOC6 | VOC7 | VOC8 | 0000 | CO. | NO2.1 | PART. |
|----------|---------|---------|---------|---------|----------------------|---------|---------|---------|---------|-------|-------|--------|
| | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (mg/m ₂) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m²) | (PPM) | (PPM) | (µg/m² |
| 3.42 | 169 | ž | 4 | 149 | 173 | 129 | 1783 | 202 | 154 | 2.89 | 0.025 | 10.20 |
| 143 | 808 | ž | 152 | 162 | 192 | 174 | 155 | 500 | 168 | 3.06 | 0.027 | 68.6 |
| IR2 | 609 | ž | 132 | 140 | 158 | 146 | 189 | 506 | 142 | 5.69 | 0.022 | 10.58 |
| BR3 | 624 | ž | 134 | 141 | 191 | 149 | 181 | 506 | 703 | 2.74 | 0.023 | 10.52 |
| IR4 | 289 | ž | 132 | 138 | 156 | 146 | 182 | 202 | 141 | 2.67 | 0.023 | 10.68 |
| 8 | 448 | ž | 127 | 446 | 306 | 139 | 128 | 158 | 136 | 2.58 | 0.021 | 10.89 |
| L. | 528 | ź | Ξ | 114 | 122 | 117 | 112 | 239 | 115 | 2.14 | 0.020 | 11.90 |
| M | 529 | ž | 911 | 118 | 127 | 121 | 246 | 525 | 120 | 2.26 | 0.020 | 11.58 |
| ΈĀ | 549 | ź | 136 | 220 | 961 | 459 | 137 | 427 | 147 | 5.51 | 0.117 | 10.65 |
| Z, | 304 | ž | 115 | 118 | 360 | 121 | 115 | 140 | 119 | 2.24 | 0.020 | 11.73 |
| ΨPV | 620 | ź | 526 | 148 | 172 | 157 | 145 | 181 | 153 | 2.87 | 0.024 | 10.23 |
| ABR | 363 | × | 366 | 123 | 135 | 127 | 127 | 146 | 125 | 233 | 0.00 | 11 36 |

| ZMLH zone 1-hr avg c | Able 21e - SinzamLH zone 1-nr avg concentrations |
|----------------------|--|
| SI ~ | 116 - 510 COO.1 CPPM 3.37 3.23 3.21 3.21 3.21 2.82 2.82 2.82 2.83 2.83 2.84 2.84 |

| VOCI | Burst - BMT | CO.1 | Oven |
|------------|-------------|--------|-------------|
| V0C2 | | N02.1 | Oven |
| VOC3 | | PART,1 | Oven |
| VOC4 | | CO.2 | Heater |
| VOCS | | N02.2 | Heater |
| 000 000 | | PART.2 | Heater |
| V0C7 | | CO.3 | Outdoor air |
| VOC8 | | NO2.3 | Outdoor a |
| 000 | Burst - BR3 | PART.3 | Outdoor a |

| VOCI | V0C2 | VOC3 | V0C4 | VOCS | 900A | V0C7 | VOC8 | V0C9 | CO.1 | N02.1 | PART.1 | CO.2 | NO2.2 | PART.2 | CO.3 | N02.3 | PART.3 |
|--------|---------|---------|---------|---------|---------|---------|---------|----------------------|-------|-------|---------|-------|-------|---------|-------|-------|---------|
| (g/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (mg/m³) | (mg/m³) | (µg/m³) | (µg/m³) | (mg/m ₃) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| 640 | 11745 | 160 | 183 | 182 | 183 | 166 | 302 | 175 | 2.29 | 0.015 | 7.60 | 2.15 | 0.017 | 8.22 | 6.72 | 0.053 | 5.62 |

| 7-077 | | | | | | | | | | | | | | | | | |
|-------|-----------|---------|---------|---------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|
| × | 70C1 VOC2 | 32 VOC3 | VOC4 | VOC5 | VOC6 | V0C7 | 800x | 6000 | CO.1 | N02.1 | PART.1 | CO.2 | NO2.2 | PART.2 | CO.3 | N02.3 | PART.3 |
| gn) | _ | _ | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (μg/m³) | (PPM) | (PPM) | (μg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| 15 | | | 372 | 384 | 373 | 3583 | 520 | 376 | 4.76 | 0.083 | 7.59 | 4.00 | 0.129 | 10.42 | 8.93 | 0.073 | 1.49 |
| 15 | | | 384 | 395 | 385 | 308 | 521 | 387 | 4.81 | 0.087 | 7.62 | 4.01 | 0.134 | 10.48 | 8.93 | 0.075 | 0.56 |
| 14 | | | 353 | 354 | 352 | 287 | 503 | 346 | 4.51 | 0.074 | 8.83 | 3.84 | 0.116 | 10.51 | 00.6 | 0.083 | 13.96 |
| 15 | | | 365 | 367 | 365 | 300 | 517 | 1779 | 4.67 | 0.078 | 8.23 | 3.97 | 0.122 | 10.35 | 8.92 | 0.085 | 9.17 |
| 15 | 1510 8599 | 3 292 | 365 | 367 | 365 | 309 | 517 | 360 | 4.67 | 0.078 | 8.01 | 3.97 | 0.122 | 10.36 | 8.92 | 0.083 | 7.72 |
| 13 | | | 1197 | 327 | 459 | 790 | 206 | 316 | 5.63 | 0.121 | 9.30 | 3.64 | 0.104 | 10.68 | 9.35 | 0.118 | 18.43 |
| 13 | | | 369 | 392 | 334 | 270 | 648 | 325 | 4.26 | 0.070 | 8.96 | 3.63 | 0.108 | 10.75 | 9.36 | 0.115 | 17.47 |
| 14 | | | 352 | 358 | 346 | 1670 | 592 | 475 | 4.48 | 0.063 | 8.51 | 3.85 | 0.105 | 10.49 | 8.99 | 0.097 | 12.73 |
| 13 | | | 337 | 338 | 875 | 275 | 753 | 327 | 11.22 | 0.347 | 8.70 | 3.74 | 0.108 | 10.47 | 00.6 | 0.098 | 11.02 |
| 12 | | | 287 | 984 | 355 | 256 | 469 | 309 | 4.60 | 0.073 | 8.76 | 3.60 | 960.0 | 10.62 | 9.27 | 0.104 | 12.62 |
| 15 | | | 372 | 384 | 373 | 336 | 270 | 376 | 4.74 | 0.083 | 7.60 | 4.00 | 0.129 | 10.40 | 8.93 | 0.073 | 1.28 |
| 14 | | | 338 | 343 | 117 | 483 | 211 | 346 | 4 42 | 0.061 | 7 05 | 3.85 | 0 100 | 10 27 | 8 02 | 0 0 0 | 5 78 |

| Table 2 | 2c - SIM2 | MTC zor | ITC zone 24-hr av | vg conce. | ntrations | | | | | | | | | | | | | |
|---------|-----------|---------|-------------------|-----------|-----------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|
| | VOC1 | V0C2 | VOC3 | 4 | VOCS | 900A | V0C7 | 800A | VOC9 | CO.1 | N02.1 | PART.1 | CO.2 | N02.2 | PART.2 | CO.3 | N02.3 | PART.3 |
| | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (μg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (mg/m³) |
| BA2 | 715 | 2609 | 158 | 185 | 184 | 185 | 349 | 303 | 178 | 2.31 | 0.012 | 7.24 | 2.24 | 0.019 | 7.95 | 6.81 | 0.045 | 0.60 |
| BA3 | 719 | 7505 | 158 | 185 | 184 | 185 | 162 | 303 | 179 | 2.31 | 0.013 | 7.23 | 2.24 | 0.019 | 7.94 | 6.81 | 0.045 | 0.42 |
| BR2 | 654 | 7085 | 152 | 176 | 175 | 176 | 155 | 285 | 171 | 2.26 | 0.013 | 7.74 | 2.19 | 0.018 | 8.39 | 6.82 | 0.056 | 5.57 |
| BR3 | 685 | 7352 | 155 | 180 | 180 | 181 | 129 | 293 | 261 | 2.28 | 0.013 | 7.52 | 2.21 | 0.018 | 8.20 | 6.81 | 0.051 | 3.50 |
| BR4 | 069 | 7422 | 156 | 181 | 181 | 181 | 160 | 295 | 175 | 2.29 | 0.012 | 7.47 | 2.21 | 0.018 | 8,15 | 6.81 | 0.049 | 2.98 |
| DR | 290 | 6411 | 146 | 219 | 191 | 179 | 149 | 283 | 162 | 2.28 | 0.017 | 8.31 | 2.13 | 0.018 | 8.89 | 6.79 | 0.069 | 10.63 |
| ENT | 609 | 6473 | 148 | 174 | 171 | 171 | 151 | 333 | 165 | 2.18 | 0.013 | 8.12 | 2.15 | 0.020 | 8.78 | 91.9 | 0.063 | 8.39 |
| HAL | 651 | 7260 | 152 | 178 | 179 | 177 | 228 | 312 | 171 | 2.23 | 0.012 | 7.72 | 2.18 | 810'0 | 8.38 | 6.78 | 0.051 | 4.66 |
| KFA | 626 | 9119 | 120 | 172 | 172 | 212 | 152 | 344 | 167 | 2.57 | 0.028 | 7.98 | 2.18 | 0.020 | 8.63 | 6.79 | 0.057 | 6.41 |
| LR | 299 | 0929 | 147 | 190 | 213 | 174 | 120 | 273 | 164 | 2.22 | 0.014 | 8.18 | 2.12 | 0.017 | 8.75 | 6.79 | 0.063 | 86.8 |
| MBA | 715 | 7680 | 160 | 185 | 184 | 185 | 163 | 302 | 179 | 2.31 | 0.012 | 7.23 | 2,24 | 0.018 | 7.94 | 6.81 | 0.044 | 0.58 |
| au v | (1) | 2222 | 9 | 100 | 100 | 100 | 170 | 000 | 176 | | | 2 40 | 000 | 2100 | 21.0 | 00 / | 2100 | 200 |

| | | | | | | | | 0000 | 00000 | . 00 | | | | | 1 |
|-----|---------|-------------|---------|---------|---------|-------------|---------|---------|-------------|-------|-------|---------|-------|-------|---------|
| | 200 | 7 0 0 | VOC3 | ۲ د | VOC5 | 2 C C | | Š | ري د د د | | NO2.1 | PART. | C0.7 | NO2.2 | PARI |
| | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/ш³) | (µg/m³) | (μg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| BA2 | 1211 | ž | 220 | 270 | 270 | 177 | 632 | 423 | 259 | 3.82 | 0.036 | 7.01 | 16.1 | 0.017 | 7.88 |
| BA3 | 1226 | ¥ | 220 | 271 | 27.1 | 272 | 226 | 422 | 260 | 3.84 | 0.037 | 7.00 | 16.1 | 0.017 | 7.87 |
| BR2 | 1127 | Ϋ́ | 211 | 257 | 257 | 258 | 215 | 392 | 247 | 3.66 | 0.034 | 7.41 | 1.87 | 0.016 | 8.34 |
| BR3 | 1193 | ž | 218 | 267 | 267 | 268 | 224 | 414 | 466 | 3.78 | 0.035 | 7.05 | 1.89 | 0.017 | 8.25 |
| BR4 | 1190 | ž | 218 | 267 | 267 | 268 | 224 | 416 | 256 | 3.78 | 0.035 | 7.06 | 1.89 | 0.017 | 8.16 |
| DR | 666 | Ϋ́ | 197 | 363 | 238 | 270 | 201 | 418 | 229 | 3.87 | 0.046 | 8.04 | 1.92 | 0.021 | 8.97 |
| ENT | 186 | ٧ | 195 | 244 | 249 | 238 | 198 | 576 | 226 | 3.44 | 0.032 | 8.02 | 2.11 | 0.035 | 80.6 |
| HAL | 1061 | V | 504 | 254 | 256 | 251 | 437 | 419 | 251 | 3.59 | 0.031 | 7.49 | 1.98 | 0.023 | 8.44 |
| ΚFΛ | 1052 | ٧ | 203 | 246 | 246 | 344 | 207 | 909 | 237 | 5.03 | 0.093 | 7.78 | 2.09 | 0.033 | 9.01 |
| E E | 983 | V | 961 | 594 | 347 | 250 | 199 | 371 | 228 | 3.59 | 0.035 | 8.01 | 1.89 | 0.017 | 8.70 |
| MBA | 1210 | ٧ | 224 | 270 | 270 | 27.1 | 228 | 418 | 259 | 3.82 | 0.036 | 7.00 | 1.91 | 0.017 | 7.87 |
| MRP | 1105 | Z | 325 | 757 | 258 | 257 | 171 | 412 | 240 | 3 65 | 0.00 | 7 7 | 5 | 6100 | 0 |

| CO.1 CO.2 | | | | | | | | | | | | | |
|-----------|-------|------|------|------|------|------|------|------|------|------|------|------|------|
| C0.2 | (PPM) | 2.08 | 5.08 | 2.01 | 2.03 | 5.04 | 5.04 | 2.23 | 2.11 | 2.23 | 2.02 | 2.08 | 200 |
| CO.1 | (PPM) | 3.81 | 3.92 | 3.61 | 3.70 | 3.70 | 4.59 | 3.48 | 3.38 | 8.42 | 3.65 | 3.79 | 3 35 |
| | | BA2 | BA3 | BR2 | BR3 | BR4 | DR | ENT | HAL | KFA | LR | MBA | MRD |

| これのこれ | | | |
|-------|-------------|--------|-------------|
| VOCI | Burst - BMT | CO.1 | Oven |
| V0C2 | Floor | N02.1 | Oven |
| V0C3 | Burst - MBR | PART.1 | Oven |
| V0C4 | Burst - DR | CO.2 | Heater |
| VOC5 | Burst - LR | N02.2 | Heater |
| 00Ce | Burst - KFA | PART.2 | Heater |
| VOC7 | Burst - BA2 | CO.3 | Outdoor air |
| VOC8 | Burst - GAR | NO2.3 | Outdoor air |
| VOC9 | Burst - DR3 | PART.3 | Outdoor air |

| Table | 23b - SIM2h | ~ | TM zone peak concentrate | oncentral | 0 | | | | | | | | | | | | | |
|-------|-------------|---------|--------------------------|-----------|---------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|
| | VOCI | VOC2 | VOC3 | V0C4 | VOCS | 900x | V0C7 | 800x | V0C9 | CO.1 | N02.1 | PART.1 | CO.2 | N02.2 | PART.2 | CO.3 | N02.3 | PART.3 |
| | (µg/m³) | (mg/m³) | (mg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| BA2 | 1707 | 15689 | 302 | 346 | 397 | 370 | 13124 | 424 | 376 | 4.38 | 0.051 | 8.82 | 3.57 | 0.102 | 11.41 | 8.26 | 0.047 | 7.39 |
| BA3 | 1743 | 16091 | 316 | 364 | 418 | 389 | 302 | 416 | 395 | 4.56 | 0.055 | 8.49 | 3.68 | 0.10 | 11.43 | 8.24 | 0.050 | 0.91 |
| BR2 | 1608 | 14434 | 275 | 314 | 360 | 337 | 201 | 422 | 341 | 4.11 | 0.045 | 88.6 | 3.40 | 0.00 | 11.32 | 8.75 | 0.059 | 14.61 |
| BR3 | 1643 | 14994 | 283 | 323 | 370 | 346 | 419 | 418 | 4196 | 4.18 | 0.047 | 9.20 | 3.44 | 0.093 | 11.29 | 8.52 | 0.050 | 7.38 |
| BR4 | 1512 | 12830 | 276 | 315 | 361 | 337 | 327 | 404 | 343 | 4.14 | 0.047 | 10.21 | 3.41 | 0.092 | 11.45 | 9.13 | 0.107 | 20.59 |
| ř | 1541 | 15668 | 526 | 3476 | 201 | 426 | 273 | 453 | 319 | 5.04 | 0.064 | 10.12 | 3.24 | 0.076 | 11.18 | 8.55 | 0.062 | 15.10 |
| ENT | 1431 | 11637 | 253 | 277 | 322 | 302 | 297 | 7117 | 308 | 3.60 | 0.041 | 11.53 | 3.36 | 0.088 | 13.36 | 10.23 | 0.178 | 34.97 |
| HAL | 1357 | 12353 | 270 | 253 | 290 | 279 | 2848 | 642 | 346 | 3.36 | 0.032 | 11.27 | 3.08 | 0.075 | 13.04 | 10.16 | 0.161 | 28.44 |
| KI:V | 1991 | 15547 | 263 | 318 | 342 | 2074 | 270 | 1392 | 324 | 22.62 | 0.664 | 10.05 | 3.87 | 0.077 | 10.86 | 8.30 | 0.042 | 5.87 |
| ĭ | 1355 | 13042 | 230 | 387 | 2415 | 588 | 281 | 317 | 274 | 3.57 | 0.037 | 10.93 | 2.82 | 0.063 | 11.64 | 9.28 | 0.104 | 22.24 |
| MBA | 1702 | 16257 | 489 | 345 | 396 | 369 | 340 | 408 | 376 | 4.38 | 0.051 | 9.21 | 3.53 | 0.101 | 11.41 | 8.27 | 0.050 | 10.49 |
| MARD | 1300 | 14206 | 2003 | 386 | 200 | 202 | 466 | 370 | 276 | 3 48 | 0.034 | 10 69 | 2 05 | 0.068 | 11.85 | 8 75 | 0.076 | 18 07 |

| Table | 3c - SIM2 | MIM zor | nc 24-hr | avg concc | niralions | | | | | | | | | | | | | |
|-------|-----------|---------|----------|-----------|-----------|---------|----------|---------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|
| | VOCI | VOC2 | VOC3 | VOC4 | VOCS | VOC6 | VOC7 | VOC8 | 6200 | CO.1 | NO2.1 | PART.1 | CO.2 | NO2.2 | PART.2 | CO.3 | NO2.3 | PART.3 |
| | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (mg/m³) |
| BA2 | 1058 | 12987 | 173 | 961 | 214 | 500 | 1060 | 256 | 195 | 2.44 | 0.00 | 7.32 | 2.63 | 0.011 | 8.41 | 6.70 | 0.025 | 1.68 |
| BA3 | 1116 | 13257 | 179 | 204 | 222 | 218 | 194 | 258 | 203 | 2.52 | 0.00 | 7.07 | 5.69 | 0.012 | 8.21 | 6.72 | 0.021 | 0.34 |
| BR2 | 952 | 12009 | <u>3</u> | 184 | 701 | 195 | 211 | 247 | 184 | 2.35 | 0.007 | 7.82 | 2.54 | 0.011 | 8.81 | 6.75 | 0.033 | 4.21 |
| BR3 | 1001 | 12559 | 168 | 189 | 207 | 701 | 506 | 252 | 522 | 2.39 | 0.00 | 7.57 | 2.59 | 0.011 | 8.62 | 6.73 | 0.029 | 2.82 |
| BR4 | 861 | 10654 | 157 | 176 | 161 | 187 | 176 | 225 | 175 | 2.31 | 800.0 | 8.38 | 2.46 | 0.012 | 9.28 | 08.9 | 0.049 | 8.43 |
| NY C | 932 | 12638 | 165 | 420 | 231 | 218 | 179 | 248 | 184 | 2.61 | 0.010 | 7.69 | 2.52 | 0.010 | 8.61 | 6.71 | 0.030 | 3.67 |
| ENT | 160 | 7367 | 137 | 150 | 167 | 155 | 191 | 259 | 148 | 2.05 | 0.010 | 9.53 | 2.42 | 0.023 | 10.58 | 6.77 | 0.082 | 19.95 |
| HAI, | 748 | 8603 | 143 | 155 | 171 | 191 | 274 | 241 | 157 | 5.09 | 0.00 | 9.28 | 2.39 | 0.018 | 10.21 | 6.77 | 0.071 | 15.82 |
| KFA | 186 | 13086 | 168 | 195 | 207 | 375 | 181 | 402 | 189 | 4.17 | 0.054 | 7.65 | 2.73 | 0.016 | 8.79 | 69.9 | 0.03 | 1.76 |
| 1,R | 757 | 10206 | 148 | 180 | 342 | 173 | <u>2</u> | 211 | 162 | 2.20 | 800.0 | 8.71 | 2.34 | 0.010 | 9.46 | 6.75 | 0.054 | 10.53 |
| MBA | 1017 | 12951 | 701 | 192 | 210 | 202 | 193 | 246 | 191 | 2.41 | 0.00 | 7.42 | 2.59 | 0.011 | 8.45 | 6.70 | 0.026 | 1.92 |
| MBR | 821 | 11368 | 303 | 169 | 184 | 178 | 190 | 226 | 691 | 2.21 | 0.00 | 8.32 | 2.41 | 0.010 | 9.17 | 6.71 | 0.042 | 7.50 |

| Г | _ | _ | | | _ | - | | | _ | _ | | _ | _ | - |
|-----------|---------|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------|-------|-------|
| DADE | LAK 1.2 | (µg/m³) | 7.23 | 7.12 | 7.55 | 7.37 | 8.00 | 7.38 | 10.58 | 9.57 | 8.90 | 8.27 | 7.17 | 7 88 |
| NIO 2 | 7.70 | (PPM) | 0.010 | 0.010 | 0.011 | 0.011 | 0.011 | 0.012 | 0.023 | 0.05 | 0.045 | 0.013 | 0.010 | 1100 |
| 000 | 7.00 | (PPM) | 2.44 | 2.45 | 2.43 | 2.43 | 2.31 | 2.48 | 2.81 | 2.52 | 3.06 | 2.34 | 2.43 | 336 |
| DADTI | 1.174 | (µg/m³) | 8.16 | 7.72 | 8.71 | 8.50 | 9.07 | 8.32 | 10.79 | 10.46 | 9.05 | 9.94 | 8.29 | 90 |
| NO.3 | 1.70 | (PPM) | 0.017 | 0.018 | 0.015 | 910.0 | 0.017 | 0.022 | 0.016 | 0.015 | 0.212 | 0.015 | 0.016 | 0.014 |
| 100 | 5 | (PPM) | 3.24 | 3.53 | 3.08 | 3.13 | 3.11 | 3.84 | 2.35 | 2.43 | 10.47 | 2.69 | 3.14 | 196 |
| 0000 | 2 | (µg/m³) | 252 | 278 | 232 | 947 | 229 | 239 | 156 | 170 | 236 | 182 | 242 | 187 |
| 0.507 | 3 | (µg/m³) | 328 | 313 | 324 | 325 | 301 | 314 | 387 | 372 | 811 | 212 | 298 | 281 |
| CANA | 3 | (µg/m³) | 1931 | 238 | 281 | 897 | 235 | 205 | 146 | 426 | 204 | 163 | 252 | 256 |
| NOCK | 2 | (µg/m³) | 263 | 293 | 240 | 249 | 239 | 313 | 162 | 171 | 940 | 193 | 252 | 102 |
| VOCE | 3 | (µg/m³) | 283 | 306 | 262 | 270 | 258 | 335 | 208 | 213 | 258 | 564 | 569 | 213 |
| S COLLCE | 3 | (mg/m ₃) | 247 | 272 | 228 | 235 | 226 | 854 | 162 | 691 | 236 | 229 | 237 | 184 |
| 1007 | 3 | (µg/m³) | 802 | 228 | 193 | 861 | 192 | 661 | 140 | 146 | 197 | 159 | 303 | 442 |
| COOM TALL | 700 | (µg/m³) | ž | ž | ž | ž | ž | ž | ž | × | ž | ¥ | ž | YZ |
| 7 100/1 | 3 | (µg/m³) | 1164 | 1274 | 1040 | 1087 | 1003 | 982 | 814 | 843 | 993 | 646 | 1074 | 770 |
| I and 27 | | | BA2 | BA3 | BR2 | BR3 | BR4 | DR | ENT | IIAL. | ΚFΛ | LR R | MBA | MRP |

| | CO.1 | C0.2 | CO.1 CO.2 |
|----------|-------|-------|-----------|
| | (PPM) | (PPM) | |
| BA2 | 2.24 | 2.51 | |
| BA3 | 2.26 | 2.52 | |
| DR2 | 2.30 | 2.52 | |
| BR3 | 2.27 | 2.51 | |
| BR4 | 2.40 | 2.35 | |
| DK DK | 2.29 | 2.58 | |
| ENT | 2.38 | 3.12 | |
| IM | 2.40 | 2.70 | |
| ΚΓΛ | 16.55 | 3.44 | |
| LR | 2.39 | 2.39 | |
| MBA | 2.23 | 2.49 | |
| MBR | 2.27 | 2.43 | |

| VOCI | Burst - BMT | CO.1 | Oven |
|------|--------------|--------|-------------|
| VOC2 | Floor | NO2.1 | Oven |
| VOC3 | Burst - MBR | PART.1 | Oven |
| VOC4 | Burst - DR | | Heater |
| VOCS | Burst - LR | | Heater |
| VOC6 | Burst - KI'A | PART.2 | Heater |
| VOC7 | Burst - BA2 | | Outdoor air |
| VOC8 | Burst - GAR | | Outdoor air |
| VOC9 | Burst - BR3 | _ | Outdoor air |

| able 24 | a - SIM2l | MTH ove | rall 24-hr | avg conc | entration | S | | | | | | | | | |
|----------|-----------|---------|------------|----------|-----------|---------|---------|---------|---------------|-------|-------|---------|-------|-------|---------|
| | VOCI | V0C2 | VOC3 | VOC4 | VOCS | 900v | V0C7 | VOC8 | VOC9 | CO.1 | NO2.1 | PART.1 | CO.3 | NO2.3 | PART. |
| | (µg/m³) | (µg/m³) | (mg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | $\overline{}$ | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| 4 hr ave | 802 | 21581 | 184 | 205 | 218 | 218 210 | 200 | 232 | 197 | 2.60 | 0.015 | 7.78 | 6.83 | 0.041 | 6.13 |

| | VOCI | VOC2 | VOC3 | VOC4 | VOCS | VOC6 | VOC7 | VOC8 | VOC9 | CO.1 | NO2.1 | PART.1 | CO.3 | NO2.3 | PART.3 |
|------|---------|---------|---------|---------|---------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|
| | (mg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| 3A2 | 1787 | 19708 | 326 | 372 | 416 | 383 | 12685 | 328 | 393 | 4.62 | 0.082 | 7.48 | 8.61 | 0.053 | 3.56 |
| BA3 | 1802 | 25067 | 336 | 383 | 430 | 396 | 347 | 330 | 405 | 4.81 | 0.089 | 7.42 | 8.61 | 0.055 | 0.67 |
| 3R2 | 1662 | 16995 | 313 | 356 | 389 | 364 | 389 | 319 | 364 | 4.36 | 0.070 | 8.46 | 8.60 | 0.059 | 7.29 |
| 383 | 1756 | 18378 | 320 | 365 | 398 | 373 | 407 | 321 | 4725 | 4.40 | 0.073 | 8.13 | 8.60 | 0.052 | 5.14 |
| 3R4 | 1742 | 16877 | 318 | 362 | 396 | 370 | 462 | 320 | 370 | 4.37 | 0.073 | 8.42 | 8.61 | 0.053 | 7.60 |
| Z. | 1644 | 22011 | 302 | 3309 | 477 | 411 | 314 | 347 | 354 | 5.02 | 0.094 | 7.98 | 8.59 | 0.055 | 7.50 |
| IN | 1412 | 11711 | 268 | 302 | 329 | 308 | 349 | 630 | 309 | 3.89 | 0.064 | 11.09 | 9.93 | 0.171 | 34.59 |
| -tvr | 1657 | 13536 | 300 | 337 | 372 | 345 | 2583 | 490 | 362 | 3.97 | 0.049 | 10.87 | 9.21 | 0.137 | 25.87 |
| CFA | 1748 | 19698 | 310 | 380 | 387 | 2024 | 320 | 750 | 329 | 17.63 | 0.591 | 8.81 | 8.66 | 0.049 | 2,21 |
| R | 1396 | 14588 | 267 | 375 | 2259 | 312 | 273 | 562 | 307 | 3.77 | 0.055 | 10.14 | 9.15 | 0.097 | 17.64 |
| MBA | 1783 | 18821 | 451 | 371 | 416 | 382 | 342 | 322 | 392 | 4.62 | 0.082 | 8.21 | 8.62 | 0.053 | 3.88 |
| MBR | 1497 | 13989 | 1857 | 313 | 343 | 321 | 369 | 284 | 321 | 3.84 | 0.051 | 0.07 | 888 | 0.087 | 15 43 |

| | _ | _ | _ | | | | | | | _ | | | | _ |
|------------|--------|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | PART.3 | (µg/m³) | 1.14 | 0.42 | 3.12 | 1.80 | 2.91 | 2.68 | 20.82 | 10.76 | 1.01 | 11.14 | 1.26 | 8.31 |
| | NO2.3 | (PPM) | 0.028 | 0.024 | 0.033 | 0.029 | 0.033 | 0.029 | 0.088 | 0.00 | 0.025 | 0.058 | 0.028 | 0.050 |
| | CO.3 | (PPM) | 7.12 | 7.42 | 7.04 | 7.06 | 7.01 | 7.20 | 6.77 | 6.73 | 7.19 | 6.85 | 7.02 | 18.9 |
| | PART.1 | (µg/m³) | 7.13 | 6.41 | 7.58 | 7.35 | 7.55 | 7.20 | 65.6 | 8.84 | 7.20 | 8.83 | 7.36 | 8.57 |
| | N02.1 | (PPM) | 0.009 | 0.010 | 0.009 | 0.00 | 0.00 | 0.010 | 0.012 | 0.010 | 0.044 | 0.010 | 0.009 | 0.009 |
| | CO.1 | (PPM) | 2.67 | 3.00 | 2.52 | 2.57 | 2.53 | 2.81 | 2.06 | 2.14 | 3.90 | 2.23 | 2.57 | 2,22 |
| | V0C9 | (µg/m³) | 204 | 220 | 192 | 431 | 195 | 199 | 153 | 169 | 199 | 991 | 861 | 170 |
| | 800x | (mg/m ₃) | 215 | 219 | 211 | 214 | 506 | 232 | 212 | 208 | 404 | 172 | 202 | 183 |
| | V0C7 | (µg/m³) | 745 | 208 | 961 | 201 | 200 | 187 | 152 | 536 | 187 | 91 | 194 | 180 |
| | 00Ce | (µg/m³) | 210 | 228 | 197 | 203 | 200 | 223 | 156 | 168 | 327 | 171 | 203 | 173 |
| niralions | VOCS | (mg/m ₃) | 221 | 240 | 503 | 215 | 211 | 239 | 691 | 182 | 216 | 293 | 214 | 183 |
| ivg conce | V0C4 | (µg/m³) | 202 | 222 | 193 | 661 | 195 | 392 | 155 | 191 | 207 | 184 | 199 | 171 |
| nc 24-hr a | VOC3 | (µg/m³) | 181 | 195 | 172 | 177 | 174 | 178 | 142 | 152 | 178 | 152 | 200 | 260 |
| M I H 201 | VOC2 | (µg/m³) | 13039 | 14423 | 12080 | 12648 | 12158 | 13781 | 6335 | 8265 | 13172 | 9781 | 12832 | 9882 |
| tc - SIMZ | VOCI | (µg/m³) | 992 | 1109 | 903 | 946 | 910 | 905 | 662 | 743 | 910 | 649 | 676 | 717 |
| Table 74 | | | BA2 | BA3 | BR2 | BR3 | BR4 | DR | ENT | HAL | KFA | 1.R | MBA | MBR |
| | | | | | | | | | | | | | | |

| 4 2000 | 2010 - DL7 2100 I | | 111 COUC T- III G | · B collect | and and | | | | | | | |
|--------|-------------------|---------|-------------------|-------------|---------|---------|----------------------|---------|---------|-------|-------|---------|
| | VOCI | VOC2 | VOC3 | VOC4 | VOCS | 00Ce | V0C7 | 00C8 | VOC9 | CO.1 | NO2.1 | PART. |
| | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (mg/m ₃) | (µg/m³) | (µg/n³) | (PPM) | (PPM) | (µg/m³) |
| BA2 | 1252 | ž | 226 | 566 | 298 | 277 | 2261 | 271 | 271 | 3.88 | 0.031 | 7.14 |
| BA3 | 1332 | × | 235 | 278 | 309 | 290 | 250 | 267 | 280 | 3.97 | 0.033 | 7.07 |
| BR2 | 1164 | × | 217 | 255 | 285 | 265 | 279 | 797 | 260 | 3.74 | 0.027 | 7.23 |
| BR3 | 1187 | × | 220 | 258 | 586 | 569 | 276 | 268 | 1116 | 3.77 | 0.028 | 7.22 |
| 3R4 | 1162 | × | 217 | 254 | 285 | 265 | 277 | 265 | 260 | 3.74 | 0.028 | 7.32 |
| DR | 1116 | ٧X | 216 | 920 | 329 | 303 | 226 | 564 | 256 | 4.12 | 0.034 | 7.25 |
| EN. | 825 | ٧X | 155 | 176 | 216 | 178 | 184 | 405 | 176 | 2.84 | 0.024 | 9.71 |
| HAL | 880 | ž | 171 | 195 | 230 | 661 | 546 | 347 | 212 | 3.13 | 0.022 | 8.67 |
| ΚFΛ | 1099 | ٧V | 214 | 592 | 278 | 119 | 223 | 1119 | 253 | 7.69 | 0.151 | 7.74 |
| R | 812 | ×Z | 180 | 252 | 655 | 216 | 193 | 220 | 208 | 3.23 | 0.023 | 8.62 |
| MBA | 1205 | ٧× | 301 | 262 | 292 | 273 | 250 | 252 | 266 | 3.84 | 0.030 | 7.19 |
| MAD | 888 | YZ | 2,60 | 214 | 230 | 222 | 250 | 231 | 220 | 3 30 | 0.00 | 8 14 |

|--|--|--|--|--|--|--|

| מכנות | | | |
|-------|-------------|--------|------------|
| 100A | Burst - BMT | CO.1 | Oven |
| V0C2 | Floor | N02.1 | Oven |
| VOC3 | Burst - MBR | PART.1 | Oven |
| VOC4 | Burst - DR | CO.2 | Heater |
| VOC5 | Burst - LR | NO2.2 | Heater |
| VOC6 | Burst - KFA | PART.2 | Heater |
| V0C7 | Burst - BA2 | _ | Outdoor at |
| 00C8 | Burst - GAR | N02.3 | Outdoor ai |
| VOC9 | Burst - BR3 | PART.3 | Outdoor ai |

| Table 25s | - SIMIF | LCF over | Table 25a - SIM IFLCF overall 24-hr avg concentration | avg conc | entrations | S | | | | | | | | | | | | |
|---------------------------------------|---------|----------|---|----------------------|------------|---------|---------|---------|---------|------|-------|---------|------|-------|---------|-------|-------|---------|
| | VOCI | V0C2 | VOC3 | VOC4 | VOC5 | 900A | V0C7 | 800X | VOC9 | CO.1 | N02.1 | PART.1 | CO.2 | NO2.2 | PART.2 | CO.3 | NO2.3 | PART.3 |
| | (µg/m³) | (µg/m³) | (mg/m ₃) | (mg/m ₃) | (µg/m³) | (µg/m³) | (mg/m³) | (µg/m³) | (µg/m³) | mdd | mdd | (µg/m³) | mdd | udd | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| 24 hr avg | 265 | 2909 | 218 | 183 | 117 | 225 | 219 | 217 | 205 | 2.75 | 0.026 | 9.26 | 1.60 | 800.0 | 9.17 | 6.77 | 0.079 | 14.52 |
| | | | | | | | | | | | | | | | | | | |
| T.L. OCL. CIMIEI OF and and acceptant | CINCIL | TOTAL | 1000 | | | | | | | | | | | | | | | |

| U | VOC2 | VOC3 | VOCI VOC2 VOC3 VOC4 VOC | VOCS | 900A | VOC7 | VOC8 | VOC9 | CO.1 | N02.1 | PART.1 | CO.2 | NO2.2 | PART.2 | CO.3 | NO2.3 | PART.3 |
|--------|------|---------|-------------------------|---------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|
| ug/m³) | | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| 1815 | | 645 | 232 | 131 | 393 | 347 | 13163 | 281 | 4.93 | 0.056 | 8.31 | 2.25 | 0.010 | 8.31 | 9.48 | 0.104 | 8.89 |
| 9465 | | 384 | 197 | 126 | 314 | 271 | 253 | 234 | 4.10 | 0.047 | 10.14 | 2.35 | 0.017 | 10.13 | 9.84 | 0.165 | 22.86 |
| 1060 | | 672 | 506 | 126 | 347 | 354 | 274 | 4099 | 4.57 | 0.046 | 9.36 | 2.30 | 0.011 | 9.36 | 9.65 | 0.107 | 16.59 |
| 1961 | | 1630 | 303 | 177 | 462 | 296 | 390 | 407 | 5.50 | 0.083 | 11.36 | 2.46 | 0.017 | 11.35 | 10.15 | 991.0 | 26.29 |
| 7974 | | 297 | 274 | 091 | 4332 | 255 | 258 | 236 | 44.43 | 1.434 | 14.46 | 2.41 | 0.014 | 11.07 | 10.00 | 0.140 | 23.94 |
| 7537 | | 337 | 1593 | 416 | 482 | 258 | 237 | 215 | 6.14 | 0.089 | 10.64 | 2.42 | 0.013 | 10.68 | 10.03 | 0.132 | 19.44 |
| \$409 | | 293 | 208 | 125 | 312 | 9360 | 500 | 247 | 3.92 | 0.054 | 11.93 | 2.51 | 0.019 | 11.93 | 10.35 | 0.191 | 33.43 |
| 5516 | | 2430 | 178 | 120 | 256 | 752 | 221 | 214 | 3.33 | 0.045 | 11.80 | 2.51 | 0.021 | 11.80 | 10 34 | 0.210 | 35 40 |

| Table 250 | C - SIMIF | LCF zone | 3 24-hr av | 'g concer | trations | | | | | | | | | | | | | |
|----------------------------|-----------|----------|------------|-----------|----------|---------|---------|----------|----------------------|-------|-------|---------|-------|-------|---------|-------|-------|---------|
| VOC1 VOC2 VOC3 VOC4 VOC5 V | VOCI | VOC2 | VOC3 | VOC4 | VOCS | 920A | VOC7 | NOC8 | VOC9 | CO.1 | NO2.1 | PART.1 | CO.2 | NO2.2 | PART.2 | CO.3 | NO2.3 | PART.3 |
| | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/in³) | (mg/m ₃) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (FPM) | (µg/m³) |
| BA2 | 134 | 8418 | 255 | 138 | 109 | 130 | 200 | 1915 | 160 | 2.38 | 0.000 | 7.13 | 19.1 | 0.005 | 7.09 | 08.9 | 0.047 | 3.48 |
| BR2 | 112 | 6422 | 172 | 124 | 901 | 157 | 155 | 149 | 137 | 2.09 | 0.010 | 8.98 | 19.1 | 0.007 | 8.95 | 6.81 | 0.075 | 13.07 |
| BR3 | 113 | 8211 | 252 | 132 | 107 | 178 | 961 | 165 | 727 | 2.30 | 0.00 | 7.73 | 1.62 | 0.005 | 7.69 | 6.82 | 0.000 | 5.13 |
| HAL | 123 | 5249 | 316 | 128 | 108 | 177 | 223 | 155 | 145 | 2.32 | 910.0 | 9.75 | 1.60 | 0.00 | 9.70 | 6.77 | 0.086 | 16.09 |
| KIT | 105 | 5540 | 149 | 133 | 109 | 647 | 142 | 142 | 132 | 6.59 | 0.124 | 9.80 | 1.60 | 0.008 | 9.28 | 6.74 | 0.084 | 15.70 |
| LDA | 901 | 6040 | 162 | 312 | 141 | 206 | 147 | 141 | 131 | 2.62 | 0.018 | 9.26 | 19.1 | 0.008 | 9.18 | 6.77 | 0.076 | 13.63 |
| MBA | 104 | 4130 | 136 | 911 | 103 | 136 | 1021 | 133 | 125 | 1.92 | 0.013 | 10.03 | 1.59 | 0.010 | 10.02 | 6.71 | 0.105 | 22.29 |
| MRR | 107 | 3082 | 345 | 113 | 103 | 120 | 256 | 127 | 122 | 1.85 | 0.012 | 10.54 | 1 50 | 1100 | 10.52 | 677 | 0 108 | 24.41 |

| Table 25 | able 25d - SIMIFLCF | LCF zon | e 4-hr av | g concent, | rations | | | | | | | | | | |
|----------|---------------------|----------------------|-----------|------------|---------|---------|----------|---------|---------|-------|-------|---------|-------|-------|---------|
| | VOCI | VOC2 | VOC3 | VOC4 | VOC5 | 900A | VOC7 | VOC8 | VOC9 | CO.1 | NO2.1 | PART.1 | CO.2 | NO2.2 | PART.2 |
| | (µg/m³) | (mg/m ₃) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| BA2 | 147 | Ν | 449 | 170 | 811 | 276 | 274 | 5479 | 504 | 3.51 | 0.015 | 7.27 | 1.55 | 0.007 | 6.82 |
| BR2 | 114 | Ν | 289 | 145 | 113 | 500 | 202 | 175 | 191 | 2.93 | 0.012 | 8.78 | 99.1 | 0.012 | 9.20 |
| BR3 | 114 | ¥ | 426 | 153 | 114 | 243 | 249 | 190 | 1958 | 3.36 | 0.015 | 7.98 | 1.54 | 0.007 | 7.27 |
| HAL | 138 | Ν | 170 | 168 | 126 | 327 | 394 | 200 | 213 | 4.21 | 0.036 | 68.6 | 1.65 | 0.012 | 99.6 |
| KIT | 104 | Ϋ́ | 981 | 181 | 126 | 1808 | 891 | 170 | 191 | 23.65 | 0.515 | 11.79 | 1.60 | 0.011 | 8.84 |
| LDA | 105 | Ϋ́ | 204 | 168 | 244 | 325 | <u>2</u> | 160 | 151 | 5.09 | 0.046 | 99.6 | 1.59 | 0.010 | 8.71 |
| MBA | 102 | Ϋ́ | 181 | 137 | 801 | 174 | 3126 | 159 | 152 | 2.59 | 0.013 | 10.23 | 1.64 | 0.013 | 9.52 |
| MBR | 108 | NA | 922 | 133 | 108 | 164 | 551 | 150 | 152 | 2.47 | 0.012 | 10.50 | 1.69 | 0.015 | 10.54 |
| | | | | | | | | | | | | | | | |

| one 1-hr avg concentration | 2 | <u> </u> | | | | | | LDA 3.87 1.65 | | |
|----------------------------|------|----------|------|------|------|------|-------|---------------|------|------|
| LCF z | CO.7 | (PPM | 1.67 | 1.68 | 1.65 | 1.66 | 1.6 | 1.65 | 1.63 | |
| 25e - SIMIF | CO.1 | (PPM) | 2.54 | 2.52 | 2.58 | 3.54 | 33.72 | 3.87 | 2.55 | 0,00 |
| Table 2 | | | BA2 | BR2 | BR3 | HAL | KIT | LDA | MBA | 2000 |

| LEGEND | 0 | | |
|--------|-------------|--------|-------------|
| VOCI | Burst - UCL | CO.1 | Oven |
| VOC2 | Floor | N02.1 | Oven |
| VOC3 | Burst - MBR | PART.1 | Oven |
| VOC4 | Burst - LDA | CO.2 | Heater |
| VOCS | Burst - GAR | NO2.2 | Heater |
| NOC6 | Burst - KIT | PART.2 | Heater |
| VOC7 | Burst - MBA | CO.3 | Outdoor air |
| VOC8 | Burst - BA2 | N02.3 | Outdoor air |
| VOC9 | Burst - BR3 | PART.3 | Outdoor air |

| | | | | 1 | | | | | | | | | | | _ |
|---|--------|----------------------|-----------|---|---|--------|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|
| | PART.3 | (µg/m³) | 14.74 | | | PART.3 | (µg/m³) | 8.90 | 22.99 | 16.59 | 26.38 | 23.95 | 19.44 | 33.44 | 35.56 |
| | NO2.3 | (PPM) | 0.084 | | | NO2.3 | (PPM) | 0.134 | 0.179 | 0.124 | 0.171 | 0.154 | 0.141 | 0.191 | 0.213 |
| | CO.3 | (PPM) | 6.79 | | | CO.3 | (PPM) | 9.73 | 10.04 | 98.6 | 10.32 | 10.19 | 10.20 | 10.57 | 10.50 |
| | PART.2 | (mg/m ₃) | 10.92 | | | PART.2 | (mg/m ₃) | 10.73 | 11.58 | 10.70 | 11.91 | 11.62 | 11.25 | 12.16 | 12.19 |
| | NO2.2 | mdd | 0.008 | | | NO2.2 | (PPM) | 0.013 | 0.018 | 0.012 | 0.017 | 0.015 | 0.014 | 0.019 | 0.021 |
| | CO.2 | mdd | 19.1 | | | CO.2 | (PPM) | 2.32 | 2.40 | 2.36 | 2.50 | 2.46 | 2.47 | 2.57 | 2.55 |
| | PART.1 | (µg/m³) | 11.02 | | | PART.1 | (µg/m³) | 10.74 | 11.59 | 10.72 | 11.93 | 15.81 | 11.32 | 12.16 | 12.19 |
| | NO2.1 | mdd | 0.026 | | | NO2.1 | (PPM) | 0.051 | 0.044 | 0.042 | 0.080 | 1.435 | 0.000 | 0.050 | 0.042 |
| | CO.1 | mdd | 2.68 | | | CO.1 | (PPM) | 4.49 | 3.78 | 4.24 | 5.21 | 44.46 | 91.9 | 3.54 | 3.06 |
| | V0C9 | (µg/m³) | 199 | | | V0C9 | (µg/m³) | 249 | 210 | 4094 | 330 | 212 | 195 | 221 | 200 |
| | VOC8 | (µg/m³) | 208 | | | VOC8 | (µg/m³) | 13153 | 225 | 245 | 365 | 230 | 212 | 236 | 199 |
| | V0C7 | $(\mu g/m^3)$ | 211 | | | V0C7 | (µg/m³) | 319 | 247 | 332 | 594 | 231 | 236 | 9358 | 750 |
| S | 920A | (µg/m³) | 216 | | | 900A | (µg/m³) | 347 | 279 | 310 | 431 | 4328 | 478 | 275 | 228 |
| entration | VOCS | (µg/m³) | 116 | | ons | VOCS | (µg/m³) | 125 | 123 | 121 | 174 | 157 | 414 | 120 | 118 |
| avg con | VOC4 | $(\mu g/m^3)$ | 178 | | oncentrati | VOC4 | $(\mu g/m^3)$ | 500 | 180 | 189 | 287 | 257 | 1591 | 189 | 26 |
| rall 24-h | VOC3 | (μg/m³) | 509 | | e peak co | V0C3 | (µg/m³) | 638 | 352 | 999 | 1627 | 268 | 313 | 261 | 2428 |
| LCH ove | VOC2 | (mg/m³) | 5563 | | LCH zon | VOC2 | (µg/m³) | 10953 | 8668 | 10390 | 7338 | 7348 | 7200 | 2807 | 2909 |
| Table 26a - SIM1FLCH overall 24-hr avg concentrations | VOCI | (µg/m³) | 263 | | Fable 26b - SIM1FLCH zone peak concentrations | VOCI | (µg/m³) | 302 | 184 | 156 | 332 | 134 | 131 | 134 | 149 |
| Table 26s | | | 24 hr avg | | Table 26t | | | BA2 | BR2 | BR3 | HAL | KIT | LDA | MBA | MBR |

| Table 26 | c - SIMIF | LCH zon | e 24-hr a | vg conce | ntrations | | | | | | | | | | | | | |
|----------|---------------------|---------------|-----------|-----------------------|-----------|---------|---------|---------|---------------|-------|-------|---------|-------|-------|---------|-------|-------|---------|
| | VOCI VOC2 VOC3 VOC4 | V0C2 | V0C3 | V0C4 | VOCS | 900A | VOC7 | VOC8 | V0C9 | CO.1 | NO2.1 | PART.1 | CO.2 | NO2.2 | PART.2 | CO.3 | NO2.3 | PART.3 |
| | (µg/m³) | $(\mu g/m^3)$ | (µg/m³) | (µg/m ⁻³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | $(\mu g/m^3)$ | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| BA2 | 132 | 7558 | 240 | 131 | 107 | 173 | 186 | 1899 | 148 | 2.26 | 0.009 | 10.11 | 1.62 | 900.0 | 10.05 | 6.84 | 0.056 | 3.83 |
| BR2 | Ξ | 5888 | 162 | 119 | 105 | 147 | 146 | 140 | 130 | 2.01 | 0.010 | 10.82 | 1.61 | 0.008 | 10.79 | 6.83 | 0.080 | 13.30 |
| BR3 | == | 7485 | 240 | 126 | 106 | 165 | 184 | 153 | 717 | 2.19 | 0.009 | 10.23 | 1.62 | 9000 | 10.19 | 6.85 | 0.057 | 5.41 |
| HAL | 121 | 4824 | 309 | 124 | 107 | 169 | 216 | 148 | 139 | 2.25 | 0.016 | 11.24 | 1.60 | 0.009 | 11.18 | 6.78 | 0.000 | 16.29 |
| KIT | 104 | 5032 | 140 | 129 | 108 | 638 | 134 | 133 | 126 | 6.51 | 0.124 | 11.59 | 1.60 | 0.009 | 11.06 | 91.9 | 0.089 | 15.95 |
| LDA | 104 | 5545 | 154 | 308 | 140 | 161 | 139 | 133 | 125 | 2.55 | 0.019 | 10.99 | 1.62 | 0.008 | 10.01 | 6.79 | 0.081 | 13.84 |
| MBA | 103 | 3712 | 129 | 113 | 102 | 128 | 1044 | 126 | 120 | 1.85 | 0.013 | 11.54 | 1.59 | 0.011 | 11.52 | 6.72 | 0.110 | 22.54 |
| MBR | 901 | 3669 | 339 | 110 | 102 | 123 | 251 | 121 | 118 | 1.80 | 0.013 | 11.64 | 1.59 | 0.011 | 11.62 | 6.73 | 0.112 | 24.58 |

| Table 26d | - SIMIF | LCH zon | e 4-hr avg | g concent | rations | | | | | | | | | | |
|-------------|----------|---------|----------------------|-----------|---------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|
| VOCI VOC2 V | VOCI | V0C2 | VOC3 | VOC4 | VOCS | 900v | VOC7 | VOC8 | V0C9 | CO.1 | NO2.1 | PART.1 | C0.2 | NO2.2 | PART.2 |
| | (µg/m³) | (µg/m³) | (mg/m ₃) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (mg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| BA2 | 145 | Ν | 426 | 158 | 115 | 251 | 256 | 5458 | 186 | 3.41 | 0.015 | 9.74 | 1.59 | 0.008 | 10.44 |
| BR2 | 113 | NA | 274 | 138 | Ξ | 193 | 190 | 162 | 156 | 2.86 | 0.012 | 10.39 | 1.68 | 0.013 | 11.30 |
| BR3 | 112 | NA | 408 | 14 | 112 | 224 | 235 | 174 | 1945 | 3.29 | 0.015 | 9.95 | 1.58 | 0.008 | 10.46 |
| HAL | 137 | NA | 757 | 162 | 125 | 313 | 384 | 189 | 204 | 4.14 | 0.036 | 11.10 | 1.67 | 0.013 | 11.47 |
| KIT | 103 | Ν | 172 | 173 | 124 | 1793 | 157 | 158 | 150 | 23.57 | 0.515 | 13.20 | 1.63 | 0.012 | 11.18 |
| LDA | <u>8</u> | Ν | 192 | 191 | 243 | 311 | 155 | 149 | 142 | 5.03 | 0.046 | 10.98 | 1.61 | 0.011 | 11.03 |
| MBA | 102 | NA | 169 | 130 | 106 | 191 | 3116 | 148 | 143 | 2.51 | 0.013 | 11.41 | 1.66 | 0.014 | 11.55 |
| MBR | 108 | NA | 912 | 127 | 107 | 153 | 543 | 141 | 4 | 2.41 | 0.012 | 11.42 | 1.70 | 0.016 | 11.87 |

| : 1-hr avg concentrations | • | | | | | | | | | MBR 2.54 1.64 |
|---------------------------|------|-------|------|------|------|------|-------|------|------|---------------|
| CH zone | CO.2 | (PPM) | 1.70 | 1.69 | 1.68 | 1.67 | 1.66 | 1.67 | 1.6 | 1.64 |
| - SIMIF | CO.1 | (PPM) | 2.58 | 2.55 | 2.62 | 3.56 | 33.75 | 3.90 | 2.58 | 2.54 |
| Table 26e | | | BA2 | BR2 | BR3 | HAL | KIT | LDA | MBA | MBR |

| LEGEND | 0 | | | |
|--------|-------------|--------|-------------|--|
| 100V | Burst - UCL | CO.1 | Oven | |
| VOC2 | Floor | N02.1 | Oven | |
| VOC3 | Burst - MBR | PART.1 | Oven | |
| VOC4 | Burst - LDA | CO.2 | Heater | |
| VOCS | Burst - GAR | NO2.2 | Heater | |
| NOC6 | Burst - KIT | PART.2 | Heater | |
| VOC7 | Burst - MBA | CO.3 | Outdoor air | |
| VOC8 | Burst - BA2 | NO2.3 | Outdoor air | |
| VOC9 | Burst - BR3 | PART.3 | Outdoor air | |
| | | | | |

| | - | (PPM) (µg/m³) | | | _ | (PPM) (µg/m³) | | | | | | | | |
|-----------|--------------|------------------|-----------|--|--------|----------------------|-------|-------|-------|-------|-------|-------|-------|-----|
| | | (PPM) 6.78 | | | | (PPM) | | | | | | | | |
| | | (μg/m³) | | | Γ | (µg/m³) | | | | | | | | |
| | N02.2 | ppm 0 000 | | | N02.2 | (PPM) | 0.013 | 0.017 | 0.012 | 0.017 | 0.015 | 0.014 | 0.019 | |
| | C0.2 | mdd 1 60 | | | C0.2 | (PPM) | 2.28 | 2.37 | 2.33 | 2.47 | 2.43 | 2.44 | 2.54 | 1 |
| | PART.1 | (μg/m³) 10 97 | | | PART.1 | (µg/m³) | 10.71 | 11.56 | 10.66 | 11.92 | 15.75 | 11.29 | 12.16 | 0 |
| | N02.1 | mdd 0.056 | | | N02.1 | (PPM) | 0.051 | 0.044 | 0.042 | 0.081 | 1.437 | 0.090 | 0.050 | |
| | CO.1 | ppm 2.7.1 | | | C0.1 | (PPM) | 4.54 | 3.86 | 4.30 | 5.34 | 44.51 | 91.9 | 3.60 | |
| | VOC9 | (µg/m³) | | | V0C9 | (µg/m ₃) | 252 | 214 | 4097 | 396 | 216 | 198 | 224 | 000 |
| | 0008 0008 | (μg/m³) 211 | | | 800X | (µg/m³) | 13162 | 237 | 252 | 380 | 238 | 218 | 246 | 000 |
| | V0C7 | (μg/m³) 214 | | | VOC7 | (µg/m³) | 323 | 255 | 336 | 594 | 235 | 240 | 9359 | 1 |
| 5 | | (µg/m³) | 1 | | 900A | (µg/m³) | 354 | 289 | 319 | 448 | 4332 | 480 | 283 | 100 |
| ⊆۱ | | (µg/m³) | | rations | VOCS | (µg/m ₃) | | | | | | | | |
| -hr avg c | VOC4 | (µg/m³) (µg/m³) | | concent | VOC4 | _ | | | | | | | | |
| verall 24 | | | 1 | one peak | VOC3 | (µg/m³) | | | | | | | | |
| FLCHO (| | (µg/m³) | 1 | FLCH0 2 | VOC2 | (µg/m³) | | | | | | | | |
| a - SIMI | VOCI | (µg/m³) | 1 | Table 27b - SIM1FLCHO zone peak concentrations | VOCI | (µg/m³) | 288 | 179 | 151 | 318 | 131 | 129 | 132 | |
| Table 27 | | 24 hr ava | 9.11 11.2 | Table 27 | | | BA2 | BR2 | BR3 | HAL | KIT | LDA | MBA | |

| Table 7/ | C-SIMIL | LCHU ZO | ne 24-nr | avg conc | entrations | | | | | | | | | | | | | |
|----------|---------------------------------------|---------|----------|----------|------------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|-------|-------|---------|
| | VOCI | VOC2 | V0C3 | V0C4 | VOCS | | V0C7 | VOC8 | 620A | CO.1 | NO2.1 | PART.1 | CO.2 | N02.2 | PART.2 | CO.3 | N02.3 | PART.3 |
| | m/gn) (εm/gn) (εm/gn) (εm/gn) (εm/gn) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (μg/m³) | (µg/m³) | (μg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (μg/m³) | (PPM) | (PPM) | (mg/m³) |
| BA2 | 127 | 7754 | 245 | 129 | 194 | | 190 | 1907 | 150 | 2.28 | 0.00 | 10.05 | 1.61 | 0.005 | 66.6 | 6.82 | 0.054 | 3.64 |
| BR2 | 109 | 6075 | 991 | 118 | 103 | | 149 | 143 | 131 | 2.04 | 0.010 | 10.76 | 19.1 | 800.0 | 10.73 | 6.82 | 0.078 | 12.91 |
| BR3 | 109 | 7704 | 245 | 125 | <u>\$</u> | | 188 | 157 | 722 | 2.22 | 600.0 | 10.17 | 1.62 | 900.0 | 10.12 | 6.84 | 0.055 | 5.08 |
| HAL | 119 | 4968 | 313 | 123 | 105 | | 219 | 151 | 141 | 2.27 | 910.0 | 11.19 | 1.60 | 600.0 | 11.13 | 6.77 | 0.089 | 15.92 |
| KIT | 103 | 5158 | 142 | 125 | 105 | | 136 | 136 | 127 | 6.61 | 0.125 | 11.56 | 1.60 | 0.00 | 11.02 | 6.75 | 0.088 | 15.64 |
| LDA | 103 | 5720 | 157 | 308 | 132 | | 141 | 136 | 126 | 2.58 | 0.019 | 10.94 | 1.61 | 0.008 | 10.86 | 6.78 | 0.079 | 13.46 |
| MBA | 102 | 3834 | 131 | 112 | 101 | | 1050 | 128 | 121 | 1.87 | 0.013 | 11.50 | 1.59 | 0.011 | 11.48 | 6.71 | 0.109 | 22.14 |
| MBR | 105 | 3784 | 343 | 110 | 101 | | 254 | 123 | 119 | 1.81 | 0.012 | 11.60 | 1.59 | 0.011 | 11.58 | 6.72 | 0.111 | 24.17 |

| Table 27c | 1-SIMIE | LCHO zc | one 4-hr | wg conce | ntrations | | | | | | | | | | |
|-----------|---------|---------|----------|----------|-----------|---------|---------|---------|---------|-------|-------|---------|-------|-------|---------|
| | VOCI | VOC2 | V0C3 | V0C4 | VOC5 | 900A | V0C7 | VOC8 | 620A | CO.1 | N02.1 | PART.1 | CO.2 | N02.2 | PART.2 |
| | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (µg/m³) | (PPM) | (PPM) | (µg/m³) | (PPM) | (PPM) | (µg/m³) |
| BA2 | 138 | NA N | 433 | 156 | 108 | 256 | 260 | 5468 | 189 | 3.40 | 0.014 | 9.65 | 1.59 | 0.008 | 10.41 |
| BR2 | == | Ϋ́ | 281 | 137 | 107 | 198 | 194 | 168 | 158 | 2.87 | 0.012 | 10.31 | 1.68 | 0.013 | 11.26 |
| BR3 | 110 | NA | 417 | 143 | 107 | 230 | 240 | 181 | 1955 | 3.30 | 0.015 | 98.6 | 1.57 | 0.008 | 10.41 |
| HAL | 134 | NA | 765 | 160 | 116 | 320 | 389 | 195 | 506 | 4.16 | 0.036 | 11.05 | 1.67 | 0.013 | 11.44 |
| KIT | 103 | Ϋ́ | 177 | 163 | 114 | 1819 | 160 | 163 | 152 | 23.74 | 0.516 | 13.16 | 1.63 | 0.012 | 11.15 |
| LDA | 103 | Ν | 197 | 764 | 214 | 318 | 158 | 154 | 143 | 5.05 | 0.046 | 10.92 | 19.1 | 0.010 | 10.99 |
| MBA | 101 | Ν | 173 | 129 | 103 | 164 | 3125 | 152 | 14 | 2.52 | 0.013 | 11.37 | 99.1 | 0.014 | 11.51 |
| MBR | 107 | NA | 920 | 127 | 104 | 156 | 548 | 145 | 146 | 2.41 | 0.012 | 11.38 | 1.70 | 0.015 | 11.84 |

| Table 27e - SIM I FLCHO zone 1-hr avg concentrations | | | | | | | | | | |
|--|------|-------|------|------|------|------|-------|------|------|------------|
| CHO zon | CO.2 | (PPM) | 1.70 | 1.69 | 1.68 | 1.67 | 1.66 | 1.66 | 2.5 | <u>2</u> . |
| - SIMIF | CO.1 | (PPM) | 2.55 | 2.53 | 2.59 | 3.54 | 33.82 | 3.88 | 2.56 | 2.52 |
| Table 276 | | | BA2 | BR2 | BR3 | HAL | KIT | LDA | MBA | MBR |

| Q | Burst - UCL CO.1 Oven | | Burst - MBR | Burst - LDA CO.2 | Burst - GAR | | CO.3 O | Burst - BA2 NO2.3 Outdoor air | Burst - BR3 PART.3 Outdoor air |
|-------|-----------------------|------|-------------|--------------------|-------------|------|--------|-------------------------------|--------------------------------|
| LEGEN | VOCI | VOC2 | VOC3 | VOC4 | VOCS | 900A | VOC7 | VOC8 | VOC9 |





